INVESTIGATION OF WELDING THERMAL STRAINS IN MARINE STEELS

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BY

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ABSTRACT

The stress-strain-temperature response of metal plates during welding is discussed and current efforts to analyze the phenomena are outlined. Transient strain and temperature data obtained from welding experiments on HY-80, HY-130, low carbon and maraging steels are presented. The experiments were designed to approximate ship structural weldments including thick-section, multi-pass butt welds.

The experimental data are compared to analytical predictions obtained from computer programs developed for the National Aeronautics and Space Administration. Results indicate that the programs can be used to analyze complex structural weldments applicable to ship and submarine fabrication. It was also found that the effects of thick-section, multi-pass welding are more pronounced in the early passes and tend to level off as deposited weld metal increases. The transient strain response of both thin and thick section plates was found to be predominantly longitudinal



except in the immediate area of the welding arc itself. The maximum mechanical strains observed on plates of varying strength levels were found to be roughly proportional to the inverse of the base plate yield strength. Finally, the strain plots of the two highest strength steels were characterized by unusual secondary tensile peaks which may be linked to phase transformations in the heat affected zone during cool-down.

Several recommendations are made concerning further investigations aimed at developing the NASA programs and subsequent experiments into shipyard design and production tools.

THESIS SUPERVISOR: Koichi Masubuchi

TITLE: Professor of Naval Architecture



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NOMENCLATURE

v	travel speed of welding arc
$\Delta \mathbf{T}$	change in temperature
$\sigma_{\mathbf{x}}$	stress in x-direction
σy	stress in y-direction
τ_{xy}	shear stress
psì	pounds-per-square-inch
ksi	pounds-per-square-inch × 1,000
GMA	Gas Metal Arc welding process, also known as MIG (Metal Inert Gas)
ΔR	change in resistance
$\Delta R(\varepsilon_{\rm e})$	change in resistance corresponding to elastic mechanical strain
$\Delta R (\varepsilon_p)$	change in resistance corresponding to plastic mechanical strain
ΔR (αΤ)	change in resistance corresponding to temperature induced thermal strain
ΔR(T)	change in resistance caused by thermo-electric effects in the strain gage
°F	temperature in degrees Fahrenheit
DCRP	direct current, reversed polarity (electrode positive, plate negative)
ipm	inches-per-minute (a measure of travel speed)
02	molecular Oxygen (gaseous)
microstra	in 10 ⁻⁶ inches-per-inch elongation (or contraction)



I INTRODUCTION

A. Background

In the fabrication of complex welded structures, several serious problems are caused by the occurance of welding thermal strains. Distortion, strain aging and high residual stresses can be traced directly to this phenomenon. Unfortunately, thermal strains are inherent in the welding process. They result primarily from plastic flow accompanying localized arc heating. (A detailed discussion of the mechanism will be presented later.) If welding thermal strains cannot be prevented, structural safety and reliability demand that they be controlled. This concept is critical in the fabrication of modern ships and submarines.

The distortion problem in ship construction is well documented. Distortion often prevents the achievement of design tolerances, reduces joint strength by mismatching, and imparts initial deflections into structural members. 1,2,3 Corrugation of shell plating is a common distortion-induced failure in surface ships; in submarines, shape imperfections caused by weld distortion can result in premature yielding and hull failure by general instability. 4

The problems associated with residual stresses are equally ominous. Several investigators have established the role of residual welding stresses in the initiation of low-stress brittle fracture. ^{5,6} Below a certain temperature, normally ductile steels will fail catastrophically in the



presence of high tensile stresses and some sharp notch such as a weld crack or lack-of-fusion defect. Since residual welding stresses are often at or near the base plate yield strength, brittle fracture of welded structures can and has occurred at very low applied stress levels.

The development of high strength submarine steels has recently added a new dimension to the residual stress problem. Both quenched-and-tempered and maraging-type steels have been found highly susceptible to hydrogen embrittlement. At strength levels above 180-ksi, maraging steels have suffered stress corrosion cracking and hydrogen embrittlement in ordinary marine environments. 7,8 The exact mechanism controlling these failure modes has been the subject of considerable dispute, but both are characterized by time-dependent brittle fracture in areas of localized high tensile stress. 9

The problem of distortion and residual stress can be considered part of the cummulative results of welding processes. The transient strain response produced by a moving welding arc gives rise to yet another deleterious effect—strain aging. This term refers to the loss in ductility observed in certain steels undergoing plastic deformation during particular periods of time. Strain aging is strongly dependent on temperature and appears sensitive to tension—compression cycling. Ocupled with possible phase transformations in the heat-affected zone, weld-induced strain aging can result in severe degradation of the physical properties of the base plate.



B. Welding Stress-Strain Development

The mechanism by which thermal stresses and strains are developed in welded plates has been described by Dr. Koichi Masubuchi. 11 The description is based on current theories of heat flow and stress-strain-temperature relationships. It begins by recognizing that a weldment is locally heated by the welding arc, and the temperature in the metal is therefore not uniform and changes as welding progresses. This non-uniform temperature distribution causes thermal strains and stresses in the weldment which also change during the process.

Figure 1 shows schematically how welding thermal stresses are formed. Figure la indicates a bead-on-plate weld in which a weld bead is being deposited at a speed, v. O-xy is the coordinate system; the origin, O, is on the surface underneath the welding arc, and the x-direction lies in the direction of arc travel.

Figure 1b shows the temperature distribution along several cross sections. Along Section A-A, which is ahead of the arc, the temperature change due to welding, ΔT, is almost zero (Figure 1b-1). Along Section B-B, which crosses the welding arc, the temperature distribution is very steep (Figure 1b-2). Along Section C-C, some distance behind the arc, the distribution of temperature is as indicated in Figure 1b-3. Far behind the arc (Section D-D), the temperature change due to welding again diminishes (Figure 1b-4).



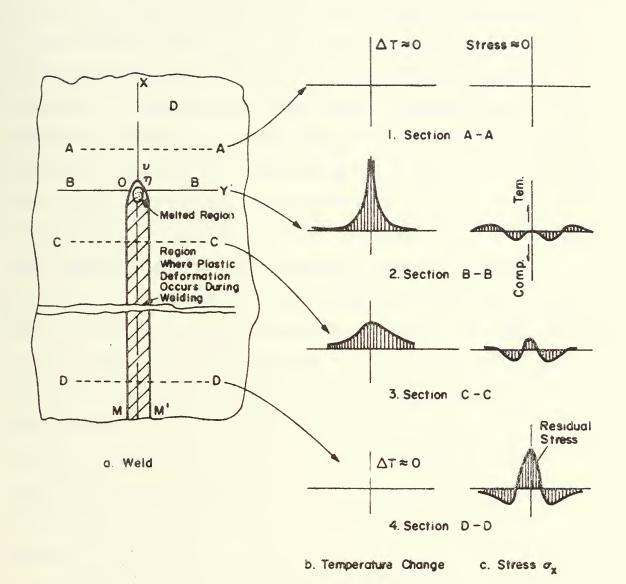


Figure 1. Schematic Representation of Changes of Temperature and Stresses

During Welding



Figure 1c shows the distribution along these sections of the x-direction stress, o. Stress in the y-direction, $\sigma_{_{\mathbf{V}}}$, and shear stress, $\tau_{_{\mathbf{X}\mathbf{V}}}$, also exist in a two dimensional stress field but are secondary and are neglected in this discussion. Along Section A-A, thermal stresses due to welding are essentially zero (Figure 1c-1). The stress distribution along Section B-B is shown in Figure 1c-2. In the area beneath the welding arc stresses are near zero because molten metal cannot support loads. Immediately outside the weld puddle, stresses are compressive because thermal expansion of these areas is restrained by surrounding areas that are heated to lower temperatures. Since the temperatures of the areas immediately adjacent to the puddle are quite high and the strength of the material is correspondingly low, stresses in these areas are as high as the yield strength and plastic straining occurs. Stresses in areas away from the weld are tensile and balance with the compressive stresses near the weld. In other words, $\int \sigma_{x} \cdot dy = 0$ across Section B-B.

The distribution along Section C-C is shown in Figure 1c-3. Here the weld metal and base metal regions near the weld are cooling and tend to shrink. This causes tensile stresses in these regions near the weld and compressive stresses in areas further away.

Figure 1c-4 shows the stress distribution along Section D-D. Continued cooling and shrinkage has left very high



tensile stresses in and near the weld, and offsetting compressive stresses across the rest of the section. This is the residual stress distribution after complete cool-down.

Note that the cross-hatched area, MM', in Figure la indicates the region where plastic deformation occurs during the welding thermal cycle. The region outside MM' remains elastic during the entire cycle.

C. Previous Investigations

In spite of an enormous research effort expended over the years, understanding and control of the complex mechanisms producing welding thermal strains have been elusive. pretive reviews by Kihara and Masubuchi provide an indication of the progress in the field as well as extensive bibliographies. 2,11 The closest approach to a break-through so far has been the development by several authors of computerized models of simplified welding theories. The Prokhorovs in Russia and Tall in this country have produced significant results in this area in the last few years. 12,13 In order to expand and apply the available knowledge, NASA's George C. Marshall Space Flight Center supported continuing studies at Battelle Memorial Institute and the Massachusetts Institute of Technology on a quantitative analysis of thermal stresses and metal movement during welding. The most important result to date has been the development by Masubuchi and others of a one dimensional computer model applicable to bead-on-plate and butt welds of thin plates. 14



While the use of high speed computers has led to impressive analytical progress, a distinct lack of complete and reliable experimental data has retarded further advances. Attempts to physically verify analytical results have been incomplete and often contradictory. The most common experimental techniques have involved some type of post-weld stress relaxation. Here information is gained by removing metal around a weld and observing the resulting strain changes in the specimen (by means of strain gages, X-rays, or photoelastic coatings, for example). The observed strains are then related to residual stresses by Hooke's law. 15 The results obtained in these experiments vary widely since straining is a strong function of the amount and distribution of metal removed -- a parameter which often varies from one investigation to the next. The most serious limitation, however, is the fact that these techniques record only the cummulative, residual effects of the weld process and provide no direct measurement of the transient stress-strain development.

There have been attempts to obtain dynamic as well as residual measurements of metal movement during welding, but until quite recently the results have been only qualitative and indirect. The use of laser interferometry has appeared promising but nothing has been published on it as yet. In 1964, R. E. Travis and others obtained some useful indirect data by cementing electric-resistance strain gages on a



C-shaped constraining bar and then depositing welds on small specimens clamped between the jaws of the bar. 16 Perhaps the first truly direct data on transient weld stresses were recorded by Wilson and Corderoy in Australia in 1967. 17 In this case, thermocouples and electric-resistance strain gages were cemented on large, one-inch thick steel plates. The gages were arranged to provide both transverse and longitudinal readings at various distances from the weld line. The transient stress-strain response of the plate was then recorded during single-pass butt welds. By comparing their results with Tall's theoretical analysis, 13 the authors were able to conclude that at least qualitative verification exists.

Transient data has also been obtained in Russia utilizing pneumatic tensile strain gages. Kasatkin and others measured the movement of a selected point in the weld heat-affected zone as up to four weld beads were deposited consecutively on a small 1/4 inch iron specimen. They confirmed the Wilson-Corderoy results as well as obtaining important information on multi-pass effects. In a later series of experiments these same investigators obtained longitudinal stress-strain measurements by placing pneumatic gages on a larger plate (4 x 24 inches) at various distances from a single-pass edge weld. Comparison with theoretical computations again produced reasonable agreement.

As part of the NASA study at M.I.T., Masubuchi and his co-workers attempted to verify their analytical results by



using electric-resistance strain gages to measure strain changes during bead-on-plate welding of 1/4-inch, 2219 aluminum plates. 14 Here, thermocouples and three-element strain rosettes were mounted on 18 by 30 inch plates in much the same manner as the Wilson-Corderoy experiments. Readings were taken during the passage of the welding arc and continued until complete cool-down of the specimen. The most important results of the investigation were as follows:

- 1. In general, longitudinal strains (along the axis of the weld) were predominant. Transverse and shear strains were of smaller magnitude except in the immediate area of the live welding arc. For this reason the one-dimensional computer predictions were essentially verified.
- Heat input significantly affected the extent of the tensile residual stress zone.
- 3. High compressive stresses occurred in areas ahead of the moving arc.

Concurrent with the NASA study, a similar investigation on 1/4-inch low carbon (mild) steel and HY-80 steel plates was undertaken by Klein and Maclin at the Portsmouth Naval Shipyard in New Hampshire. The results corraborated Masubuchi's aluminum experiments. (The Portsmouth data has been re-analyzed and appended to this report.)



D. Aim and Purpose of the Present Study

The scientific information gained in previous investigations has certainly been important. It now appears possible, however, to make more practical use of these experimental techniques. Some of the computer models, though admittedly simplified, might be proven applicable to production methods currently in operation. The aim of this study is to take a step in that direction. The need for such an effort in the shipbuilding industry has already been established. With this in mind, an approach to the problem of measuring dynamic thermal strains in production welds applicable to marine structures was initiated.

Of the techniques discussed previously, the use of electric-resistance thermocouples and three-element strain rosettes appeared most promising. This method allows for temperature compensation of the gages and also provides enough data to determine principle as well as longitudinal and transverse strains at selected points in the weldment. When applied to ship-production welds, however, a serious problem arises. Ship and submarine fabrication most often means relatively thick-section, multi-pass welds. A meaningful investigation of any scope would thus entail a large number of passes and therefore produce an enormous amount of raw data. Since no automatic data reduction system was reported in any of the previous investigations, the development of one became an immediate primary aim of this study.



It became apparent that once a strain measurement technique and a computer data analysis program were developed, several opportunities could be exploited to advance the state of the art. In addition to testing the practical application of current theoretical weld models, the effects of thin vs thick section plates could be examined, and the controversial subject of base-plate strength-effect explored. The latter problem, that of determining the level and distributions of stresses and strains in plates of increasing strength, has been the subject of considerable comment--especially since the introduction of ultra high-strength marine steels. Up to now, results of post-weld stress relaxation measurements have raised as many questions in this regard as they have answered.

In summary, the primary purpose of this investigation is to obtain transient and residual strain-temperature data on production-type steel weldments applicable to marine structures. Objectives coincident to the data collection and reduction are:

- to test the applicability of the NASA one-dimensional weld analyses to practical ship structural weldments.
- 2. to determine the effect of increasing base-plate strength on weld stress-strain distributions.
- 3. to determine the effect of welds on thin vs thick section plates



- 4. to provide information for the development of more advanced (or more practical) computer programs to calculate temperature, strain and distortion changes during welding
- 5. to provide an inexpensive computer program capable of translating recorded thermocouple and strain gage rosette outputs into accurate temperature and two-dimensional strain readings
- 6. to examine the reliability and accuracy of very high temperature (HT) strain gages mounted close to the weld line.



II PROCEDURES

A. Scope of the Research

A series of three experiments measuring strain and temperature changes during welding was performed. System models representing constrained butt joints typical of ship and submarine fabrication were constructed from rolled steel plates. The steels selected varied in strength from 80- to 180-ksi and were of grades either used or intended for use in marine structures. Welding procedures followed U. S. Navy specifications as closely as possible, consistant with the equipment available in the M.I.T. Materials Joining Laboratory.

The Portsmouth data appended to this study broadens the scope to include bead-on-plate welds of thin-section 30- and 80-ksi steels.

B. Selection of Parameters

The steels selected for this investigation were HY-80 (yield strength, 80 ksi), HY-130 (140 ksi), and an experimental maraging-type nickel steel strengthened to 180 ksi. HY-80 is a quenched-and-tempered steel and has been used extensively in modern submarine construction as well as other specialized marine applications. It derives its strength during the quenching process from the formation of highly strained bainite and martensite. Some of the strain



is relieved by tempering which provides toughness and ductility at the expense of a moderate decrease in strength. HY-130 is also a quenched-and-tempered steel with a microstructure of tempered bainite and martensite. It was developed expressly for submarine applications and was used to fabricate pressure hulls for the U. S. Navy's Deep Submergence Rescue Vehicle. It is the product of a highly sophisticated manufacturing process and represents the upper strength limit for quenchedand-tempered marine steels. The 180-ksi maraging steel represents the next generation of "Ultra-service" steels designed to provide the high strength-to-weight ratio required for deep submergence applications. Its additional strength results primarily from the precipitation of various intermetallic compounds during aging of the basic martensitic microstructure. Together with the low-strength mild steel used in the Portsmouth experiments, these materials cover the spectrum of modern hydrospace steels.

The plate thicknesses used in this study were determined by availability, ease of handling, and applicability to normal end use. End use dictates thick sections. Service thicknesses for high strength steels range from 1/2 to 3 inches. Sections much in excess of one inch, however, were deemed impractical for experimental purposes. The range of 3/4 to 1 1/4 inches was thus chosen as most representative of thick section characteristics. This range provides the heat flow characteristics, constraint, multiple passes, and joint geometry typical of



normal end use. The precise thickness of each specimen within this range was determined solely by availability.

The joint design used in this experiment (double-bevel with backing plate) was selected because it is fairly common for the thickness and process utilized. It allows welding from one side of the plate only--an important feature in view of the instrumentation attached to the plate.

The level of constraint was designed to model a submarine hull or bulkhead butt joint. The specimen was clamped
at its edges to a 1/2-inch mild steel bed plate which resists
deformation, but does not preclude it any more than a betweenframe span of shell plating.

The size of the test plates was set at a nominal 18 by 30 inches (after joint fit-up) to provide essentially steady state conditions at strain gage locations. The 180-ksi plate was considerably smaller simply because a larger piece was not available.

The weld process used was semi-automatic Gas Metal-Arc (GMA or MIG). This process is normally prescribed for the ultra-high-strength steels and is not uncommon with HY-80. It allows excellent control of weld variables, reduces operator error, and fosters repeatability. Preheating of joints was accomplished by acetylene torches because electric strip-heaters were unavailable.



C. Strain Measurement by Electric Resistance Strain Gages

The fundamental concept of strain gage operation is that certain conductors exhibit a change in electrical resistance with a change in strain. Gages designed according to this principle are attached to test materials whose strains are then monitored by measuring resistance variations across the gage. In the case of welding thermal strains, the observed resistance change, ΔR , is made up of:

$$\Delta R = \Delta R_1(\epsilon_e) + \Delta R_2(\epsilon_p) + \Delta R_3(\alpha T) + \Delta R_4(T)$$

where

- $\Delta R_1(\epsilon_e)$ = the resistance change corresponding to elastic mechanical strain, ϵ_e , from which stresses can be computed.
- $\Delta R_2(\varepsilon_p)$ = the resistance change corresponding to plastic mechanical strain, ε_p , if it exists.
- ΔR_3 (αT) = the resistance change corresponding to temperature induced thermal strain, αT .
- ΔR_4 (T) = the resistance change caused by thermo-electric effects in the gage itself.

While it is not presently possible to discriminate between the two mechanical strains, $\varepsilon_{\rm e}$ and $\varepsilon_{\rm p}$, $\Delta R_{\rm 3}(\alpha T)$ and $\Delta R_{\rm 4}(T)$ can be separated out by empirical calculation. For this purpose, a test gage of the type and lot used in the experiment is mounted on a small sample of the base plate. The sample is then heated at equilibrium until a curve of



"Apparent Strain" ($R_3 + R_4$) vs temperature is obtained for the operating temperature range. The gage readings recorded in the weld experiments can then be corrected by subtracting out the apparent strain value corresponding to temperatures observed at the gage location.

Strain gages manufactured in the form of rosettes provide as many as three independent readings in three directions at a single location. This is enough to completely describe the two dimensional strain state at that location. 15,21,22,23

D. Description of Apparatus

1. Test Plates. A description of the test specimens is summarized in Table I. Plate dimensions and gage locations refer to Figure 2. The arrangement of constraining clamps is shown in Figure 3. The room temperature material properties of the test plate are as follows:

Material	Tensile Strength psi	0.2% Yield Strength psi	Young's Modulus psi
Mild Steel	58,000	32,000	29.3 × 10 ⁶
ну-80	104,000	84,000	29.3×10^{6}
HY-130	147,000	156,000	28.5×10^{6}
180-ksi	182,000	205,000	27.5×10^{6}



TABLE I. TEST PLATE GEOMETRY AND SENSOR LOCATION

TEST PLAFE	NILL STREETS	4X=50*	nY-c0	HY-130	180-ks1
(עד) אַזַּסְעָקד	30	30	30	30	1.5
AILTH (in)	γ	প্	91	γ	91
THICKNESS (in)	0.25	0.25	0.75	0.75	1.0
BEVEL ANGLE	NONE	NC NE	°09	450	009
RCCI GAP (in)	NONE	NONE	3/16	3/16	3/16
BACKING PLAIR	Bowe	NORE.	1/4-in. HY-80	1/4-in. dY-80	1/4-in. dY-80
CCNSFRAINF	Packed	PACKED	ان المريدية المرادية	USAMBEI	ांच संशक्षा
SERSCR LUSAFICA ANJ CRIENTAFICA**	WELD LINE / 2.5" T A B C	WELD LINE 1 1 1 1 1 1 1 1 1	WELD EDGE	WELD EDGE	WELD EDGE

* These experiments were performed at Portsmouth. 20

** [*]emperature sensors; A-D-J-Strain Jare dosette blements. The fils steel plate has a lemp. Jensor and strain Rosette mounted on the back side of the plate, opposite the one-inch-from-weld line location.



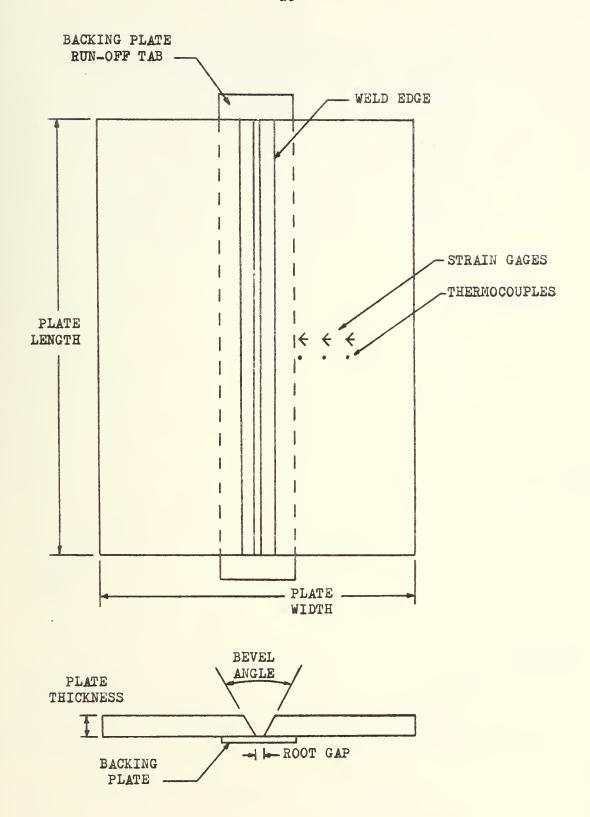


FIGURE 2. TEST PLATE AND JOINT GEOMETRY.



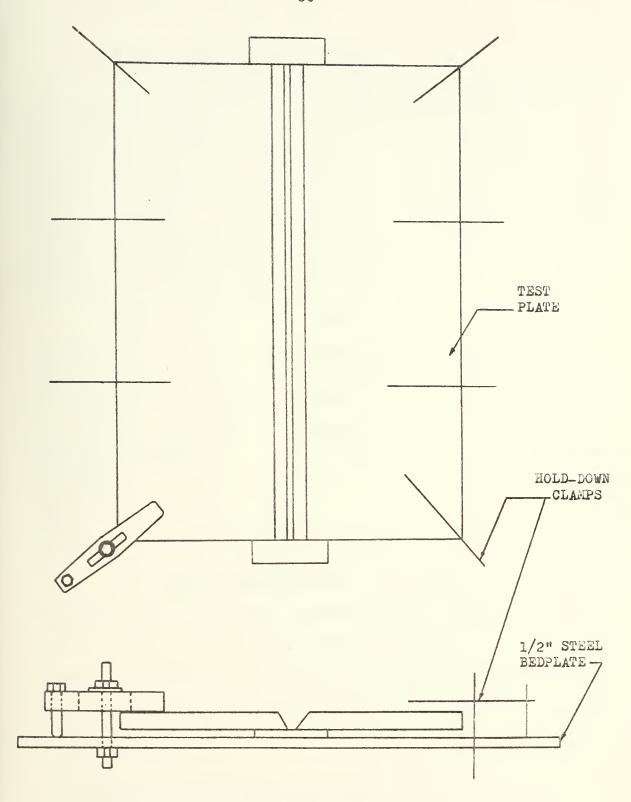


FIGURE 3. CONSTRAINING EQUIPMENT



2. Sensors and Instrumentation.

a. Strain Gages. Two types of gages were used in this investigation: SR-4 foil, 45°-rosettes; and high temperature, HT, free-filament gages. Only one set of HT gages was employed as a test of their applicability to welding experiments.* In this case three HT gages were applied in the same orientation as a 45°-rosette. All other gages were the SR-4 type. Gage properties:

Gage	SR-4	HT
Designation	FAER-25RB-12S6	HT-1212-5B
Manufacturer	BLH Electronics	BLH Electronics
Grid Length	1/4 inches	5/16 inches
Grid Width	.125 inches	3/32 inches
Temperature Range	-100 to +400 °F	-320 to +1200 °F
Resistance	120 ohms	120 ohms
Gage Factor	2.00	3.79
Cement	EPY-600	Rokide-BLH
Protective Covering	BLH Barrier-C	BLH Barrier-C

b. Temperature Sensors. All temperature sensors used were BLH Type GTM-CA (Chromel/Alumel) adhesive-bonded thermocouples. In the case of the HT gages, the thermocouple formed an integral part of one of the gages (an HT-1212-5A). In all other cases they were placed 1 1/4 inches to the left of the gages.**

^{*}HT gages were installed at the .55 inch-from-weld location on the 3/4-inch Hy-80 plate.

^{**}The Portsmouth experiments on mild steel and HY-80 utilized Micro-Measurements, Inc. equivalents to the BLH SR-4 and GTM-CA sensors. Alternative instrumentation and data-reduction techniques were used as required.²⁰



- Instrumentation. Strain gages were connected C. into a Potentiometric Circuit (Half-Wheatstone Bridge), balanced and calibrated as indicated schematically in Figure 4. Thermocouples were referenced to a 32° F ice-bath and calibrated as indicated in Figure 5. Both circuits were fed into a Honeywell continuous-recording, 12-channel Visicorder. When the raw data was actually read off the recorder tape, some traces were delayed or advanced with respect to others. This was done to correct for the finite difference in position along the weld line of the thermocouples and strain rosette elements (that is, if a thermocouple was 1 1/4 inches in front of its respective strain gage and the weld speed was .23 inches-per-second, the temperature readings were delayed 5.4 seconds with respect to the strain readings. This produces the effect of a simultaneous strain and temperature reading at the strain gage location). Timing was accomplished by means of an electric stop watch as well as a timer integral to the Visicorder.
- 3. Welding Equipment and Conditions. Welding conditions are summarized in Table II. The welding machine utilized was manufactured by the Linde Division of Union Carbide Corporation and consisted of a type HW-16 GMA torch, a SVI-300 power supply, and associated governor, carriage and wire feed mechanisms. Travel speed, arc voltage and amperage were preset before each pass. Arc length was adjustable during



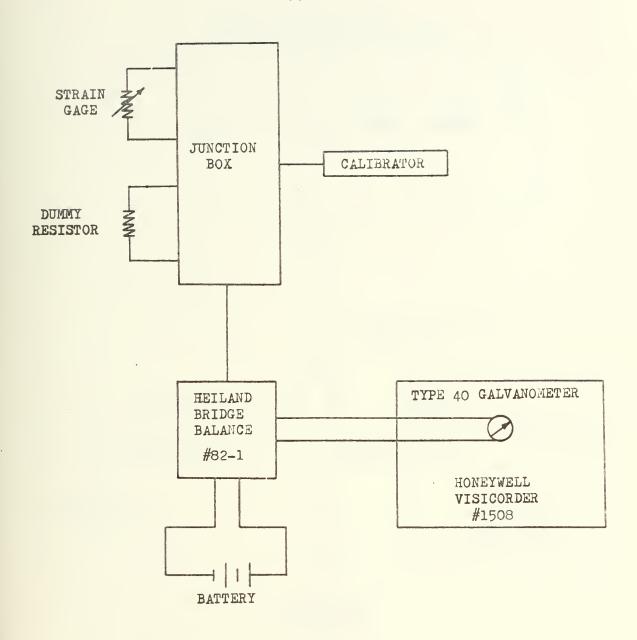


FIGURE 4. STRAIN GAGE INSTRUMENTATION CIRCUIT.

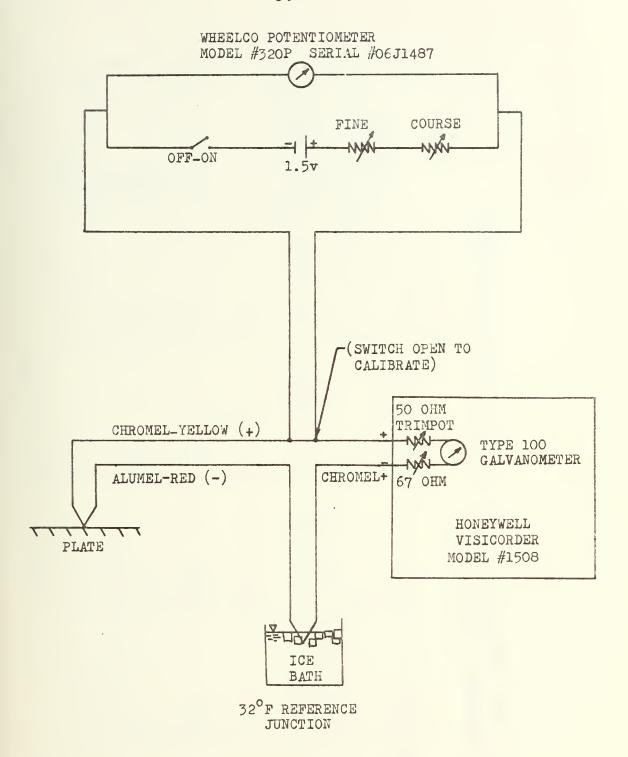


FIGURE 5. THERMOCOUPLE INSTRUMENTATION CIRCUIT.



TABLE II. WELDING CONDITIONS.

180-KSI	BUTT	GMA	28	DCRP	14	35	1/16" LINDE-140 1/16" LINDE-140	PURE ARGON	20	125-150 ⁰ F
HY-130	витт	GMA	28	DCRP	14	35	1/16" LINDE-140	PURE ARGON	8	125-150 ⁰ F
HY-80	BUTT	GMA	28	DCRP	15,20**	32,24**	1/16" AIRCO-632	PURE ARGON	18	125-150 ⁰ F
HY-80*	BEAD-0N-PLATE	GMA	30	DCRP	24	21	1/16" B-88	ARGON, 2% 02		70 ⁰ F
MILD STEEL*	BEAD-ON-PLATE	GMA	30	DCRP	24	21	1/16" B-88	ARGON, 2% 02		70 ⁰ F
TEST PLATE	WELD TYPE	PROCESS	ARC VOLTS	POLARITY	TRAVEL SPEED (IPM)	HEAT INPUT (KJOULES/IN)	FILLER WIRE	SHIELDING GAS	NO. PASSES	PRE-HEAT & INTERPASS TEMP. 70 ⁰ F

**TRAVEL SPEED CHANGED FROM 15 TO 20 IPM AFTER 3RD PASS TO IMPROVE WELD APPEARANCE. * EXPERIMENTS PERFORMED AT PORTSMOUTH. 20



the weld. Wire feed is a function of the other variables and was maintained by the machine automatically. Pre-heat was applied by acetylene torches using Linde size 30 tips. Care was taken to see that heat soaked in at least four to six inches on either side of the joint. Pre-heat and interpass temperatures were monitored by means of "Tempilstik" melting crayons as well as the installed thermocouples. Cooling between passes was aided by the application of wet rags well back from the joint. This should have approximated the heat absorption properties of a section of hull plating much larger than the 18-inch wide test specimen.

Figures 6 through 9 are photographs of the actual equipment set-up.

E. Experimental Procedures

The experimental operation is shown schematically in Figure 10. The test plate was instrumented, clamped into place and pre-heated. The welding machine was lined up with the joint and positioned over the run-off tab at the left end of the backing plate (shown in Figure 2). Welding speed, arc voltage and amperage were pre-set. The visicorder was actuated and an arc was struck on the backing plate. As the welding torch started moving down the plate, arc length was adjusted and the timer was started. The Visicorder output was marked when the arc passed the strain gage location. When the welding head reached the run-off tab at the right end of





FIGURE 6. OVERVIEW OF EXPERIMENTAL EQUIPMENT.

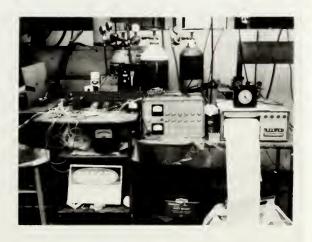


FIGURE 7. INSTRUMENTATION AND RECORDING EQUIPMENT.



FIGURE 8. 3/4-INCH HY-80 PLATE, INSTRUMENTED AND CLAMPED UNDER WELDING TORCH.



FIGURE 9. SENSOR INSTALLATION ON 180-KSI PLATE.



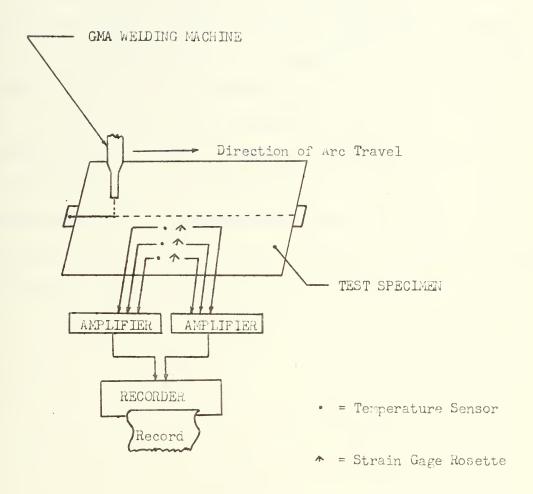


FIGURE 10. SCHEMATIC OF APPARATUS AND PROCEDURE.

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the plate, the arc was extinguished and the plate allowed to cool. The recorder continued to monitor the gages for approximately three minutes (or until conditions appeared stable). Readings were then taken periodically until the plate cooled to the required interpass temperature. After cooling, the welding head was re-aligned at the left end of the plate and the process repeated until the joint was completed. After the last pass, the plate was cooled to room temperature and the clamps released while the recorder was still monitoring. On two plates, HY-80 and 180-ksi, full cool-down occurred on an intermediate pass since the job covered more than one day's work. Pre-heat was again applied at the start of the next day.



III RESULTS

The results of this investigation consist of mechanical strain data recorded during welding of test specimens. The data is presented below in the form of plots of mechanical strain and temperature vs time. A more exact presentation in table form appears in Appendix B.

A. Presentation of Data

The plots presented in this section reflect the weld history of each of the test plates. Each plot records the strain and temperature variations during one weld pass and subsequent cool-down. Not every pass is recorded. Those selected generally include the first two, the last, and other passes considered typical of the developing trend. For each plate, the final readings on the last pass represent the cummulative strain state at the gage locations.

The plots are grouped according to the five test plates. The groups are preceded by schematic diagrams depicting the sequence and locations of the passes on the plate (Figures 11, 14, 17, 25, and 32). For comparison purposes, each group is also preceded by theoretical strain and temperature response curves obtained from the NASA computer model. The computer solution is one-dimensional and provides only longitudinal strains. Experimental data, however, is expressed in terms of the principle strains which result from any two-dimensional



strain state. For purposes of simplification, only the maximum of the two principle strains is shown.

The plots are constructed on semilog scales. The horizontal axis is a log scale of time, expressed in seconds (see Figure 12). Zero time is arbitrary, occurring some time after the arc has stabilized and is moving down the plate toward the gage location. The point at which the arc passes this location is marked ("ARC"). The limiting time on the scale (10,000 seconds) is not meant to be taken literally, but represents a time in excess of several hours by which the plate has reached ambient (residual) conditions.

The vertical axis is a linear scale of both temperature and mechanical strain. In order to fit neatly on the same scale, both quantities are expressed in unusual terms. Temperature is plotted in Degrees, Fahrenheit, divided by 1,000 and added to 1.0. Thus, 1.250 indicates a temperature of 250° F. Mechanical strain is expressed in microstrain divided by 1,000. (Microstrain equals 10⁻⁶ inches-per-inch elongation.) Thus, a value of -1.0 read off the strain scale would indicate a compressive strain of 1,000 microstrain (1,000 micro-inches-per-inch). A value of +1.0 would be a tensile strain of 1,000 micro-inches-per-inch.



TEST 1: 1/4" MILD STEEL

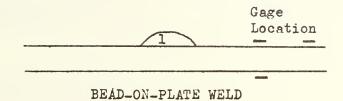


FIGURE 11. WELDING PASS SEQUENCE.

SCALES UTILIZED IN PLOTS:

1. Horizontal.

Time = Seconds

Temperature =
$$\frac{o_F}{1,000} + 1.0$$

Mech. Strain = $\frac{in/in \times 10^{-6}}{1,000} = \frac{microstrain}{1,000}$



TEST 1: 1/4" MILD STEEL

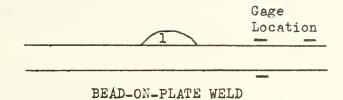


FIGURE 11. WELDING PASS SEQUENCE.

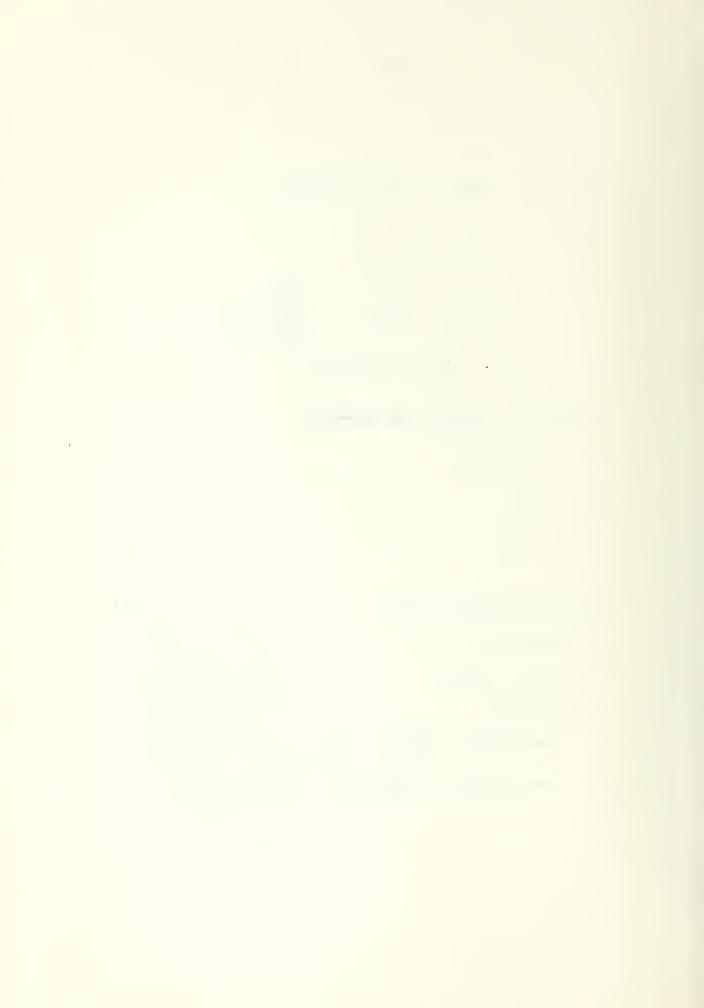
SCALES UTILIZED IN PLOTS:

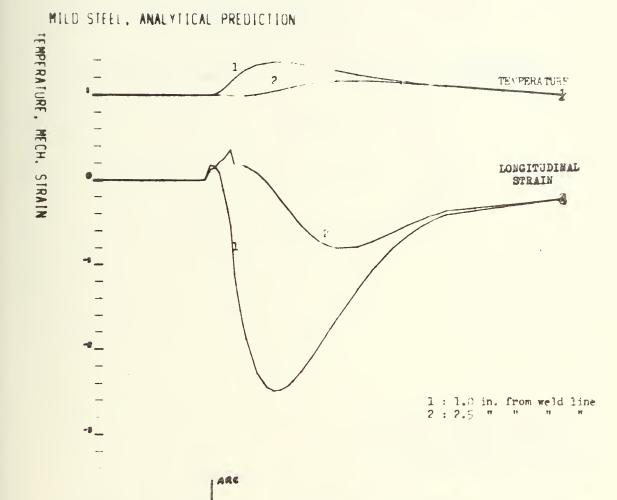
1. Horizontal.

Time = Seconds

Temperature =
$$\frac{o_F}{1,000} + 1.0$$

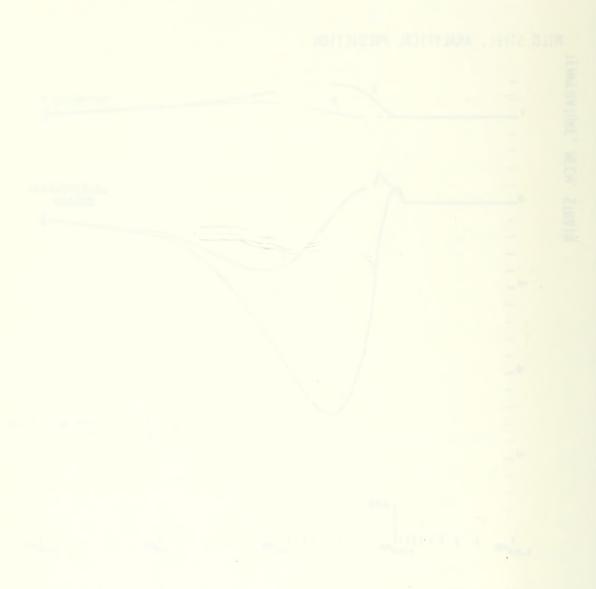
Mech. Strain = $\frac{in/in \times 10^{-6}}{1,000} = \frac{microstrain}{1,000}$



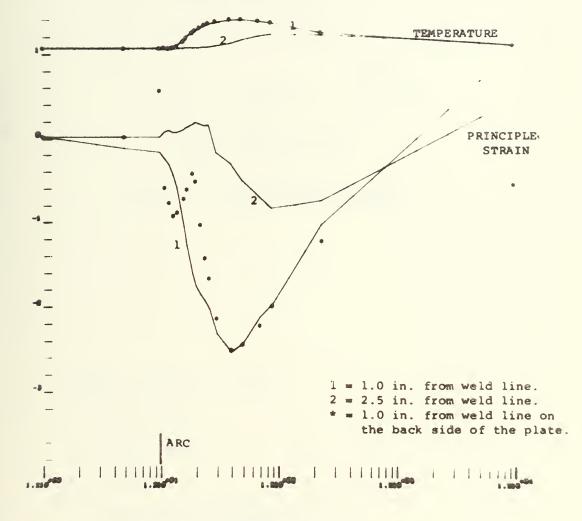


TIME IN ECONDS

FIGURE 12.



1/4 IN. MILD STEEL, EXPERIMENTAL RESULTS



TIME IN SECONDS

FIGURE 13.



TEST 2: 1/4" HY-80 STEEL

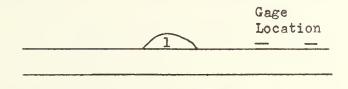


FIGURE 14. WELDING PASS SEQUENCE.

BEAD-ON-PLATE WELD

SCALES UTILIZED IN PLOTS:

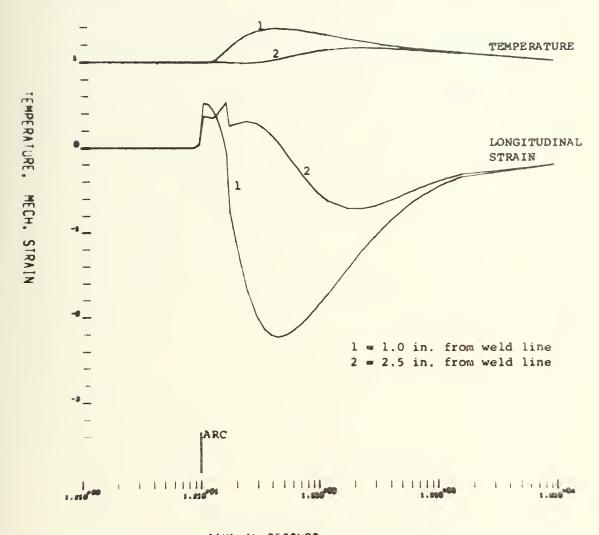
1. Horizontal.

Time = Seconds

Temperature =
$$\frac{o_F}{1,000}$$
 + 1.0
Mech. Strain = $\frac{in/in \times 10^{-6}}{1,000}$ = $\frac{microstrain}{1,000}$



1/4 IN. HY-80. ANALYTICAL PREDICTION



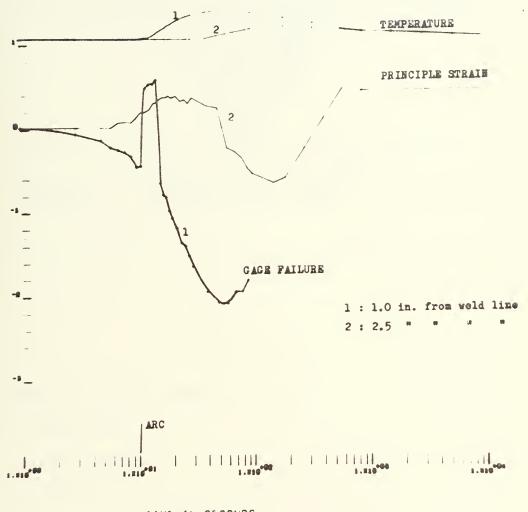
TIME IN SECONDS

FIGURE 15.

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: 4 IN. -Y 80. EXPERIMENTAL RESULTS



TIME IN SECONDS

FIGURE 16.



TEST 3: 3/4" HY-80 STEEL

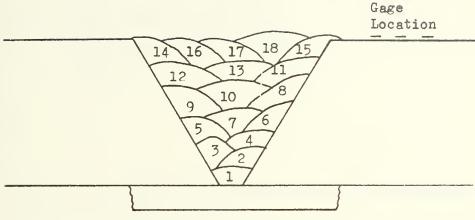


FIGURE 17. SEQUENCE OF WELD PASSES

SCALES UTILIZED IN PLOTS:

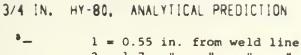
1. Horizontal.

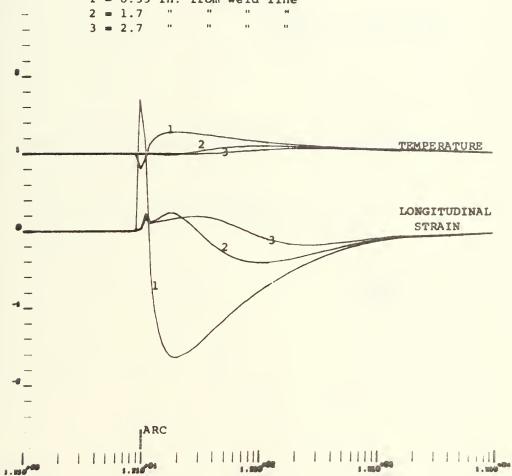
Time = Seconds

Temperature =
$$\frac{o_F}{1,000}$$
 + 1.0
Mech. Strain = $\frac{in/in \times 10^{-6}}{1,000}$ = $\frac{microstrain}{1,000}$







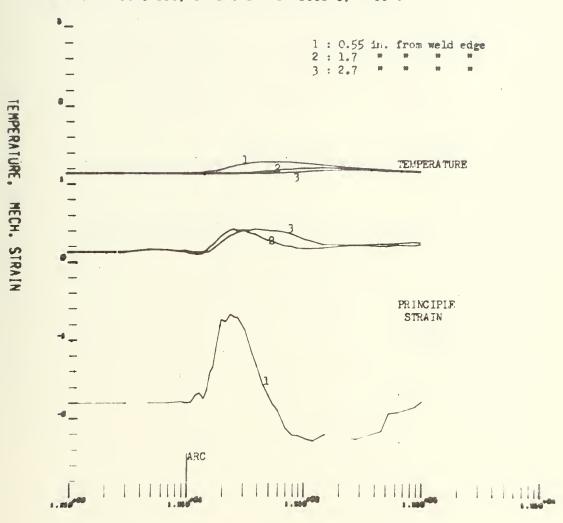


TIME IN SECONDS

FIGURE 18.





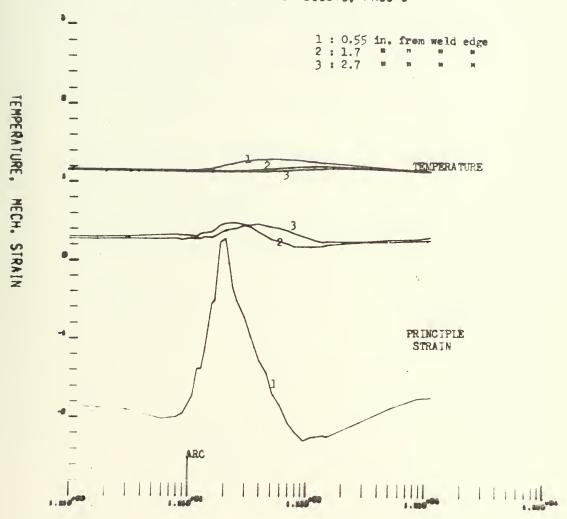


TIME IN SECONDS

FIGURE 19.



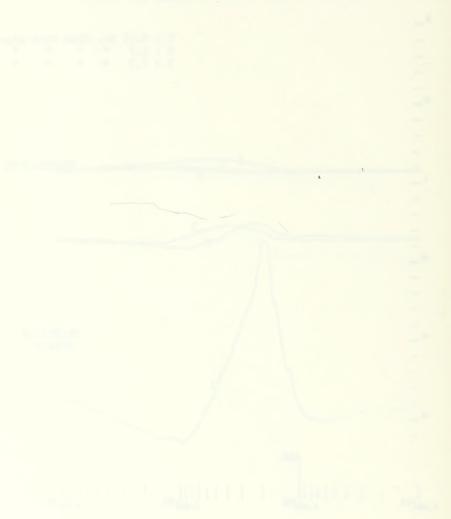




TIME IN SECONDS

FIGURE 20.

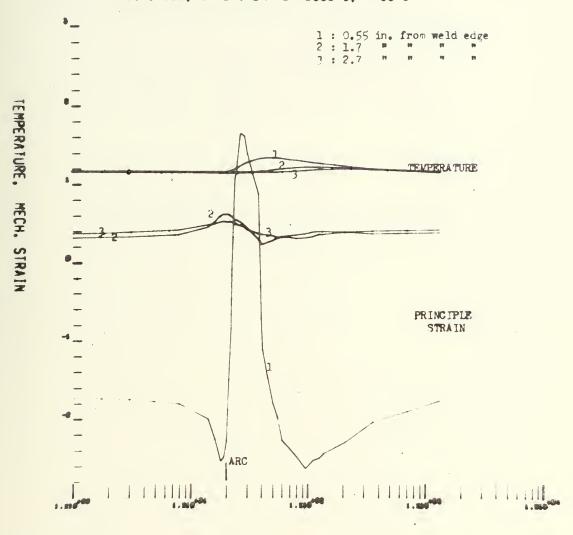




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108 (100)

3/4 IN. HY-80 STEEL, EXPERIMENTAL RESULTS. PASS 6



TIME IN SECONDS

FIGURE 21.

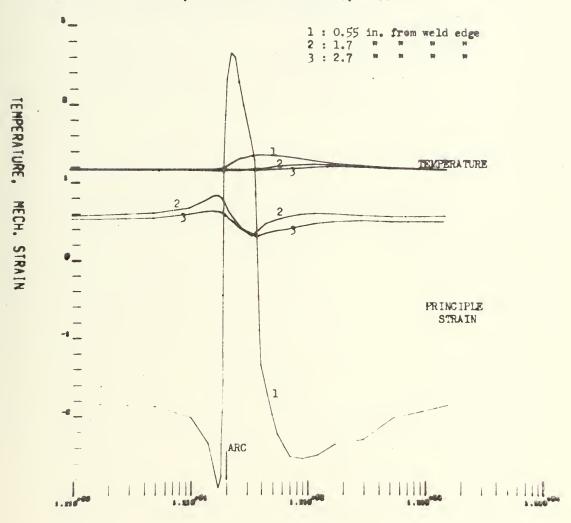




Total or and

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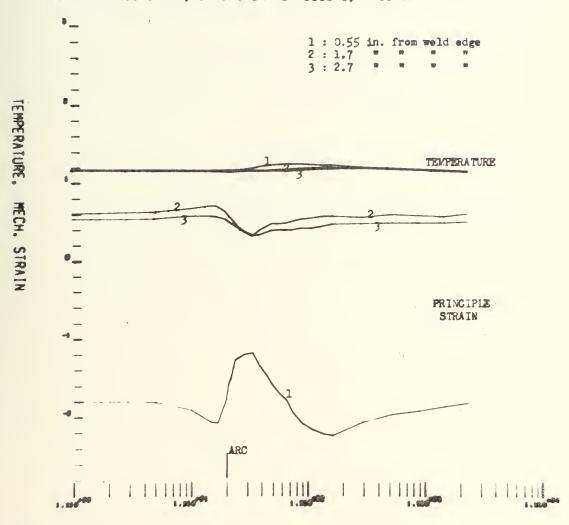


TIME IN SECONDS

FIGURE 22.





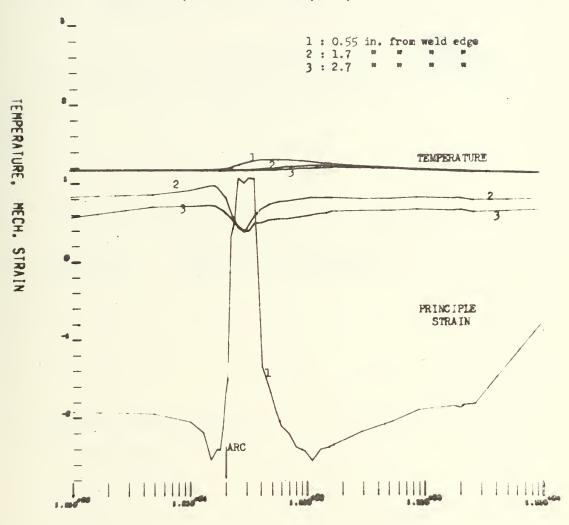


TIME IN SECONDS

FIGURE 23.







TIME IN SECONDS

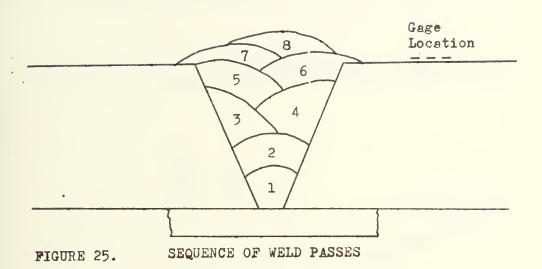
FIGURE 24.

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The Spinster

TEST 4: HY-130 STEEL



SCALES UTILIZED IN PLOTS:

1. Horizontal.

Time = Seconds

2. Vertical.

Temperature =
$$\frac{o_F}{1,000} + 1.0$$

Mech. Strain = $\frac{in/in \times 10^{-6}}{1,000} = \frac{microstrain}{1,000}$

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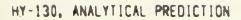
Larcontrick ...

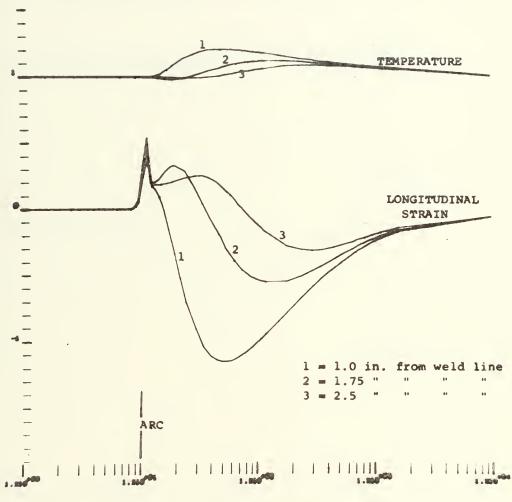
chromet a sure

January Verticals.

OCC., Stands of Lines of Lines

TEMPERATURE, MECH. STRAIN



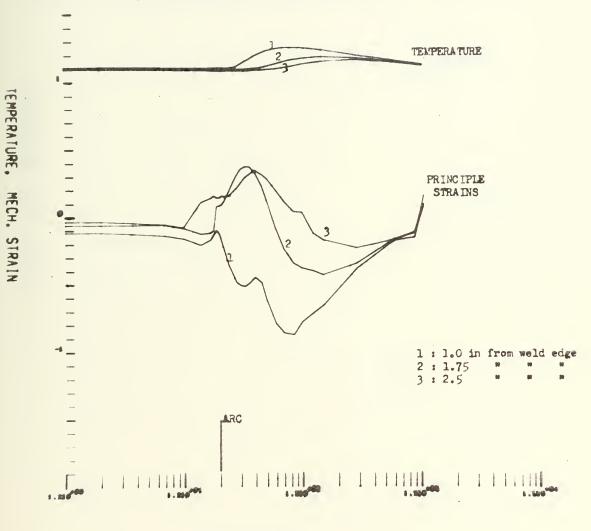


TIME IN SECONDS

FIGURE 26.



3/4 IN. HY-130 STEEL, EXPERIMENTAL RESULTS, PASS 1

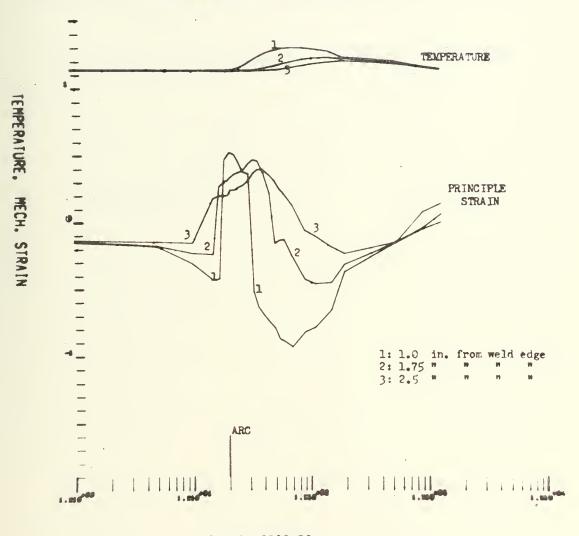


TIME IN SECONDS

FIGURE 27.



3/4 IN. HY-130. EXPERIMENTAL RESULTS. PASS 2

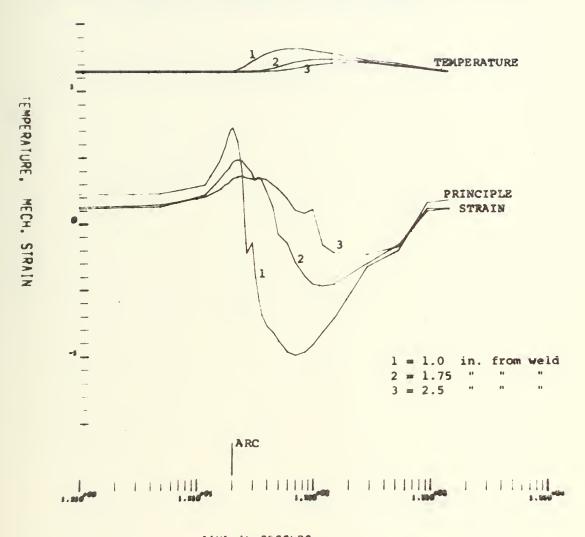


TIME IN SECONDS

FIGURE 28.



3/4 IN. HY-130 STEEL, EXPERIMENTAL RESULTS, PASS 4

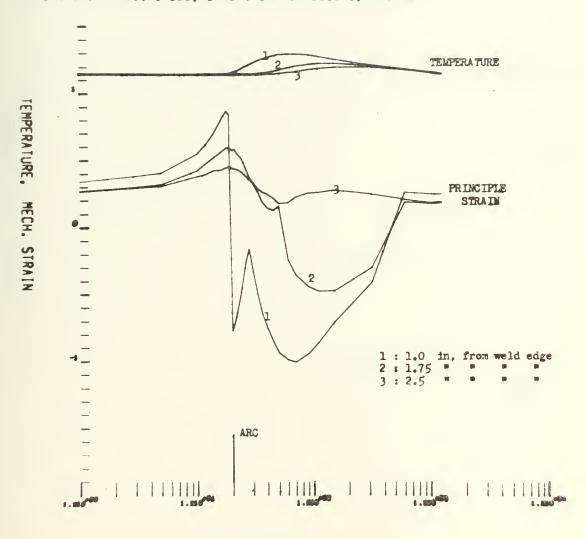


TIME IN SECONDS

FIGURE 29.



3/4 IN. HY-130 STEEL, EXPERIMENTAL RESULTS, PASS 6



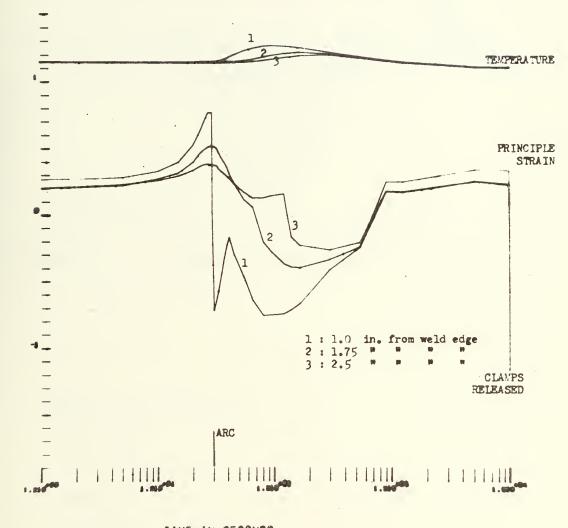
TIME IN SECONDS

FIGURE 30.



3/4 IN. HY-130 STEEL, EXPERIMENTAL RESULTS, PASS 8

TEMPERATURE, MECH. STRAIN



TIME IN SECONDS

FIGURE 31.



TEST 5: 180-ksi STEEL

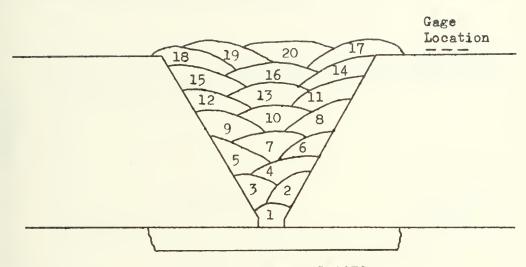


FIGURE 32. SEQUENCE OF WELD PASSES

SCALES UTILIZED IN PLOTS:

1. Horizontal.

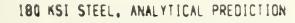
Time = Seconds

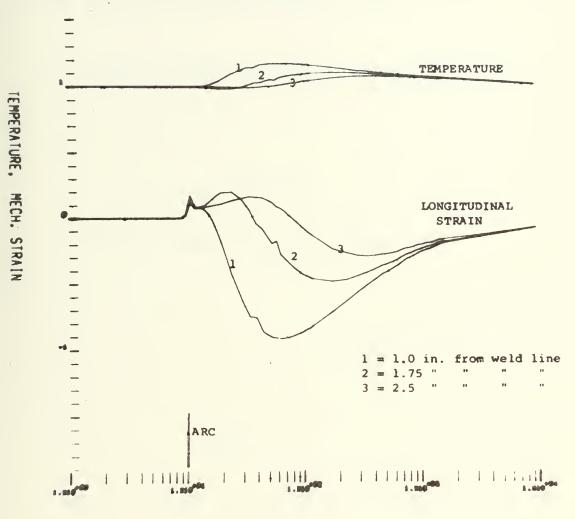
2. Vertical.

Temperature =
$$\frac{o_F}{1,000} + 1.0$$

Mech. Strain = $\frac{in/in \times 10^{-6}}{1,000} = \frac{microstrain}{1,000}$



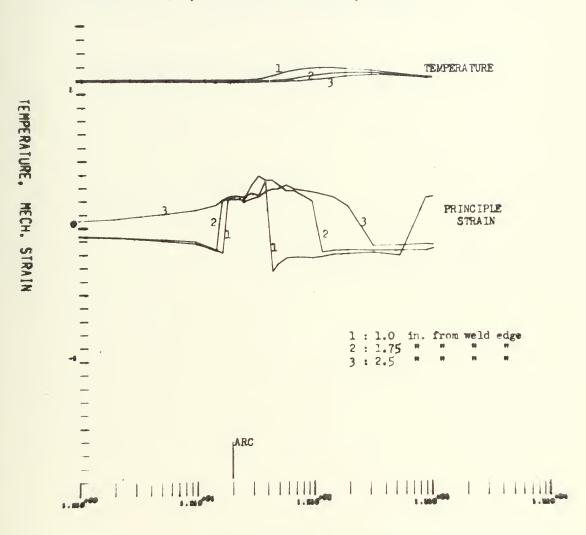




TIME IN SECONDS

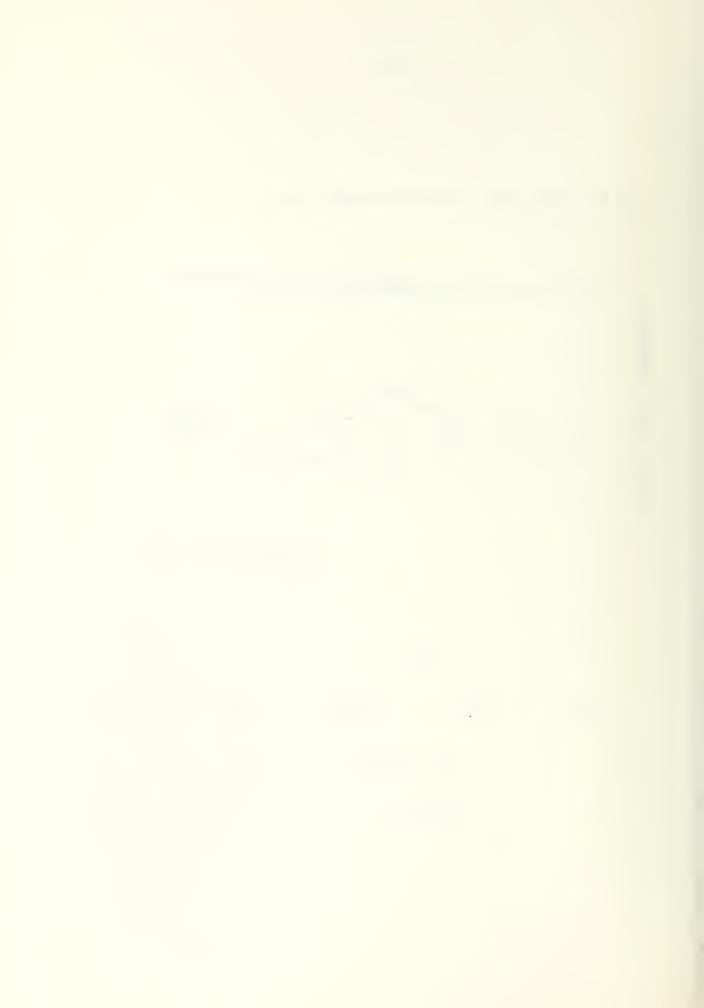
FIGURE 33.



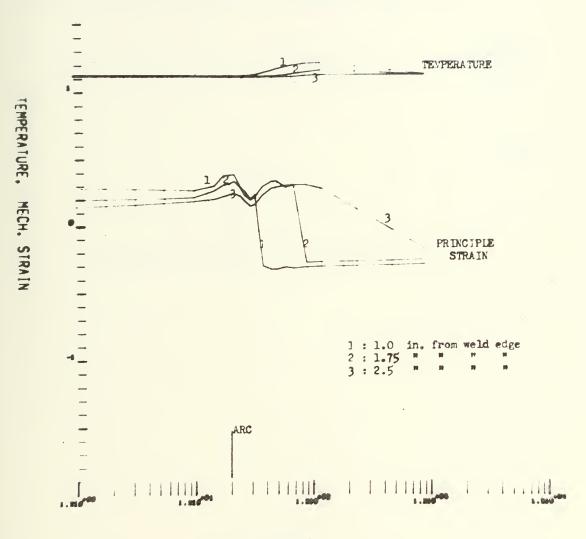


TIME IN SECONDS

FIGURE 34.



1.0 IN. 180-KSI STEEL, EXPERIMENTAL RESULTS, PASS 2

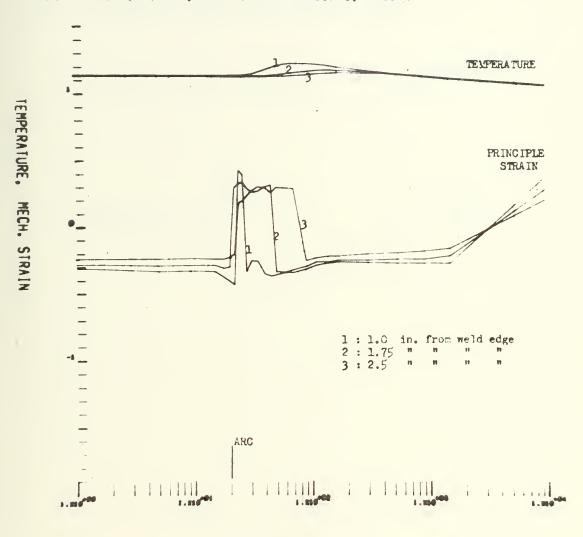


TIME IN SECONDS

FIGURE 35.

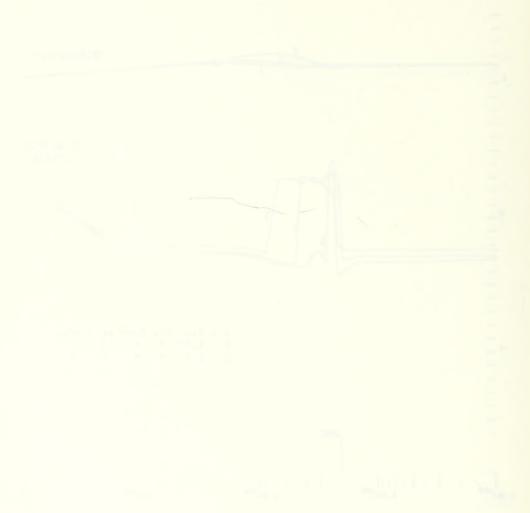
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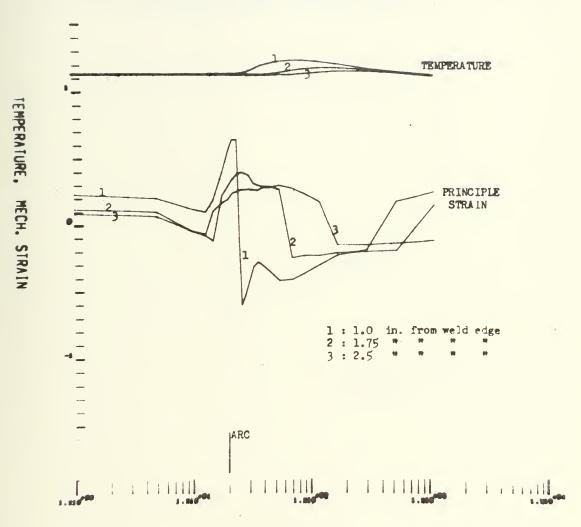
TIME IN SECONDS

FIGURE 36.



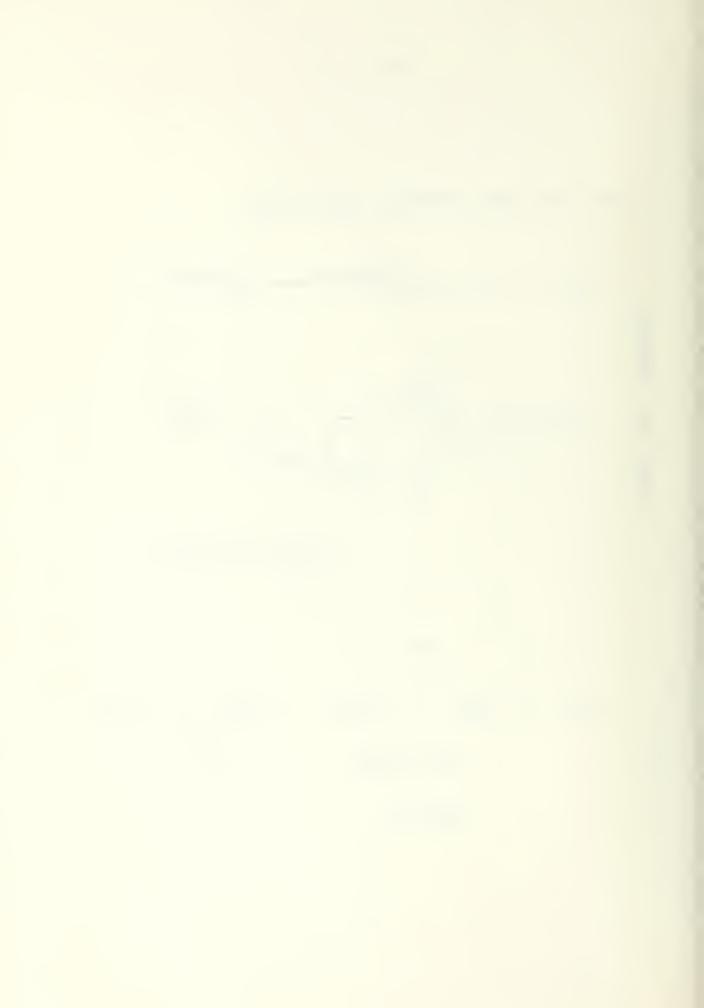
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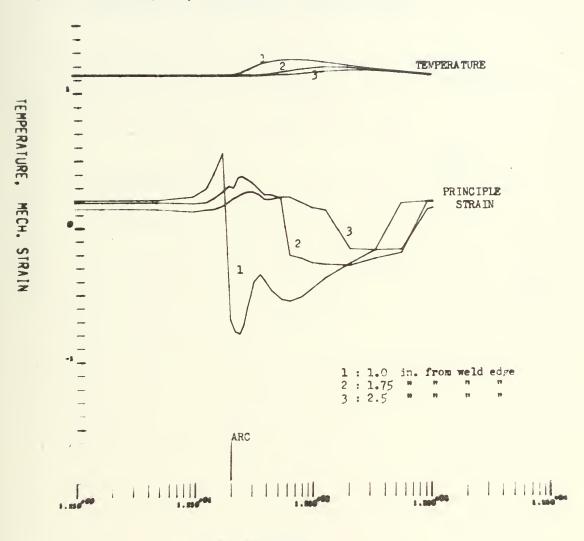
. NE BEHOVE



TIME IN SECONDS

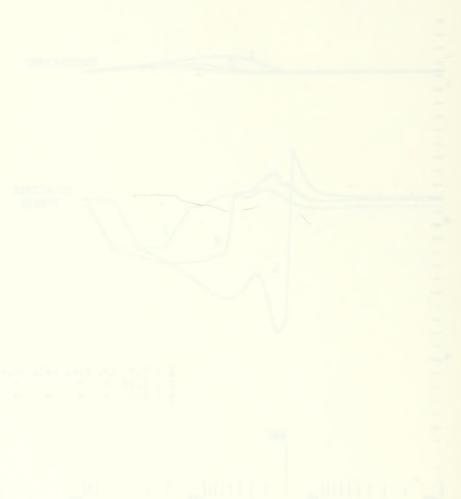
FIGURE 37.



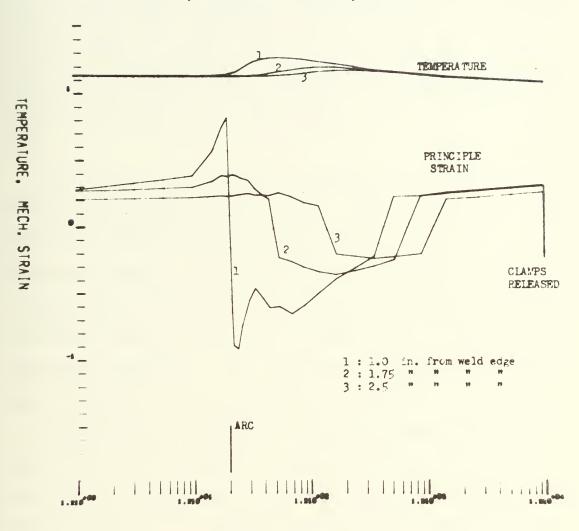


TIME IN SECONDS

FIGURE 38.



TIPE IN SECONOS-



TIME IN SECONDS

FIGURE 39.



B. Observations

The first two groups of plots show the results of the bead-on-plate welds performed at Portsmouth on 1/4-inch low carbon (mild) steel and HY-80. Figures 12 and 13 refer to the mild steel; Figures 14 and 15 refer to HY-80. On the HY-80 plate, a gage failure (shorted lead wire) occurred at the one-inch-from-weld-line location, 90.6 seconds into the run.

The third group of plots (beginning with Figure 18) refers to the 3/4-inch HY-80 plate. Weld quality for this particular specimen was impaired somewhat by a slightly excessive arc length. The arc wavered from side to side, shedding small vortices in the puddle in its wake. Although subsequent passes filled most of these voids, some porosity undoubtedly remained. The effect of these defects on the strain history is not considered significant.

The fourth set of results (beginning with Figure 27) refers to the HY-130 plate. On the first pass, several longitudinal cracks (1/4 ~ 1/2 inch long) were observed. The probable cause of the cracking was excessive constraint imposed by the 45° bevel angle. Cracking was not observed on subsequent passes and the effects of first-pass defects diminish rapidly with increasing weld metal deposition. Some porosity also occurred near the gage location in the sixth and eighth passes. Probable cause: contamination of the weld puddle by the gage protective coating. After final



cool-down on the last pass, the constraining clamps were released and another set of readings were taken (Figure 31).

The fifth set of plots refers to the 180-ksi plate.

While this specimen was only 15 inches long, the weld appearance was excellent through all passes. On the last pass

(Pass 20), a particle of hot spatter fell on the thermocouple leads and burned through them. Data was thus unusable for the run itself, but the leads were repaired in time to take cooldown readings. The readings were found to be identical to the Pass 17 values at time 1500 seconds, so the residual and "clamps-released" conditions were plotted at the end of Pass 17.

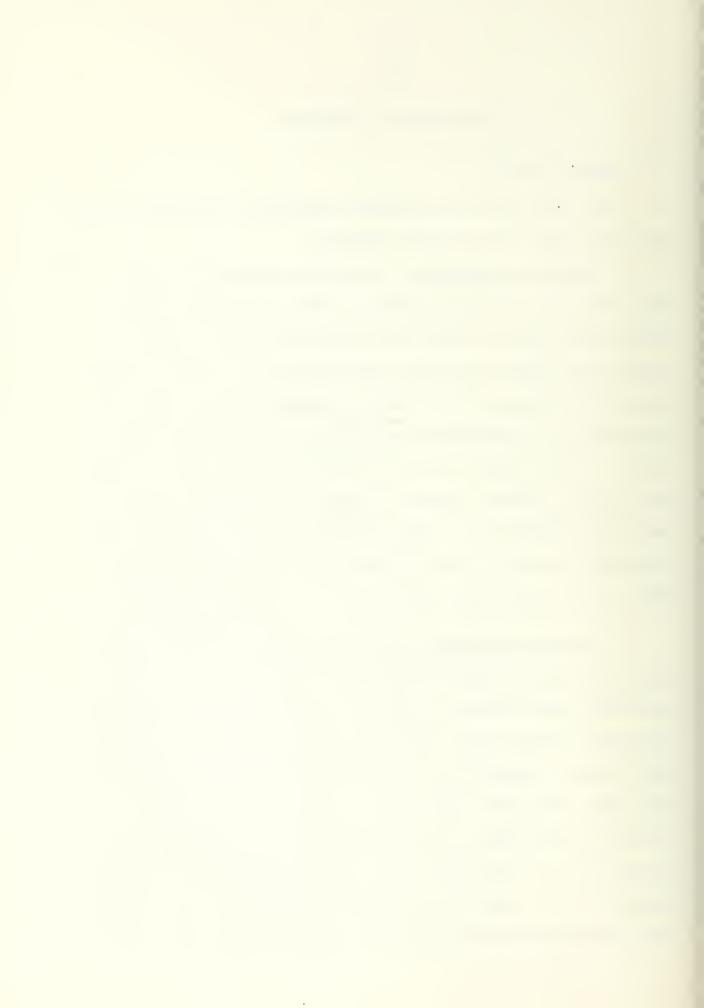


IV DISCUSSION OF RESULTS

A. General Trends

The variation of experimental parameters discussed earlier produced several discernable effects:

- 1. Effect of Preheat. Localized preheating of constrained plates imposed generally minor mechanical strain changes in areas an inch or more from the joint. These changes are reflected in the time-one-second values of strain plotted in Figures 19, 27, and 34. Magnitudes are too small in relation to experimental accuracy to indicate any clear trend. In the case of the .55-inch location on the 3/4-inch HY-80 plate, preheat imposed a highly compressive strain indication (Figure 19). This indication is viewed with some suspicion, however, since it was registered on HT gages.
- 2. Section Thickness and Multipass Effects. Comparison of thin-section, bead-on-plate welds with thick-section, multipass welds reveals a definite trend. The strain response of thicker plates does not develop into the clearly discernable pattern observed on thin sections until several passes have been deposited. For the HY-130 plate, the pattern begins to take shape in the fourth pass (Figure 29); for 180-ksi, it is the eighth pass (Figure 37). The slow development of this pattern is undoubtedly caused by the relatively long distance between the early passes and the gage locations.



As shown in Figure 17, the gages were placed on the top surface of the thick plates near the edge of the bevelled joint. As weld metal fills the joint openning, successive passes are deposited closer to the gages and thus produce greater effects by reason of their proximity. Looking beyond proximity variations, section thickness effect can be assessed by comparing the strain response of the 1/4-inch HY-80 plate tested in Portsmouth with that of the 3/4-inch HY-80 plate welded at M.I.T. Passes 11 and 18 on the 3/4-inch plate (Figures 22 and 24) were deposited at the same distance from their respective 2.5-inch gage locations as the single pass on the 1/4-inch plate (Figure 16). Both passes on the 3/4-inch plate produced smaller responses at the gage than was measured on the 1/4-inch plate. These results are consistant with the theoretical predictions plotted in Figures 14 and 18. The larger mass of metal in the thick section distributes and dissipates arc heat more readily and also provides greater constraint, both of which limit metal movement.

The effect of multiple passes recorded in this investigation is obscured by the proximity variations. Residual strains do appear to accumulate in the early passes (that is, the strain state reached by the last pass becomes the starting point for the next pass which then reaches a still higher residual strain state). The last few passes on each plate, however, show little or no cummulative trend.



Figure 40, for example, shows passes 4, 6, and 8 on the HY-130 plate (all deposited approximately the same distance from the gage locations). There is essentially no difference in the response of the plate to these passes. This is not inconsistant with the findings of previous investigators. Kasatkin found that on small specimens, permanent strains immediately under the weld line increased markedly during four passes of a tungsten arc. 18 As indicated in Figure 41, he also found that the direction of arc travel had a significant effect on the residual strain state. Kihara and Masubuchi measured transverse shrinkage on welds of more than four passes and found that the response levels off logarithmically during later passes (Figure 42). 24 appears reasonable to infer, therefore, that the principle strains accumulating during multi-pass welding also build up logarithmically, with the greatest increase in residual strain occurring in the early passes.

3. Effect of Plate Strength. As the strength level of the test plates increased from 30 to 180 ksi, the magnitude of both transient and residual welding strains decreased. At the one-inch-from-weld location, the transient response of the higher strength steels is noticeably less than that of the low carbon (mild) steel or even HY-80. To obtain a quantitative measure of this trend, the maximum transient strain change recorded during any pass on a plate was plotted vs base plate yield strength (Figure 43). The results indicate



HY-130 STEEL, EXPERIMENTAL RESULTS

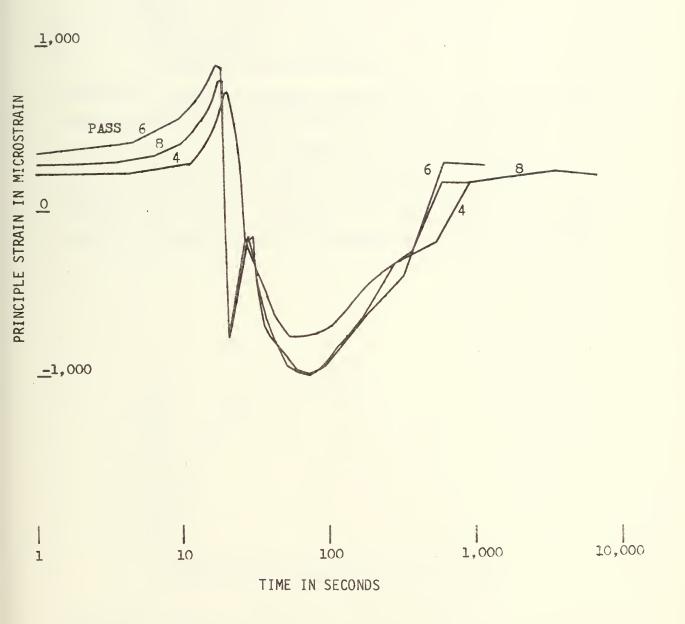


FIGURE 40. MULTI-PASS EFFECT. COMPARISON OF PRINCIPLE STRAIN RESPONSE DURING PASSES 4, 6, AND 8. (STRAINS MEASURED ONE INCH FROM THE WELD LINE.)



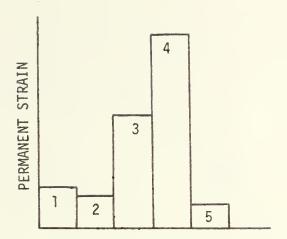


FIGURE 41. DIAGRAM OF PERMANENT MOVEMENTS OF A POINT WHEN SILICON IRON IS WELDED BY DIFFERENT VARIATIONS OF MULTI-PASS WELDING:

1. SINGLE-PASS; 2. TWO-PASS WELDING IN DIFFERENT DIRECTIONS; THE FIRST BEAD COOLED BEFORE DEPOSITING THE SECOND; 3. THREE-PASS WELDING IN ONE DIRECTION, WITH EACH BEAD COOLED BEFORE DEPOSITING THE NEXT; 4. THE SAME, NO COOLING; 5. FOUR-PASS CONTINUOUS WELDING WITH THE BEADS DEPOSITED IN ALTERNATE DIRECTIONS. (KASATKIN)

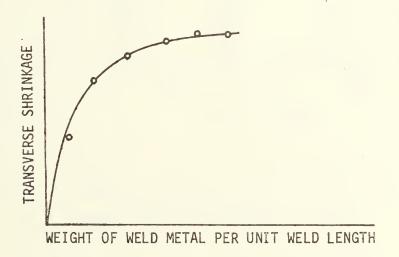


FIGURE 42. INCREASE IN TRANSVERSE SHRINKAGE DURING MULTI-PASS WELDING OF A BUTT JOINT. (KIHARA AND MASUBUCHI)



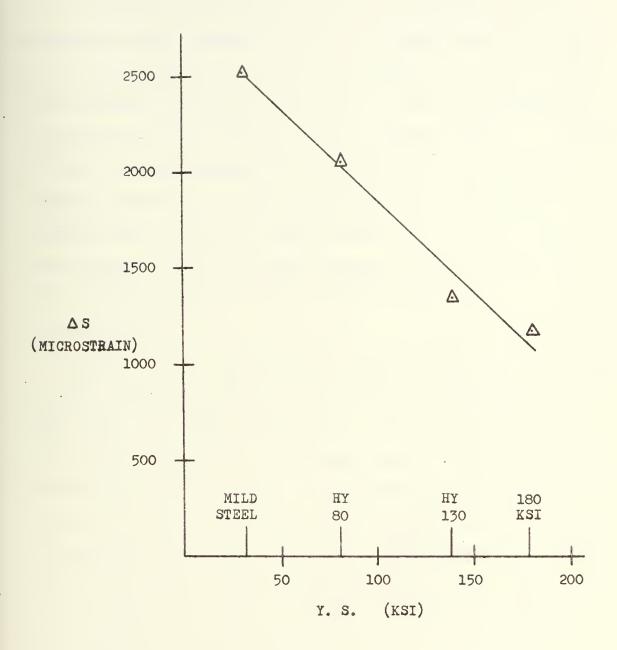


FIGURE 43. CHANGE IN WELDING MECHANICAL STRAIN (Δ S) vs.

BASE PLATE YIELD STRENGTH (Y. S.)



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that the strain response is roughly proportional to the inverse of plate strength. This can be explained by noting that of the parameters directly affecting weld strain, only yield strength changed significantly in these experiments.

(The same can also be said of most production welds.) Young's modulus, thermal expansion and conductivity coefficients, density, and heat-input-per-square-inch all varied only slightly while strength increased 600%. As a result, only a very narrow zone on the high strength steels yields plastically and the strains observed outside that zone are proportionately small.

Because of the lower strain response, the data describing the early passes on the 180-ksi plate are misleading. In these first few passes (Figures 34 - 37), the strain level was too low to show any predominance among longitudinal, transverse and shear strains. Consequently, the two principle strains, oriented 90° to each other and opposite in sign, were of comparable magnitude. Since only the largest of these two strains is plotted, abrupt changes show up in the curves when one principle strain edges the other. The strain state itself changes much more gradually.

Both of the two highest strength steels (HY-130 and 180-ksi) displayed an unusual phenomenon in the later passes. In Figures 29 - 31 and 37 - 39, a secondary tensile peak was observed in the strain response a few seconds after the arc had passed. Since there is no evidence of this response in



any of the lower strength steels or in the aluminum plates tested by Masubuchi and Arita, ¹⁴ the phenomenon is probably a material characteristic. The time-temperature history of the arc passage points to a possible phase transformation or precipitation reaction in the immediate area of the weld as the probable cause of the second peak. The transformation from Austenite to Bainite or Martensite, as discussed in a previous section, might cause a sudden compressive strain in the weld area itself and a corresponding tensile strain in surrounding areas.

4. Correlation between Principle and Longitudinal
Strains. Figures 44 - 46 indicate the correlation between
principle and longitudinal strains. As mentioned previously,
relatively low strain levels at the beginning and end of each
pass produced less predominance on the part of the longitudinal strains and thus less correlation with the principle
strains during these periods. Correlation was also diminished
at the point in time when the arc passed the gage locationdue to presence of high transverse and shear strains. All
other observations showed principle and longitudinal strains
to be quite close.

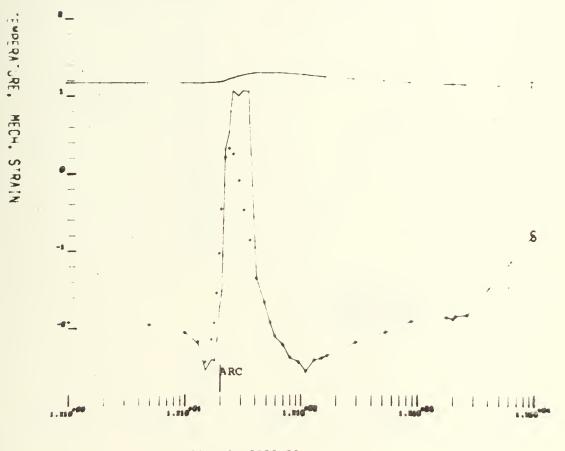
B. Comparison of Experimental Results with Theoretical Predictions

The NASA computer programs used in this investigation provide a one-dimensional solution to a simple, single-pass,



3 4 IN. -Y-80, PRINCIPLE & LONGITUDINAL STRAINS (PASS 18)

```
T = TEMPERATURE, 0.55 in. from weld edge
S = PRIN. STRAIN, " " " "
+ = LONG. STRAIN, " " " "
```



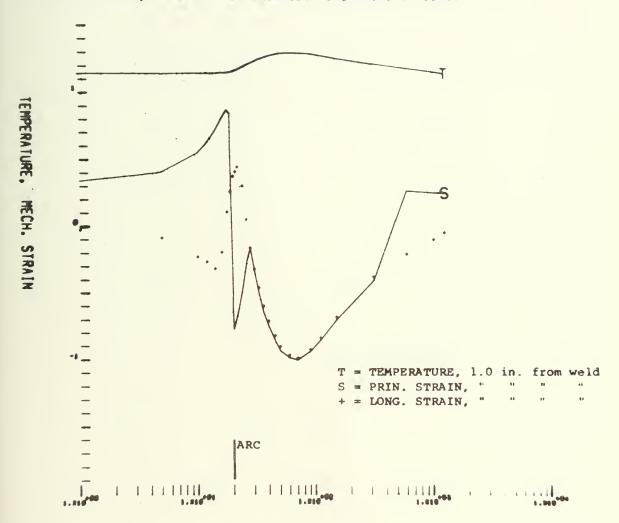
TIME IN SECONDS

FIGURE 44.

TOT 28A97 BRINGS AND AND AND STRAING TORS TOT

20000332 V INC.

AA SHURST



TIME IN SECONDS

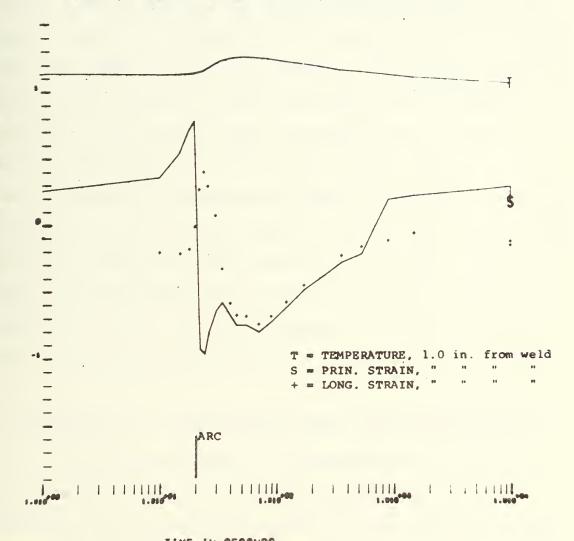
FIGURE 45.





POWERS PL BOTT

1.0 IN. 180-KSI, PRINCIPLE & LONGITUDINAL STRAINS (PASS 17/20)



TIME IN SECONDS

FIGURE 46.



thin-section weld model. The correlation between principle and longitudinal strains just discussed and the relatively small deviation between thin and thick section effects provide a key to the applicability of the programs to more complex weldments. In general, the predictions were accurate as to the trend of the strain response, the maximum value of strain imposed, and the effects of significant parameter variations. The programs did not predict the secondary tensile peaks observed in the high strength steels nor did they anticipate the cummulative effects of multipass welding. (Correlation with the later passes would be excellent if the analytical prediction were displaced so that its initial strain reading matched that of the experimental curve.) Computer solutions were also inaccurate in the immediate area of the welding arc itself.

C. Accuracy of the Experimental Model and Instrumentation

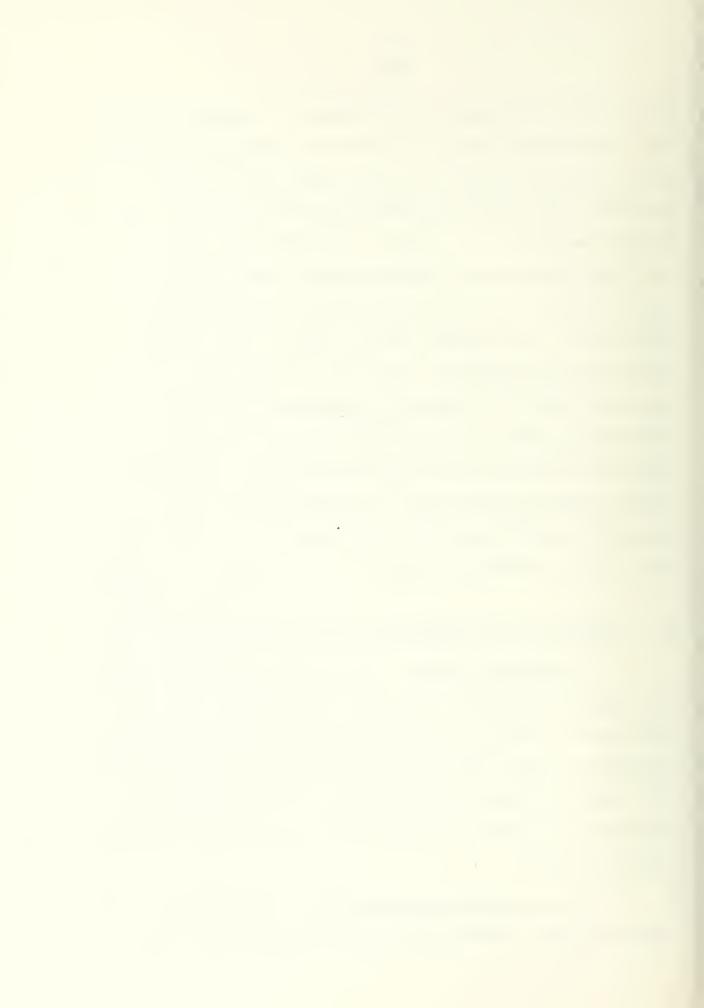
- 1. The Physical Model. As mentioned in the discussion of parameter selection, the plate geometry, the level of constraint, and the welding procedures are considered representative of ship fabrication processes. The small size of the 180-ksi specimen did not appear detrimental when its response was compared to that of the larger plates of other strength levels.
- 2. <u>Data Reduction Calculations</u>. The accuracy of the data reduction technique discussed in Section II-C and



programed in Appendix A rests primarily on one crucial assumption: that of "Linear Superposition." It is assumed that the effects of mechanical strains, temperature induced thermal strains and gage thermo-electric effects do not interact with each other and can be added or subtracted linearly. This approximation is valid only when the mechanical strains are large in relation to the thermal effects.

3. <u>Instrumentation</u>. Two key factors affect the accuracy of the instrumentation: the size of the sensing elements and their thermal response characteristics. The largest dimension of any single sensor element is 0.25 inches. This is small compared to the other length dimensions involved in the geometry. The area covered by the entire gage rosette is large, but this has been corrected by time delays mentioned in the description of procedures.

The thermal response characteristics of the SR-4 strain gages are ideal for this investigation. They are relatively insensitive to temperature changes when mounted on steel plates. As indicated in Figure 47, the maximum amount of apparent strain correction required is 130 microstrain. The HT gages are another matter, however. Figure 48 indicates a constant Apparent Strain-Temperature slope of 38.6 microstrain per °F. Thus, as temperature increases from 70° F ambient to a peak of only 360° F, the apparent strain correction becomes more than 11,000 microstrain. When compared to a calculated mechanical strain maximum of less than 2,700



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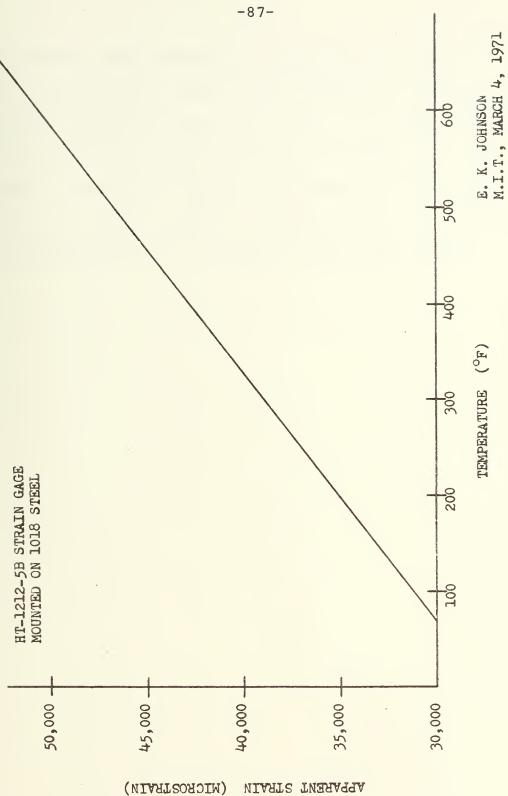
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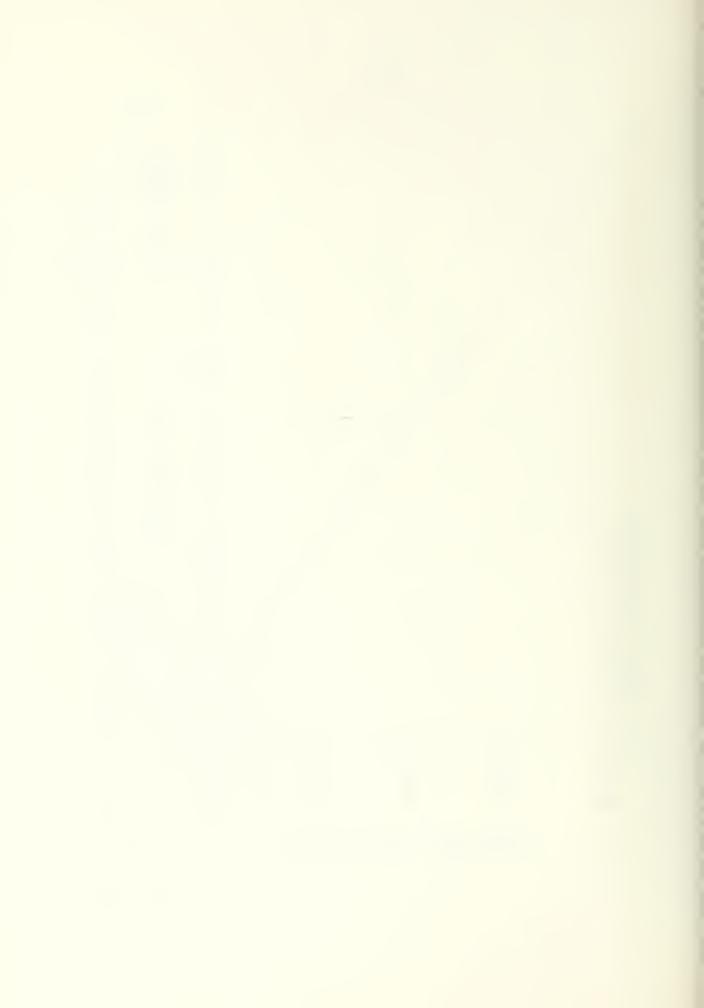


FIGURE 47. APPARENT STRAIN - TEMPERATURE CURVE, SR-4 STRAIN GAGES.

BLH DWG.NO. 217119-1



APPARENT STRAIN - TEMPERATURE CURVE, HT-1212 STRAIN GAGES. FIGURE 48.



microstrain, the assumption mentioned in Paragraph C-2 of this Section is no longer valid. Even if the Linear Superposition assumption were still valid, a 5% error in temperature or measured gage resistance would result in a 20% error in mechanical strain. As a result, the data recorded at the 0.55 inch location on the 3/4-inch HY-80 plate is considered unreliable and must be used with caution.



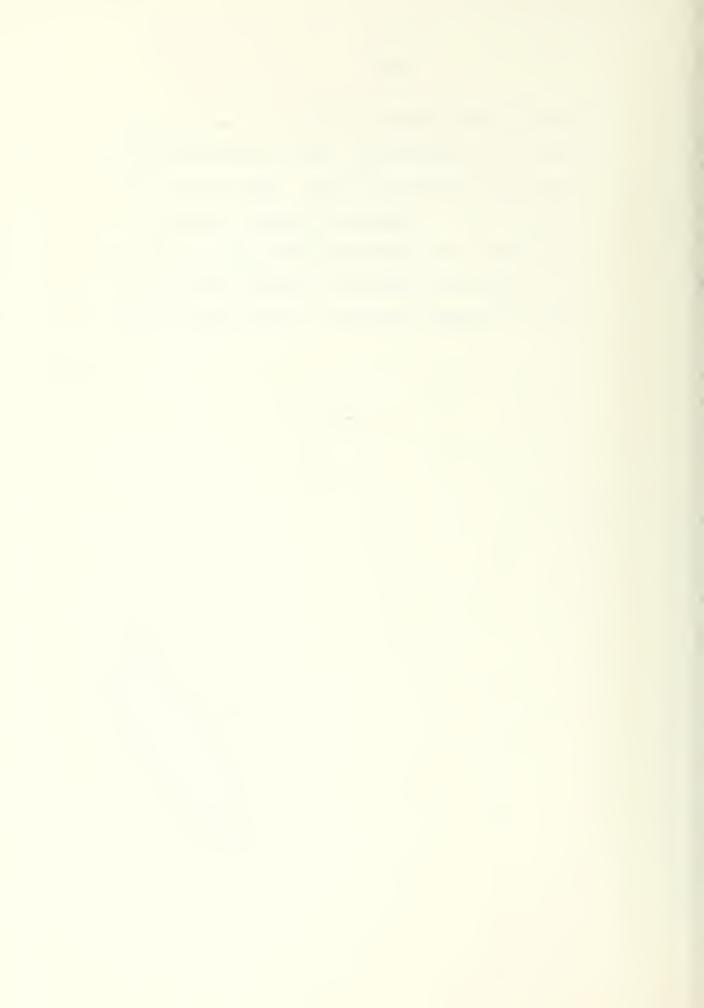
V CONCLUSIONS

Based on the preceding discussion, the conclusions reached in this investigation are:

- 1. The NASA weld analysis computer programs developed by Masubuchi and his coworkers are applicable to steel butt welds in marine structures. The programs can be used to compare alternative parameter variations as long as the point of interest is not located in the immediate area of the welding arc itself.
- 2. The thermal strain response of thick section plates to a single weld pass is slightly less than the response of thin section plates under the same conditions. Multiple passes, however, produce cummulative strain effects especially during the first few passes. Little or no accumulation is noted in later passes.
- 3. At a finite distance from the weld line, maximum mechanical strains caused by the welding arc are roughly proportional to the inverse of base plate yield strength.
- 4. In certain ultra-high strength steels, the passage of the welding arc produces an unusual strain response possibly linked to phase transformations during cooling.



- 5. Except in the immediate area of the welding arc itself, the longitudinal strain predominates over transverse and shear strains. Near the arc, the strain field is complex and rapidly changing.
- 6. The BLH HT-type high-temperature strain gages are not suitable for in-process welding experiments similar to those performed in this investigation.



VI RECOMMENDATIONS

It is recommended that research be continued with the aim of developing techniques for the production use of the NASA programs. While it would be profitable to attempt further parameter variations in laboratory experiments similar to those performed here, the next step should be to move the investigation to the Building Ways. I recommend that a ship construction project be selected and a number of production joints instrumented for in-process data collection. Parameter selection will undoubtedly be restricted by availability and minimum interference considerations, but this would not degrade the value of the results. Computer predictions run on the welds can be compared to the experimental results and a set of procedures can be worked out to use the programs as design and production tools.

The NASA computer programs should be expanded to include procedures for calculating the effects of preheat and varying levels of joint constraint. The programs could also be adapted to utilize their own output as a new set of initial conditions for multipass welds. Also, as stated in the NASA reports, two-dimensional solutions would provide more accurate information, especially in the area of the welding arc itself. 14

The value of the experiments performed in this investigation is directly proportional to the proximity of sensing elements to the weld bead. While HT gages were found

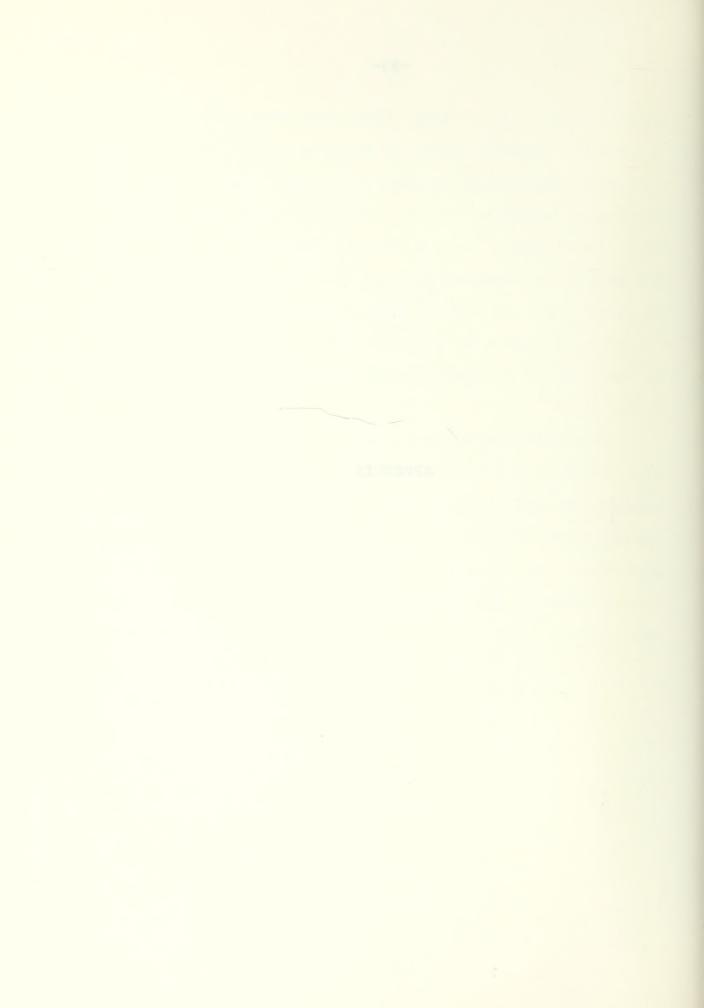


unsatisfactory, I recommend that other types of very high temperature gages be utilized and examined. Available models with good temperature compensation properties include: BLH Nichrome-V bonded or weldable gages (maximum temperature over 750° F), Microdot, Inc. MG-120 and 220 weldable gages (650° F) and equivalents manufactured by Micro-measurements, Inc. It is hoped that temperature compensated gages will be produced in the near future which will allow strain measurements to be taken in areas where welding temperatures peak at over 1,000° F.

More strain-temperature data is needed on the ultrahigh strength steels to verify the secondary tensile peaks
observed in this investigation. Specimens should be
instrumented, heated to elevated temperatures and airquenched. The results can then be compared to the welding
strain response and theories postulated to explain the
phenomenon.



APPENDIX



APPENDIX A

DATA REDUCTION COMPUTATIONS

The computer program appearing in this Appendix was used to convert the output of the strain gage recorder (Visicorder) into the data tabulated in Appendix B. The program was written in FORTRAN and utilizes two mathematical models. receives strain and temperature input in the form of offsets -linear displacements of the Visicorder tracing proportional to the resistance changes in the strain gages and thermocouples. The thermocouple readings are converted to temperature directly by means of calibration curves, but the strain readings are reduced by means of the model discussed in Section II-C, "Strain Measurement by Electric Resistance Strain Gages." Strain readings, S(I, J), are read in and converted to microstrain by calibration curves (utilizing a parabolic interpolation function, "FILLIN"). Apparent Strain corrections are made and the three readings from the strain rosette are combined into principle strains using the Mohr's Circle model.

The example listed below uses HY-130 data. Other computations require changes in calibration curves and in the call sequence for the Mohr Function. For this reason, some of the statements appearing in the program are superfluous for this particular example. Also, some manipulations of the data were performed to provide input to plotting programs.



```
READ (5,123) (METAL(I), I=1,2), THKSS, (PROC(I), I=1,2), (WELD(I), I=1,4
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           WRITE (0,13]) (METAL(I), [=1,2), THKSS, (PROC(I), [=1,2), (WELD(I), [=1,4
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        FURMAT(" METAL=",244,3x,"STEEL"/" THKSS(IN)=",F5.3/" WELD PROCESS=
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 1', 2A4/' WELD TYPE=',4A4/' NO, PASSES=', I3/' CURRENT=', A4/' ARC VOLT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            L'TRANSVERSE DISTANCE FROM WELD. "//5x, "TIME", 17x, "1.00", 12x, "1.75",
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        1AGE=',F60,1/' AMPS=',F5,U/' SPEED UF TRAVEL (IPM)=',F5,1/////28X;
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     DIMENSION T(99), S(99, 3), TZERO(99), SZERO(99, 3), TEM(20), ALPHA(20)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                CURRENT, VOLTS, AMPS, TRAVEL SPEED, NO. SENSOR LOCATIONS, NO. POINTS.
                                                                                                                                                                                               FORMAT ( * WELDING STRAIN-TEMPERATURE VARIATION, EXPERIMENTAL
                                                                                                                    WELDING STRAIN-TEMPERATURE VARIATION, EXPERIMENTAL RESULTS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            DIMENSION STRN (99,31, STR (99,31, PSTR (99), PMSTR (99), TEMP (99)
                                                                                                                                                                                                                                                                                                                                                                                                                                         INPUT: METAL TYPE, THICKNESS, WELD PROCESS, WELD TYPE,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      FDEMAT (2A4, F5, 3, 6A4, I3, A4, F0, 0, 2F5, 1, I5, F10, 4)
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   DIMENSION TR(20), ASF(20), SIGX(99), SIGMX(99)
DATA REDUCTION COMPUTATIONS
                                         3/4 IN. HY-130 STEEL
                                                                                                                                                                                                                                                                                                                                                                                                     DIMENSION WELD(9), PRUC (9), METAL (9)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  1.1, NPAS, CUR, VLT, AMP, V, SENS, ALPHI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         READ(5,141) (ALPHA(I), I=1,7)
                                                                                                                                                                                                                                          INTEGER NPAS, PASS, SENS, PTS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  READ(5,141) (TEM(I), I=1,7)
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  READ(5,141) (TR([],[=1,7]
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                                      EXAMPLE 1.
                                                                                                                                                             WRITE(6,110)
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WRITE(6,17°) TIME, (T(K), K=1,J), ((STR(K,L),K=1,J),L=1,3), (SIGX(K),K
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               "1,6X03(F11)02,6X1/" PRINC, STRN-
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   "",6X,3(F13.2,6X1/" STRAIN C.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            FORMAT (LX, F8, 2/" TEMPERATURE", 9X, 3(F10, 2, 6X)/" STRAIN A.
                                                                                                                               READ (5,150) TIME, (T(K), K=1,J), ((S(K,L),L=1,3),K=1,J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            STR4(JJ,KK)=((S(JJ,KK)-SZERO(JJ,KK))*(-10003))-ASTR
                                                                                                                                                                                                                                       3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     PSTR(JJ)=MOHR(STR(JJ,1),STR(JJ,2),STR(JJ,3))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    STR(JJ, KK)=STRN(JJ, KK)-((T(JJ)-72,2)*(ALPH))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              SIGX(JJ)=STR(JJ,1)+STR(JJ,3)-STR(JJ,2)
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                                                                                                                                                                                                                                       IF (TIME OGTS JOG SURO PASS OGTO 1)
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                     IF (PASS .EQ. 0.0) GU TO 999
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              PMSTR (JJ) =PSTR (JJ) /1 300.
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                                                                         FORMAT( PASS= 1, 15//)
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                                                                                                                                                          FDEMAT (F3.0,12F6.2)
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                                                                                                     ARITE (7,197) PASS
                                             WRITE(6,142) PASS
                                                                                                                                                                                                                                                                                                                                                                                                                               R=T(JJ)-TZERO(JJ)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          SX=SIGX(1)/10000
                                                                                                                                                                                                                                                                                           TZERO(11)=T(11)
                                                                                                                                                                                                                                                                 00 6 II=1,J
                                                                                                                                                                                                                                                                                                                                                                                                       00 8 JJ=1,J
                                                                                                                                                                                                                                                                                                                       DO 7 KK=1,3
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WRITE (7,195) I



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45 DEG. STRAIN GAGE READINGS
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                                                           FINDS PRINCIPLE STRAIN FROM THREE
                                                                                                                                                                              RUGI=SQRI((DIFEDIF)+(SQR*SQR))
                                             *** MOHR #** ROSETTE ANALYSIS
                                                                                                                                                                                                                                                                                                                                                                                                                              FUNCTION FILLIN(X, AB, OR, ND)
                                                                                             = 45 DEG. STRAIN READING
                                                                                                             C = 90 DEG, STRAIN READING
                                                                            O DEG. STRAIN READING
                             REAL FUNCTION MOHR(A, B, C)
                                                                                                                                                                                                                                                                                                                                                                                                                                                            FINDS Y(X) FROM TABLE OF
                                                                                                                                                                                                                                                                                             IF (SIG1-SIG2) 60,70,70
                                                                                                                                                               SUR= (20 * B) - SUM
                                                                                                                                                                                                                                                             SIG1=ABS(SIGMA1)
                                                                                                                                                                                                                                                                            SIG2=ABS(SIGMA2)
                                                                                                                                                                                                                                              SIGMA2=11-W
                                                                                                                                                                                                                              SIGMAI=U+W
                                                                                                                                                                                                             W=R001/2
                                                                                                                                                                                             U=SUM/2º
                                                                                                                                                                                                                                                                                                              P=SIGMA2
                                                                                                                                                                                                                                                                                                                                               P=SIGMA1
                                                                                                                              SUM=A+C
                                                                                                                                              DIF=A-C
                                                                                                                                                                                                                                                                                                                              G0 T0 2
END
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EXIT

CALL

666

ANTRA(X1, X2, X3, X, Y1, Y2, Y3)=Y1*(X-X2)*(X-X3)/((X1-X2)*(X1-X3))+ 1 Y 24 (X-X1) 4 (X-X3) / ((X2-X1) 4 (X2-X3)) + Y 34 (X-X1) 4 (X-X2) / ((X3-X1) 4 DIMENSION AG(NO), OR(NO) 1F(X-AB(1)) 1,3,2



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8.86
                                                                                                                                                                                                                                                              8.67
                                                                                                                                                                                                                                                              7.86
                                                                                                                          Y=ANT RA(AB(M-2), AB(M-1), AB(M), X,OR(M-2), JR(M-1),OR(M))
                                                                                                                                                                                            28. 290. 14.
                                                                                                                                                                                                                                                              8045 7047 7067
                                                                                                                                                                                                                                - 600 -
                                                                                                                                                                                                                        400°
                                                                                                                                                                                                                                          STRAIN AND TEMPERATURE READINGS FROM VISICORDER
                  Y=ANTRA(AB(1), AB(2), AB(3), X, OR(1), OR(2), OR(3))
                                                                                                                                                                                                               96.9
                                                                                                                                                                                                                       325°
                                                                                                                                                                                                     600°
                                                                                                                                                                                                                                 -129°
                                                                                                                                                                                            BOCRP
                                                                                                                                                                                                               609
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                                    IF(X-AB(2))1,6,5
                                                                                                                                                                                  INPUT DATA CARDS
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                                                                                    IF(X-AB(I))8,9,7
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         60 TO 99
                                                                                                       60 TU 99
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                                                                                                                                   FILLIV=Y
                                                                                                                                                                                                                        10°0
                                              Y=0R(2)
                                                                                            Y=.JR(I)
                                                                                                                                                                                                                                                              4093
Y=UR(1)
                                                                                                                                            RETURN
                                                                          1=5
                                                                                                                                                       END
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APPENDIX B
TABULATED DATA

B ATOMSYSA

BELDING STRAIN-TEMERRILME VARIATIEN, EXPERIMENTAL MESLLTS TRANSVERSE CISTANCE FICH WELL. AUSETTES BTRAIN 7: 72.2c 14.5c 14.5c 76.20 14.56 14.56 14.56 14.56 BLAIL SARINE THERMOCOUPLE = |-14.006 14.56 14.56 14.56 14.56 PEIAL HV-EC SIEEL

IPMSSIRN PCG 20

IELC FECESS WAS BELL

NC PASSES IN CLAFE IN CLAFE

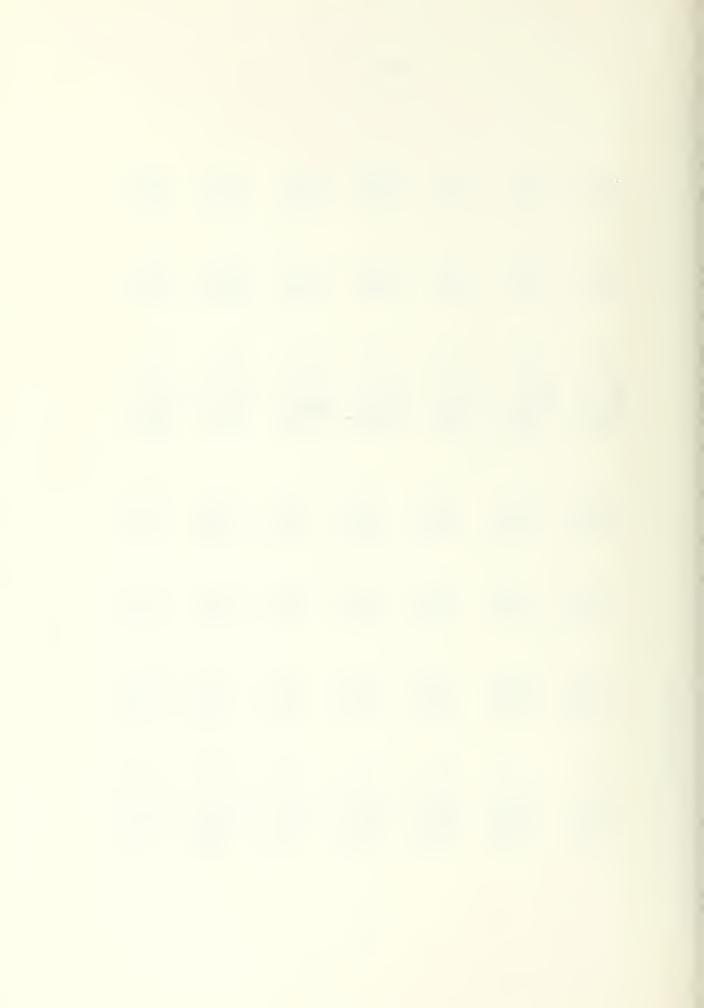
NC PASSES IN CLAFE IN CASSES SEPERATURE
SIRBIN B. LPECH.)
SIMPLIN E. B.
SIMPLIN C. B.
PFINC. SIKN. B. STAIN C. TEPPER TILKE STRAIN E. T. T. STRAIN C. T. FFINC. SIXN. T. 4 . 5 . 4 4 1 i v E 1.0 (MACK) 72.76 14.53 14.53 14.63 72.24 14.54 14.54 14.54 17.26 14.53 14.53 14.53 WELDING STRAIN-TEMPERATURE VARIATION. EXPERIMENTAL RESULTS TRANSVERSE DISTANCE FROM WELD. THERMOLOUPLE STRAIN ROSETTES 72.26 14.53 14.53 14.53 72.26 14.53 14.53 14.53 72.26 14.53 14.53 14.53 WELD LINE 72.26 -45.47 -135.47 -135.47 72.26 14.53 14.53 14.53 72.26 14.53 14.53 14.53 STEEL STABIN A. (MECH.) STRAIN R. STRAIN C. PRINC. TEMPERATURE
STRAIN A. IMFCH.)
STRAIN R. "
STRAIN C. "
PRINC. STRN. " STRAIN A. (MECH.)
STRAIN A. STRAIN C. B TEMPERATURE TEMPERATURE METALUMINO. PASS= 1 1.00 5.00 0.00



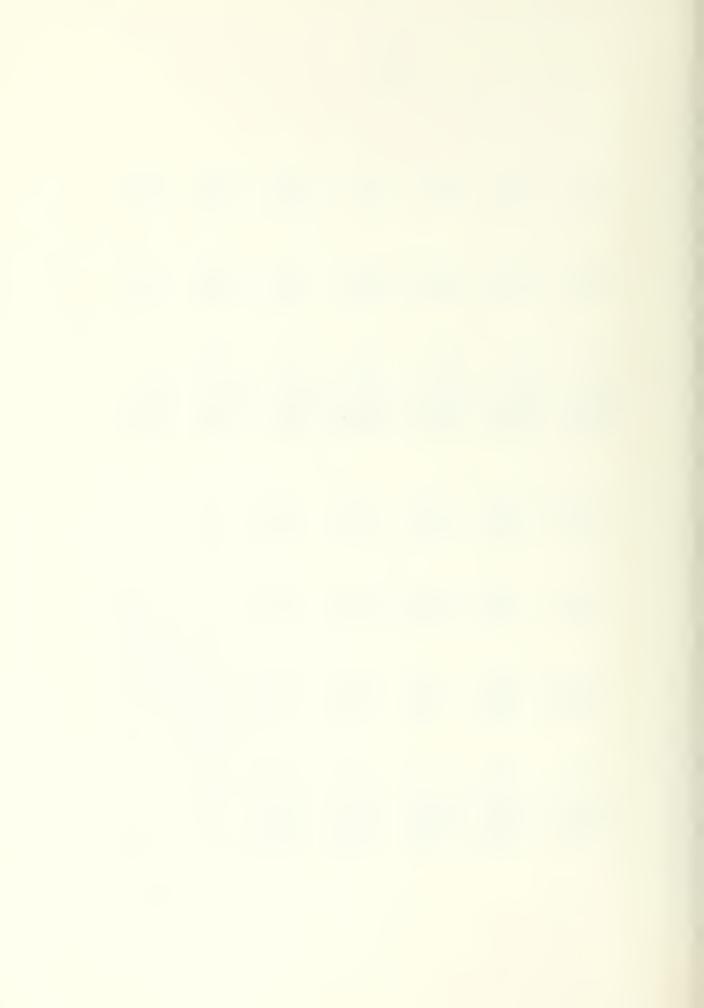
:	14.26	0:05	14026	14.56	14.56		linie	14.64	4 9 7 1	7 7 7 7	10.00				72.26	14.56	14.56	14056	34.56			12.26	14,56	74.56	74.56	66.55			14066	9:095	0107	74.00	66.00			14.26	44.66	1:4.56	34.56	136.04			12.26	910	154056	05.47	157.53	
	12026	14.50	14.56	-105-44	-13C.25		10036	99.91.	7 9 . 4	100.00					12006	-15.44	44.56	-105.44	- 444.6 1			72.26		74.56	-105.44	-411.06			14.26	-12.44	134.56	- 10:04	13017:-			74.26	-15.44	25 4 . 5 6	- 165044	-443.50			17.43	- C . 2 .	30 50 5	->6.24	-440.55	
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		77.76	-245.47	-4-5-47	£2.23.	F. F. B. F.		4	× 1 × 1		7 4					45 a 5 F	-1 K.47	-765.47	440 62	-163.10			6 H	4 1 1 1 1 1	6 3 6 5 5	- 2 .0 . 5 -	-072.7ª			37.76	240.11	-710.00	(3.00)	- 9 24 6 -			151.4	2.3.47	-576.53	-546.53	-173.44			164.00	26.97	-446.13	-535.12	-6.7.53
		72,24	14,53	14.54	16. 63	14.53			77.63	7.15	7.15	67.01	70.50			6.7. 4	22.65	23045	P 3 6 4 5	2 ° 40			20.00		16.53	74.57	74.53			72.20	-45.47	14.53	76.53	74.53			72.24	-45.47	44.53	1. 4.53	175001			77.43	-52.95	67.15	127.15	132.72
	S GAGE LOCATION)		-45.47	1145 47	P 4 U 4	-165.47			42.57	-53.52	-237, 52	-49.52	-219.52			27. 4.9	-125.52	5 5 5 6 -	5.52	-312.91			e e	£ 00 00 00 00 00 00 00 00 00 00 00 00 00	000	4.5.11	(T to 0) (F t)			172.83	- 550 R7	-379. A3	160,18	-612,32			149.99	-1054erB	-394° 18	265,92	-1.54.08			205.76	-1241.13	-441073	314.67	-12H1.AA
	ICACH (ARC PASSES	TENDERATINE	MUNICIPAL A MARCH		1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 "7"LV "L7L"C		11.73	TEWPF BATIBE	A A		\$ 0 218015	m *holy *JNIac		6	3 CT 1 C V C V C V C V C V C V C V C V C V C	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	2 TO 10 TO 1		7 2			1 70 71	TEMPERATURE	TOTAL DO THE HOLD	1 8 0 7 1 d 5 h 6	2 0		14.00	TEMPERATURE	STRAIN A. IMPIH.1	STRAIN A. "	STOATS "	PRINC. STRV. "		16.00	TEMPERATION	STRAIN A. INFCH. !	STRAIN R. "		paluf. Stav. "		17.00	TEMPFRATURE	W	STRAIN R. "	STOAIN C. "	



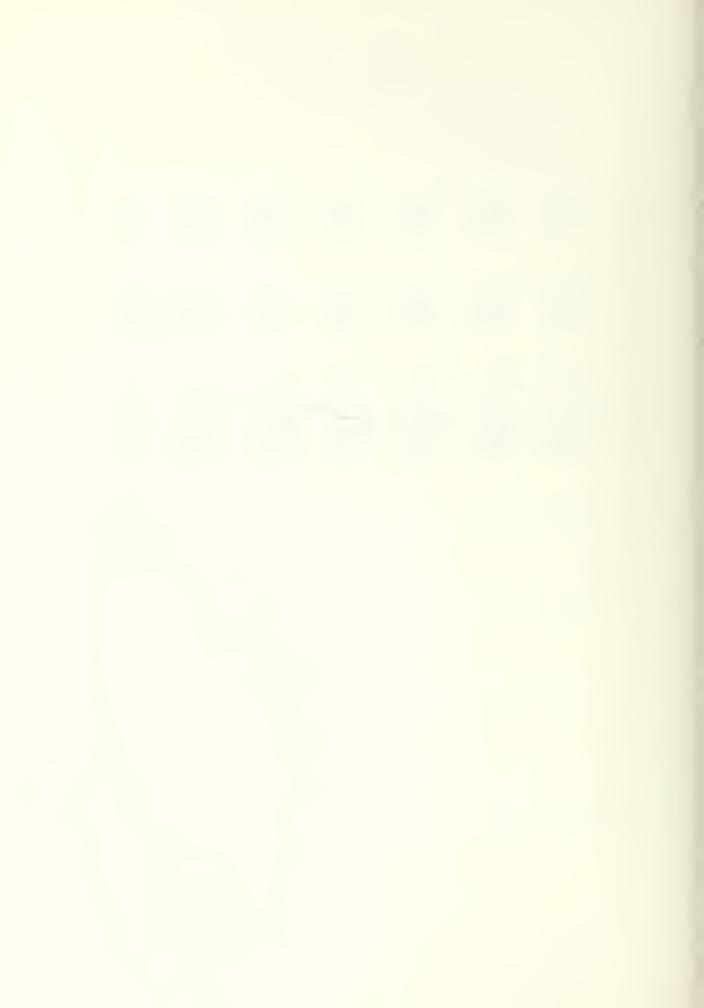
72.26 14.26 154.56 134.56 266.73	75.624 14.56 154.56 154.56 154.56	12°458 95°458 95°458 95°458	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1	1 4 4 5 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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12.CC SEMPLA COSTABLA	12°CC STABLA B. TPECH. STABLA C. STABLA C. B. STABLA C. B.	IN.CC IEPPERATURE STRAIN D. (PECF.) STRAIN C. " STRAIN C. " PRINC. STRN."	STREIN E. PECH. STREIN E. STREIN E. PECH. STREIN C. PECH. STREIN C. STR. STR. STR. STR. STR. STR. STR. STR	STAN.	TEPERATURE SIRAIN DO (PECTO) SIRAIN CO " SIRAIN CO " PAINCO SIANO"
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77-43 -47-85 -47-15 157-15 167-39	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	77°47°47°47°47°47°47°47°47°47°47°47°47°4	11111111111111111111111111111111111111	114.48 1114.48 1114.48 1114.48 1114.48 1114.18 1114.18	12 2 7 2 4 4 5 4 4 5 4 4 4 4 4 4 4 4 4 4 4 4 4
255.84 -1618.84 -518.44 301.55	275.45 -1731.98 -531.98 -7747.1	309.98 - 1849.44 - 7619.44 - 251.95 - 1848.87	19.057 -1910, 55 -1970, 55	1204-06 1204-06 1204-06 2018-24 377-51 2188-62 1156-18 2315-62	00 "00" 00 "00" 16 "00 % 6" 16
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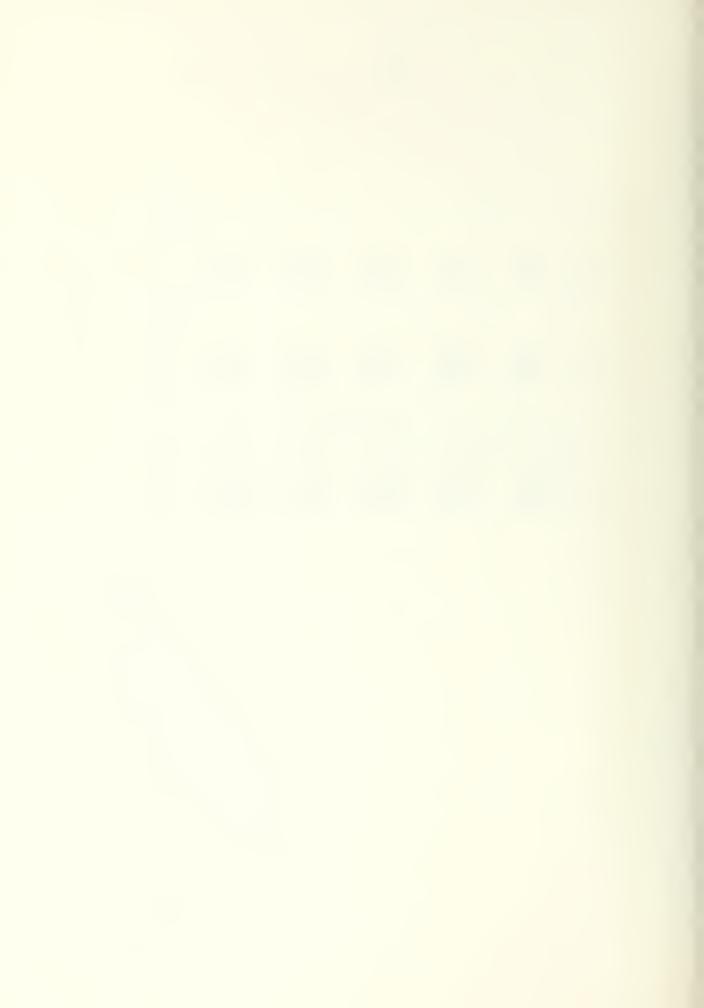
				33.61		
C				TEMPERATURE	7:10:4	74066
TO THE PARTY OF TH	419.23	160,00	610013	4	-517-5	- 15.0 64
2000	2300 13	8. 757-	-2249, K7	STHAIN E.	1:4.64	3 . 0 . 7
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		98.03	36.36.43	PEINC. SIMM.	-50505-	£ 2 5 0 m 3
ODING CTON. "	-2610-91	-407.1	-7447,12			
				3, 36		
;				1 EPPENAILME	343.10	least
	104 34	214.4	304.71	SINDIN D. (PECH.)	-10:00	-15,064
PROPERTIONS AND DESCRIPTIONS	F. 4501-	-677.14	48.96.63	å	45.2E	34051
CIREL B. LATCHOL	E	137.36	-146,35	SIPPIN C. "	435.26	4 4 0 5 4
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7	-2127.64	-604.15	-2324.51			
				. 17 17 2 3 1 2 5 C	215.2F	10000
90°00			, n	CIEBIN D. IPECH.	-1176.00	4, 5 0 3 8 .
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1 14	-1756.29	-P.17. 42	0000000	• 40 4147	425.54	: 140 6 4
	-1394,29	-1 H 7 4 5	G* 0 7 1	• WYIS CHIEG	-1175.51	45.45.5
	475.71	11/20/1	**************************************			
PRINC. STRN. "	67.2161-	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	• • • • • • • • • • • • • • • • • • • •			
				24.00	4	
30.046				TEMPERATURE	7 to the	37 9 11 -
Truperating	247,79	218.6A	ZEROKE	STERIN RO (PRCHO)	2201251	7 7 0 3
STEELIN A. IMPCH.1	-631.76	-135.37	25° 400 =		27.17.	9 0 7
STRAIN 8	-871.76	-116. 17	05.	STATE CALCO	2000	*1 *2 *** ***
STRAIN C	414,74	254.68	150.66		1	
a N	-1734.58	-746.33	-1:24.76			
				26.66		
				1 EPPERATURE	356.40	14.020
TOOL 00 00 00 00 00 00 00 00 00 00 00 00 00	77.43	R7.57	77.43	1	75-17-1-	
CTOALM A. IMPER.	127.15	84.09	-232.4°	SIFFIN E.	75 - 107 -	7 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
CTOATE B. S	-532,85	1371 . B.R.	427.15		7.07.	
	367.15	3000	127.15	PEINC. SIAN.	6107F77	3
PRINC. STRW. "	1008.89	421078	-545.40			
				26.00		90
				TEPPERATURE		9 71
COMPLE TIMES	0.73 SEC. FRECUTION TIME:		1.01 SFC.CHJECT TOSE	O THE STREET	150125-	14056
					656.45	3,04,2
				* * Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	-1510.66	164.23
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					15.55	254056
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371.53		114. 26. 6.3 -16. 6.5 116. 6.5 113. 2.3	18500	151.46 - 237.61 - 177.61 172.63	1 2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	175.11 -458.12 -7.75.12 -40.28	6
-1e34.57	4 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	402.51 -2056.71 -646.71 245.25		402.51 -1546.31 -586.31 -1546.25	194 21 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1 15 0 0 . 2 4 . 2	040E FAILURE 34C.45 15304.85 14734.85
FFIAC. STAN. "	AC.CC SEPPERATURE SIFALN A. (PECH.) SIRAIN C. "	SCOCC SPAIN A. (PECH.) SPAIN G. STAAIN C.	COCC SIFALA CO (PECHO) SIFALA CO (PECHO) SIFALA CO " " " " " " " " " " " " " " " " " "	7C.CC SFFIN A. (PECH.) SIFFIN A. (PECH.) SIFFIN C. "	BC. CC 1EFFEDATURE STRAIN 6. (PECH.) STRAIN 6. STRAIN C. PRINC. STRN.	SOCC SIRAIN A. (PECH.) SIRAIN C. " SIRAIN C. "	ICC.CC IEPERATURE STRAIN A. (PECH.1 STRAIN B. "



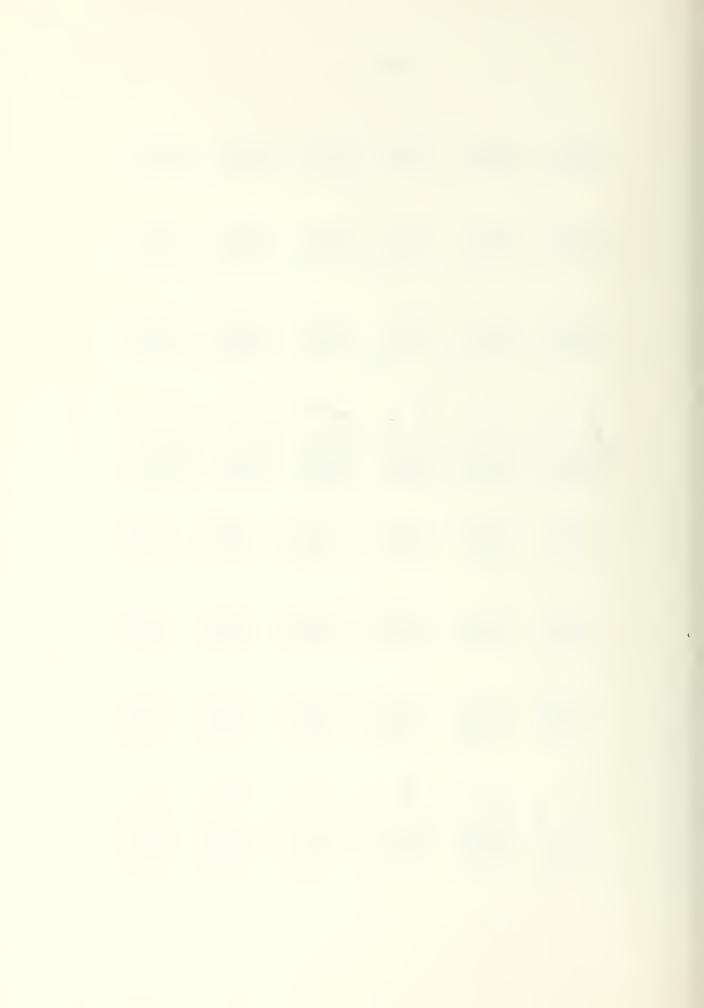
						4.11 SEC.CHURUE Cour Sec.Stuff
-925-10	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	지 보 경 (U J)	1	151.46 -137.61 -63.61 -65.035 452.035	6 1 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0 H 2 Z 2 Z 3 Z
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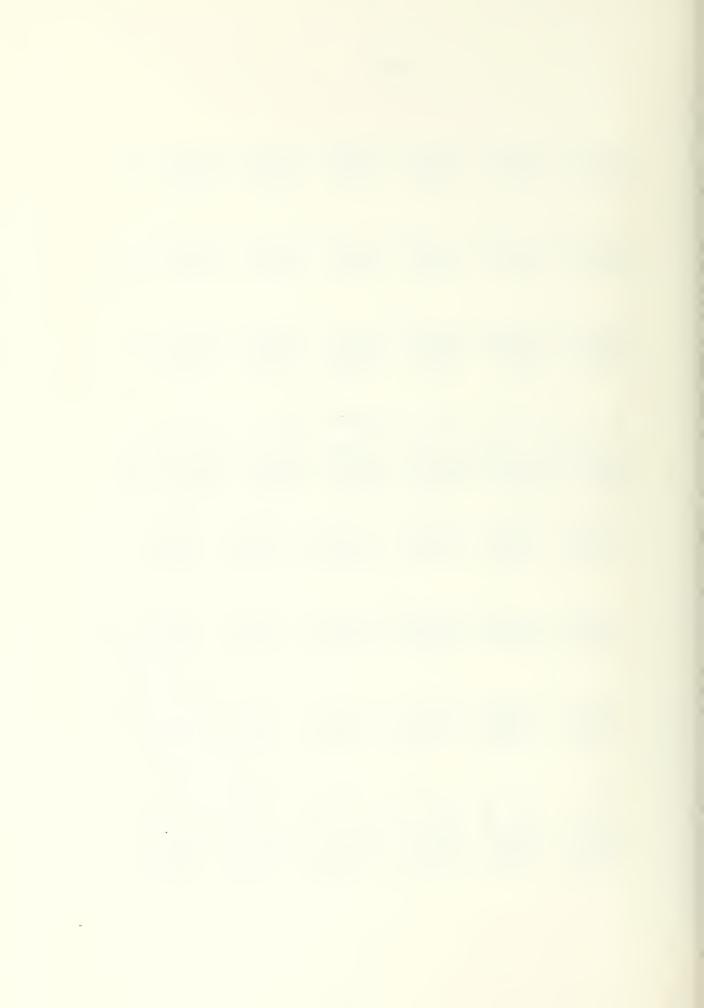
				0	0.750 INCH HT-80 STEAL (SUNTLINED)	REL (SOUTHWES)	
				PRINC. STRV	-1797.38	117.55	139.33
MFIDING STRAIN-TEMPERATUR	RATURE VARIATION	E VARIATION. EXPERIMENTAL RESULTS	RESULTS	:			
				TREPERATION	141.75	138.98	137.07
				CTBATA A. CAFCH.	-1765.34	明めの は	4.46
	5XX	WELD BOKE		STRAIN S.	-1754.79	-93,62	-45.54
		, ,		STRAIN C.	-1723.13	46.38	104.46
	-	/			-1754,79	156.38	154.46
LIP CONSTRUCT					-1797.3A	157.27	166.27
では、これでは、これには、これには、これには、これには、これには、これには、これには、これに	-						
MELO TYPE SHITT WELD							
NO DA CERCO 18	•			7.10			1
CHORENTADOR		•		TEMPERATURE	143.75	116.98	137.67
ADOLES TACK	+	, 0 K		STRAIN A. (MFCH.)	-1775.00	-13.62	-5.54
	Tampino	4 TRAIN		STRATU M. "	-1754.79	-71.62	-25.54
200	4 00				-1733.68	86.38	114.46
APPEND OF THE OFFICE OFFICE OFFICE OFFICE OFFICE OFFICE OFFICE OFFICE OFFICE OF THE OFFICE OFFICE OFFICE OFFICE OFFICE OFFICE OFFICE OFFICE OF	•			ź	-1754.70	146.38	134.46
					-1798.72	157.21	154.46
				60.00			
	TRANSVER	TRANSVERSE DISTANCE FROM WELD.	WELD.	TEMPERATIIRE	143.75	138.98	137,07
				STRAIN A. IMFCH. !	-1746.74	-3.62	4.46
11 20	4.0	1.7	2.7	STRAIN B	-1754.79	-13.62	14.46
1				STRAIN C	-1712.57	106.38	124.46
				ź	-1754.79	116.18	114.46
					-1786.83	136.52	142.57
PASS							
				In. " (ARC)	** ***	90 98	127.07
66.00		;		Traperation	61 6661	04 900	14.46
TEMBERATIRE	72.25	72.2	62.27	ľ	-1764 34	20 et - 4	24.46
146	ر"،(-			5 P-48-15	70.000	114.34	136.46
	60 of -	ຄຕ•ນ=	03.0		1344 34	174.10	124.46
STDAIN O. 8	-13° U	0 (0 0 (0 1	-2.6		97.64/1-	124.48	152.57
		r (200				
DRING. STRV. "	2.0	000	22.0				
				11			
					141.75	20 ° 20 ° 20 ° 20 ° 20 ° 20 ° 20 ° 20 °	13101
3 P. I. Bandanay	143.75	134.93	138.03	147	-1683.91	10.00	0000
STRAIN A. IMFCH.1	-1713.68	57.34	25.41		-1 AR 3. 91	E	C * * * * * *
STRATU R. "	-1786.45	-67.64	-54.50	STRAIN C. "	-1564:32	100.08	94 401
ATRATA C	-1711.68	-2.64	55.41		10.00	000000000000000000000000000000000000000	
;	-1786.45	117.36	135.41	DRING. STRN. "	-1797.01	117.80	1 3 5 0 1
PRINC. STRE	-1797. 1A	122.23	136.59				
				۲۰۰۶۱			
				TEMPFRATURE	143.75	138.98	137.07
T S C S C S C S C S C S C S C S C S C S	141.75	138.08	137.07	STRAIN A. IMPCH. 1	-1628.14	16.38	14.46
TOURS OF THE PARTY	-1721.48	A. C.	14.46	STO ALL A.	-1527.60	56.38	94.49
8 d 714010	-1784.45	-73.62	-45.54	STRAIN C	-1459.28	106.38	124.46
	-1731. 48	Se . 4	74.46	;	-1522.67	86.38	94.46
S 2000 030 a	11304 46	116.34	134.46		-1737,90	119.46	126.90



137.07 244.46 144.46 144.46 164.46 164.46	137.07 204.46 134.46 134.46 264.66 264.46 264.46	137.07 314.46 1114.46 64.46 264.46 356.46	137.07 324.46 104.46 74.66 294.46 396.46	1137.07 334.46 94.46 94.46 374.46	137.07 334.46 74.46 104.46 364.46 364.46
1186.98 906.98 96.38 - 33.62 216.38	N N N N N N N N N N N N N N N N N N N	# # # # # # # # # # # # # # # # # # #	11 + 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0 +	ME 1 MA 400 ME 1 ME	10000000000000000000000000000000000000
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PO.00 TEMPERATURE STRAIM A. (MECH.) STRAIM C. 10MG. STRAIM.	S - CO - C - C - C - C - C - C - C - C -	TEMBERATIBE STRAIN R. (MECH.) STRAIN R. (MECH.) STRAIN R. R. (MECH.) STRAIN R. R. (MECH.) STRAIN R. R. (MECH.) STRAIN R. R. (MECH.)	Porto Train a. McCM. C STRAIN A. MCCM. C STRAIN C I DMC. STRW PRIMC. STRW	TRAFRACIA STRAIN R. (MECH.) STRAIN R. (MECH.) STRAIN R. (MECH.) LINGS, STRA. 8	SACOON CANADA CA
137-07 94-40 124-40 94-40 94-40 94-90		137 138 128 128 118 96 96 128 27	137.07 124.04 124.46 104.46 106.66	11999 11999	11140 1440 14446 14444 14444 14444 14444
139 786.98 866.38 966.39	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	M M M M M M M M M M M M M M M M M M M	11 12 13 13 13 13 13 13 13 13 13 13 13 13 13	13966 2166.308 1766.308 1166.338 2166.35	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
1501.49 -1501.49 -1374.84 -1374.84 -1374.84	1896.24 -1967.44 -1967.46 -1966.87 -1749.09	-1142 -1246	159.69 -179.69 -910.59 -910.62 -910.50	165.669 -1172.56 -729.27 -623.77 -729.27 -1346.79	1 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
TEMPERATURE CTRAIN R. (4ECM.) ATRAIN R. (4ECM.) ATRAIN R. R.	TO STATE OF THE ST	15°00 TEMPERATION CIRCHAC CIRC	TEMPERATURE STRAIN A. MECH. (STRAIN G. STRAIN G. CARAIN G. COMT. STRN. B	TREET AND A CAFCHAN A CAFC	TERDERATURE STRAIN A. (MECH.) STRAIN A. I DAG, STRAN.



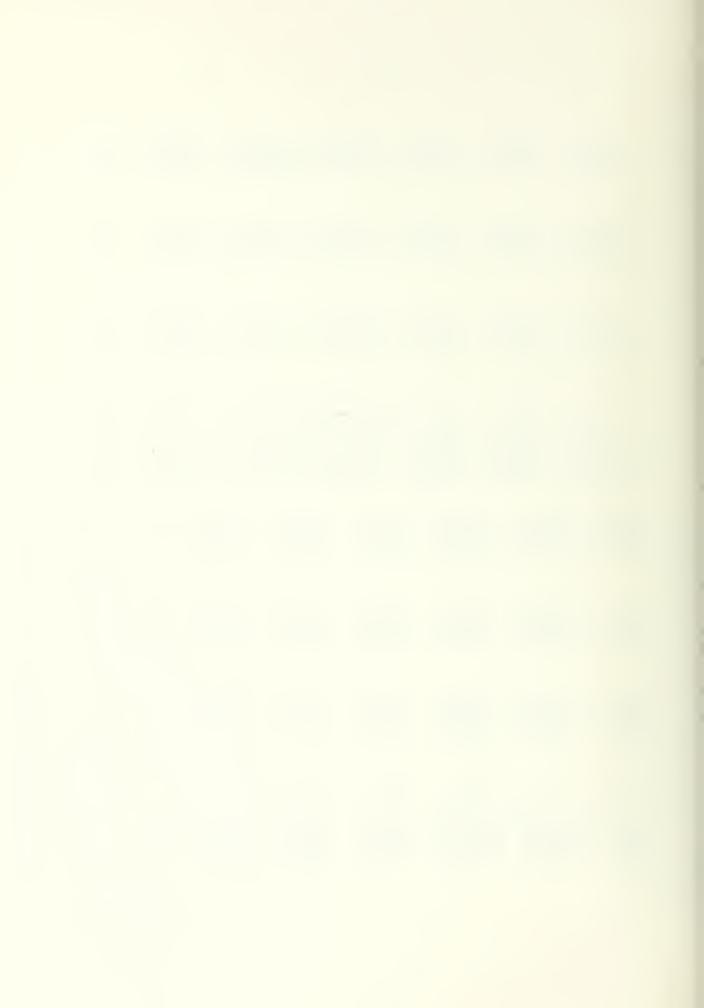
				TEMPERATURE	288° T6	168.59	149.47
36.07			138.03	STRAIN A. IMECH. I	-1222.08	179.47	288-10
TEMPERATURE	269.68	150.00			-2066-39	-2.53	46.10
STRAIN A. IMECH.)	-486.73	54% 13	1 2 2 2 4	STOATE T	-1437-48	-10.53	128.12
STRAIN B	-1035.04	-50.86	10001		06.44061	169.47	368-10
	-496-78	40.14	125.41	LIMING SIRWS	46.0003	211	20 V
8 7670 040	-1045-04	349.14	375.41	PRINC. SIRV.	-213100	24017	
	: :	372.74	405.69				
00 000 000 000				:			
					285.95	194.31	154.24
\$0°00			4	TOWN A MORONA	20 6461	186-30	282.75
TEMBERATION	278.26	155.20	138.03	Total or Minney	0000000	46.46	72.75
CTRAIN A. INCLA. I	-565.07	243.67	325.41		5.01017-	C 00 2	132.75
ALTERNATION OF THE COMME	-1230.42	-46.33	14.59	T PINELY	05 04 0 11	0.00	342.75
	14 6 0 0 5	43.67	135.41		-2101-	05.000	245012
STRAIN CO.	1 2 3 0 . 4 2	133.67	395.41	PRINC. STRN. B	-2218-32	20.20.2	91.506
COMBS SING.	-1124.02	350.37	420-83				
	9						
				60.00			
				TFMPFRATURE	287.17	200°04	158000
45.03		140.02	138.98	THE	-1376.33	173.34	2000
TEMPERATURE	67 °48 \	200	316.38	STRAIN M. "	-21TB.44	33.34	76.43
A. 1 MF	-716.00	05 04 7	46.38	STRATM C	-1576.86	-26.66	126.45
	-1486.44		144. AB	ž	-7178.44	113.34	316.45
STRAIN C	-832.09	24. 30		BOINT CTON	-2225.78	181.24	335038
	-1486.44	289.30	2			1	
	-1571,14	314.69	\$6.91 *				
				100 PA 010 PA	373 40	205.76	165.69
				CALL CALL	AA 40 4 6 1	170.41	244.15
	288.76	168.55	139.93	A. Lap		- N 0 C W	94.18
o State of the state of	10.31.01	237.14	337.36		C4 00 1/7-	1001.0	
STRAIN A. INTURA	400444	-32.86	57.36	STRAIN C.	-165Te 78	50.67-	114017
00 X 20 00 00 00 00 00 00 00 00 00 00 00 00		17.14	137.36		C4 * 0 1 2 Z =	10 0 0 P	40.000
		257.14	387.36	DRING. STRN. "	-7268.58	116.22	Z 000 F 0
	67.4401	28.4.8	407.96				
PRINC. SIRM.	7 . 6						
				129.00			
				TEMPFRATURE	266.82	208-62	170.40
55.30		173 33	142.80	_	-1579.08	174.26	234.13
TEMPERATURE	11.062	20.00	3000		-2213.43	64.26	61.601
STRATH A. IMECH.	0 - 00 CM	-27.78	60.40	STRAIN C. "	-1695.18	-35074	61.601
STRAIN S.	E P 0 C G T 1	12.23	140.40	I DNG. STRN	-2233.43	74.26	53% 15
STREEN C.	16.00.11-	242.23	380.40	PRINC. STRN. "	-2295.61	174.38	266°08
		272.30	399.29				
PRINC. SIRV.	AD 06 20 T						
				150.00			177.14
60					273040	569.17	04:416
200 00 00 00 00 00 00 00 00 00 00 00 00	289.71	179.05	144.70	STRAIN A. IMPCH. I	44 44 61 -	\$1.00 I	116.40
THE PERSON A CHARLE OF	4440	188.52	30.2.52		#10 TO TO	***	
3	0 0 0 0	-21-48	52.52	STRAIN C. "	-1687.21	02064-	
N-18 - 6.	100000	11.40	132.52	I DNG. STRN. "	-2141.74	47.000	0000
	11.07.01	208.52	382.52	PRINC. STRN. "	-2213-89	176.74	779677
CONC. SING.	-1698-65	242.69	403.12				
				240.03			103 02
				TEMPFRATURE	21T.21	198013	70 0 6 0 7



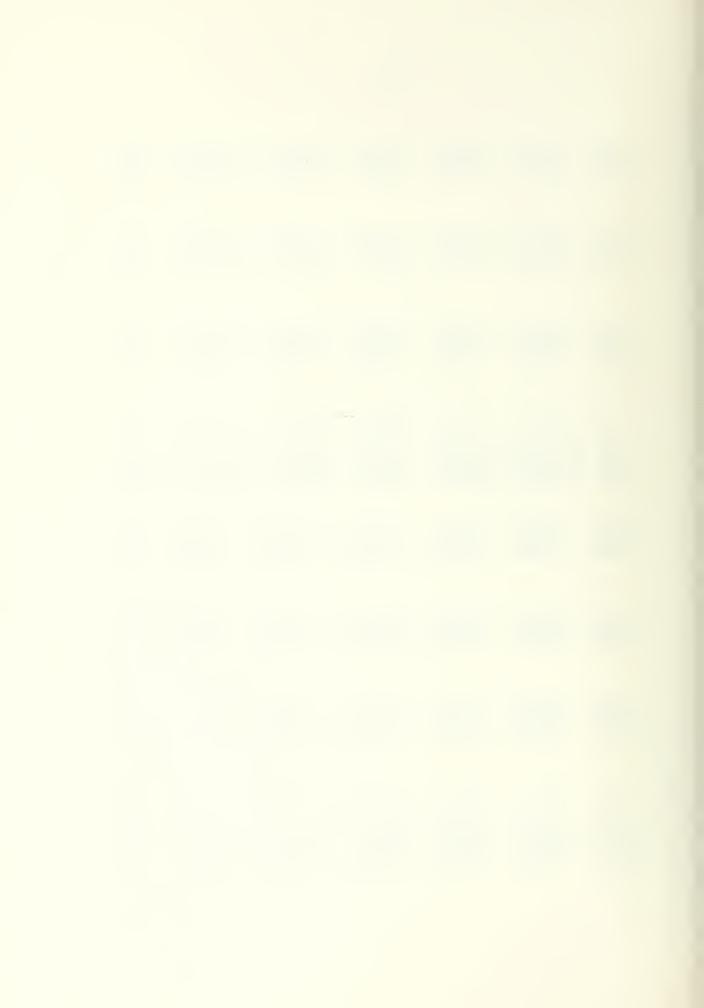
195°20 223°66 13°67 23°67 23°66 272°32	155.20 223.620 13.67 33.67 . 243.65	155.23 23.66 3.66 43.67 255.67 279.68	155.20 183.66 93.67 273.66 273.66	155.23 13.66 23.66 1.23.66 283.66 283.66	155.27 183.66 33.67 123.67 277.66	155.23
154.24 242.75 -57.25 -47.25 252.75	15% 24 23% 75 -67, 25 -47, 25 252, 75 305, 35	154.24 272.75 -874.25 -474.25 762.75 318.77	154.24 192.75 -117.25 2.75 312.75	154.24 182.75 -97.25 332.75 342.36	154,24 182,75 -77,25 62,75 372,75	154,24
159.01 -1710.19 -1740.86 -1630.76 -1740.86	159.71 -178.75 -1763.41 -1633.76 -1763.41	159,01 -179,30 -160,41 -1672,10 -1767,41	159.71 -1770.96 -1572.86 -1577.11 -1749.86	150.01 -170.07 -1633.76 -1643.70 -1643.76	159.11 -1781.52 -1598.77 -1598.77 -1598.77	150°31 -1754°15
TEMPERATURE STRAIN'A. (MECM.) STRAIN'B. ATRAIN. (TRAIN. PRINC. STRM.	TEMPERATURE STRAIN A. (MFCH.) STRAIN A. (MFCH.) STRAIN C I NOS STRN PRINC. STRN	TEMPERATURE STRAIN A. IMFCH. I STRAIN R. STRAIN R. CONG. STRN. **	TEMPERATURE STRAIN A. IMECM.) STRAIN A. IMECM.) STRAIN C. IMECM.) FORM. STRN.	FRADERALLAF STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN C. INNG. TRN. B	TEMPERATURE ATRAIN A. (MECH.) ATRAIN B. (MECH.) ATRAIN C. " I TNG. ATRN. " PRING. ATRN. "	TFMPFRATURE STRAÍN A. IMECH.)
213.92 143.92 63.92 133.92 214.09	175.23 204.30 134.30 54.30 124.30 204.47	173.32 202.22 132.22 52.22 122.22 202.39	169.51 218.14 159.14 58.14 148.14 218.76	161.88 210.26 120.26 60.26 180.26 211.74	158.06 216.45 106.45 166.45 256.45	
210,97 60,97 -19,03 137,97 216,18	182.86 212.83 32.83 -7.17 172.83 233.22	178,09 237,46 27,46 -12,56 167,46 227,84	172.37 211.20 20.20 10.20 191.20 241.20	161.88 210.26 10.26 10.26 210.26 251.68	157,111 2°5,52 5,52 5,52 2°5,52 2°5,52 2°6,94	
-1716.86 -2033.49 -1516.34 -733.49 -767.38	194,31 -1878,76 -2029,28 -1712,66 -2029,28 -2167,48	166.68 -1790.34 -1790.34 -1662.13 -1790.34 -1936.54	1A3.00 -1827.73 -1836.63 -1711.64 -1876.63 -1923.25	167.65 -1794.63 -1690.64 -1646.87 -1699.64 -1899.64	1693.97 -1693.97 -1669.97 -1648.68 -1697.97	
STRAIN A. IMFCH.) STRAIN C. CONG. STRN. B	46%, "TEMPERATURE ATRAIN A. IMFCH., J STRAIN B. " ATRAIN G. " I ONG. ATRN. " PRINC. STRN. "	TREPEDATURE TREPEDATURE TRAIN A. [MFCH.] TRAIN A. [MFCH.] TRAIN C. TRAIN C. STRN	FAMPEDATINE STRAIN A. [MECH.] STRAIN A. TATAIN C. STRAIN C. TATAIN C. TATAIN C. TATAIN C. TATAIN C. TATAIN DRING. STRN	PRPSEATINE STRAIN A. IMFCH., STRAIN R. " STRAIN R. " I ONN. STRN. " DRIVE. STRV. "	TEMPERATIRE TEMPERATIRE TOTALN A. IMECH. J. TRAIN C. TRAIN C. TRN. T. TONG. STRN. T.	

156.14

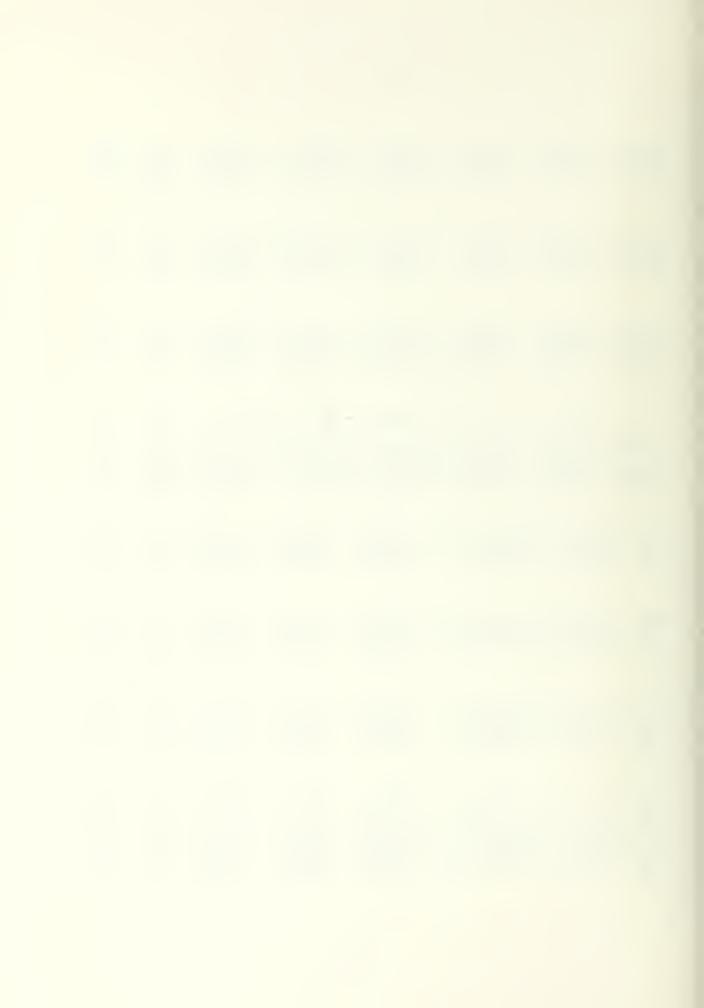
		92.75 143.66		399.66 317.91					393,60 31 42 143.44			46%.0% 36C.9%				156.15 156.15		84.59 144.59							5,52 134,59						59.01 156.15				493,41 422,84						101.22 174.59			
		•	102				•	215.30 155	~)			263.62 665				232.47 156	•		4						-19.67		4				p=4		-217.63								65.01 101			
	STRAIN A. IMECH.1	STRAIN R	E CONTRACTO	B ZOLV CINC			10.01	TEMPERATURE	STRAIN A. IMPOH.	STRAIN A.	STRAIN C.	DETAIL VIEW			21.13	TEMPERATURE	STRAIN DO CHECHAI	2	LONG. STRN.	PRINC. STRN. "		4	TEMPERATURE	TOUR A MAGNET	ATRACA B.	STRAIN C.	LONG. STRN. "	PRINC. STRV. *		24.00	TEMPERATURE	STRAIN A. (MECH.)	STRAIN B	S TOTO CTO	S PAIN COLEG		4 4 4			STRAIN A. CMFCH.		8 "ZOLV "CZC -	DATNE STRV. *	
43.67	287.36			145.20	203.67	63,66	143.67	283.67	287.68			155,20	213.66	83.67	153.67	283.66	Z88°01			155, 20	223.66	93.67	283.66	0 0	0			155.20	253.67	143.67	293.67	308.44			155.20	273.66	133.67	143.67	283.66	377.91			155,20	
192.75	336.91			154.24	192,75	-7.25	122.75	322.75	356.42			154.24	212.75	22.75	122.75	312,75	16.616			154,24	252.75	42.75	1920 75	356-30	25 % 20			154.24	262.75	122.75	342.75	363.99			154.24	312,75	82.75	112.75	342.75	376.76			154.24	
-1391.02	-1830.20			150.07	-1649.29	-1236.02	-1237.68	-1206.02	-1719.56			159.97	-1311,56	-910.50	-942,16	-913.50	A105/51-			168.55	-1282.46	-R28.63	-828-63	CD * 620 - 1 - 1 - 1 - 1 - 1 - 1	C+ *01 C T-			174.28	-1037,94	-543-00	-510.23	-1111.98			167.63	-537.84	53.19	-157.90	53°19	-549.66			197.17	
STRAIN R STRAIN C	PRINC. STRN. "		4	TEMPERATION	STRAIN A. IMECH. 1	STRATU A	STRAIN C. "		PRINC. STRN			TEMPFRATURE	STRAIN A. (MECH.)		STRAIN C	LONG. STRN. *			13.00	TEMPERATURE	I ME	STRAIN 9	LONG. STRM. "				14.07	TEMPERATURE	STRAIN A. (MFCH.)	ء ۽		PRINC. STRN. "		***	TEMPFRATURE	STRAIN A. IMECH. !			LOWG. STAN. W	PRINC. STRN.		17.03	TEMPFRATURE	



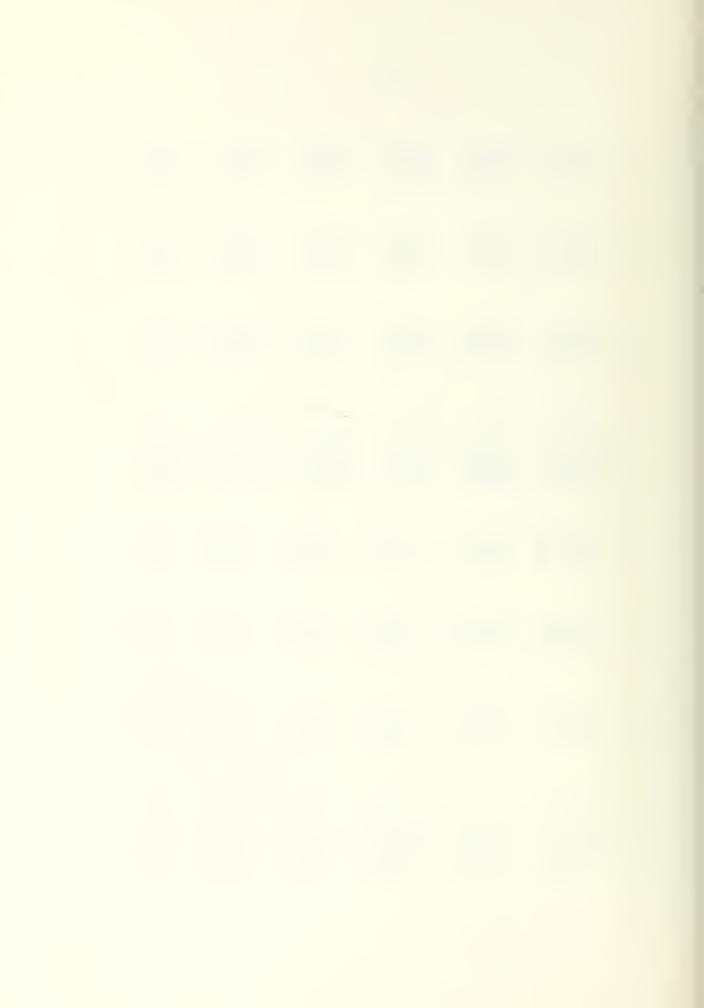
364.90	181.91 131.75 131.75 161.75 311.75	186.68 267.23 167.23 157.23 277.23 297.38	190.50 261.72 161.72 191.72 251.72	195.27 177.46 137.46 207.46 207.46	198.13 266.97 199.97 146.99 210.97 241.80	191.45 252.86 202.86 192.86
28.05 199.05 197.90	221.98 192.10 72.10 12.10 132.10	224.84 146.05 80.05 6.05 116.05 197.23	2266.75 1978.84 978.84 -2.16 97.84 197.84	2227 196° 6A 196° 6B 10° 5B 196° 6B	227, 70 218,68 98,69 -1,32 118,68	194.31 256.37 66.37 46.30
-1552.11 -2153.69 -2141.11	-1479.25 -1470.37 -1771.07 -2267.37	289.71 -1512.18 -2219.31 -2219.31 -2219.31	-2527- -2527- -17527- -1765- -2227- -	2746 -1598.45 -2189.00 -1796.00	240.653 -1620.65 -2201.10 -1757.67 -221.17	205.76 -1751.63 -1846.61 -1751.62
STRAIN C	PEMPERATURE ATRAIN A. IMECH.) ATRAIN B. CARAIN C. CARN. C. CARN. C.	TEMPFRATIRE STRAIN A. (MFCH.) STRAIN R. (MFCH.) STRAIN R. (STRAIN C. (TNG. STRN. MPRING. STRN. MPRING.	TEMPERATURE STRAIN A. (MFCH.) STRAIN A. (MFCH.) STRAIN G (INV., STRN	TEMPERATIRE STRAIN A. (MFCH.) STRAIN B. (MFCH.) STRAIN B. (MFCH.) STRAIN C. (STR.) STRAIN C. (STR.) STRAIN C. (STR.)	TEMPERATION TEMPERATION TERM A. (MECH.) TERM A. (MECH.) TERM C I DWT. STRV	TEMPERATION STRAIN A. (MFCH.) STRAIN A. (MFCH.) STRAIN G
100	9889 9889 9889 9889 9899 9899 9899 989	158.c6 336.45 206.45 206.45 446.45	160.42 319.33 99.33 219.30 439.30 446.93	164.74 313.17 103.17 213.17 423.17 430.60	166-51 308-14 106-14 168-14 366-14	175.23 264.30 114.30
-33.86 106.14 426.14 443.12	233.0 233.0 233.0 126.0 36.0 36.0 36.0 36.0 36.0 36.0 36.0 3	183.62 203.92 203.92 -180.08 93.92 93.92		199.08 192.18 22.15 72.15 242.15	207.67 169.02 39.02 203.02 203.02	2000 2000 3000 3000 500 500 500 500 500 500 50
- 785. - 785. - 786. - 786. - 881.	309.75 -406.57 -1177.12 -522.67 -1177.02	311.65 -483.17 -1335.35 -61.63 -1335.35 -1424.29	315.47 -732.43 -1645.48 -975.67 -1646.58	314.57 -915.27 -1675.40 -1255.40 -1625.40	311.65 -111.41 -703.67 -1304.38 -203.65	376.88 -1267.15 -2153.69
STAIN R. STAIN C. CLONG. STRN. W	AC. C.) TEMPERATURE STRAIN A. INFCM.) STRAIN A. STRAIN C. STRAIN C. STRAIN C.	FRAPFRATUAF STRAIN A. (MFCH.) STRAIN B. (MFCH.) STRAIN B. (MFCH.) STRAIN B. (MFCH.) I DNG. STRN. B.	SPACTION STANDS	TEMPERATURE STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN A. (MECH.) ION: STRA	TEMPERATION STRAIN R. (MFCH.) STRAIN R. (MFCH.) STRAIN R. (MFCH.) STRAIN S. (MFCH.)	AP. 13 TEMPERATURE STRAIN A. [MECH.] STRAIN A



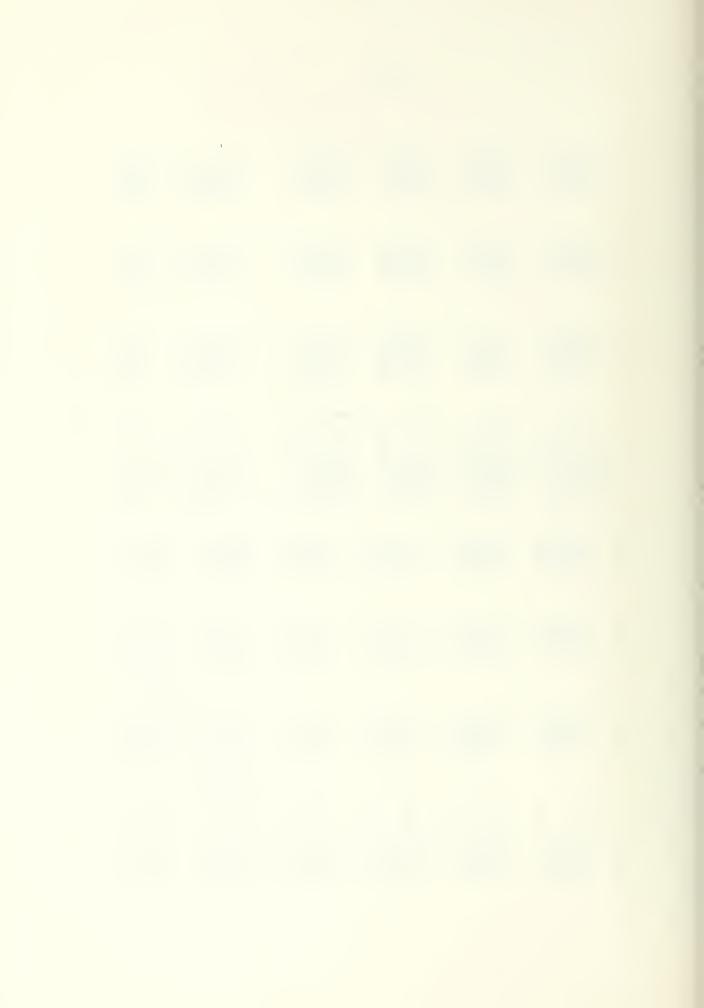
395,14 125,14 195,14 419,15	1656 1656 1656 1656 1656 1656 1656 1656	1000 05 4000 14 3100 14 3100 14 1100 14 500 16	166.65 575.14 275.14 - 14.86 215.14 526.74	1000 9300 9300 1000 1000 1000 1000 1000	2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	166.65 525.14 225.14 395.14 429.68
363.17 163.17 163.17 363.55	164.74 433.17 913.17 -6.83 113.13	2830 2830 2830 2830 1430 1230 521 521 521 523	164.74 633.17 233.17 -146.83 603.20	164.74 623.17 223.17 -166.83 253.17	164.74 623.17 173.17 -156.83 293.17 627.76	166.74 613.17 143.17 425.14
114346	271. 957. 451.	- 1868.55 - 1868.55 - 2105.68 - 1705.68 - 2105.68	166.95 -1356.94 -2156.79 -1165.27 -2156.79	169.91 -189.51 -186.61 -970.82 -186.61 -2467.12	160.51 -130.71 -151.37 -64.17 -194.32	169.51 -1234.67 -527.54 -527.94 1476.61
STRATE P. STRATE P. CONTRACTOR	ig.	TEMPERATURE STRAIN A. (MECM.) STRAIN C. LING. STRN	TREOFRATURE STRAIN & CMECKO, STRAIN & CMECKO, STRAIN CO, I DAG, STRAN, PRING, STRAN, PRING, STRAN,	TRAPERATURE STRAIN A. (RECM.) STRAIN A. (RECM.) STRAIN A. (RECM.) STRAIN C. RECM.)	TEMPERATURE STRAIN & INCC. STRAIN & INCC. STRAIN C. STRAIN C. STRAIN C. STRAIN C.	P1.07 TERPERATURE STRAIN A. (MECH.) STRAIN R. LONG. STRN PRING. STRN
152.86	177.14 276.40 186.40 106.40 196.40 276.55	170.46 274.15 174.15 100.15 200.15 200.15	1000 1000 1000 1000 1000 1000 1000 100	166.6 195.16 195.16 195.16 172.16	1 1 2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	166.65 365.14 -14.86 265.16 526.80
200° 000° 000° 000° 000° 000° 000° 000°	255.25 255.25 255.25 255.25 255.25 255.25 255.25 255.25	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1640-74 2130-17 2130-17 2030-17 320-93	1000 1000	200 200 200 200 100 100 100 100 100	164.74 34%.17 -116.83 353.17
-1846.61	181.91 -1721.62 -1721.62 -1707.91 -1721.62	173.32 -173.52 -1697.86 -1798.41 -1697.86 -1730.38	160.55 -1324.68 -1725.73 -1725.43 -1725.56	168.55 -1324.65 -1725.73 -1472.43 -1732.43	168.55 -1324.68 -1736.29 -1472.43 -1736.29	166.55 -1303.57 -370.79 -577.54 -1494.56
LOMG. STRM. "PRINC, STRW. "	BRD. CT TEMPERATURE STRAIN A. (MFCM.) STRAIN A. STRAIN C. LING. STRN. W.	0 4 4 4 7 7 Y	C.03 TEMPERATINE STRAIN A. [MECM.] STRAIN A. [MECM.] STRAIN A. [MECM.] STRAIN A. [MECM.] PRING, STRN. B.	TEMPERATURE STRAIN A. IMFCH., I STRAIN B	P.(7) FEMPRATISE STRAIN A. (MECH.) STRAIN R	FEMPRATURE STRAIN A. (MFCH.) STRAIN C. (10%) STRN. W PATKC. STRN. W



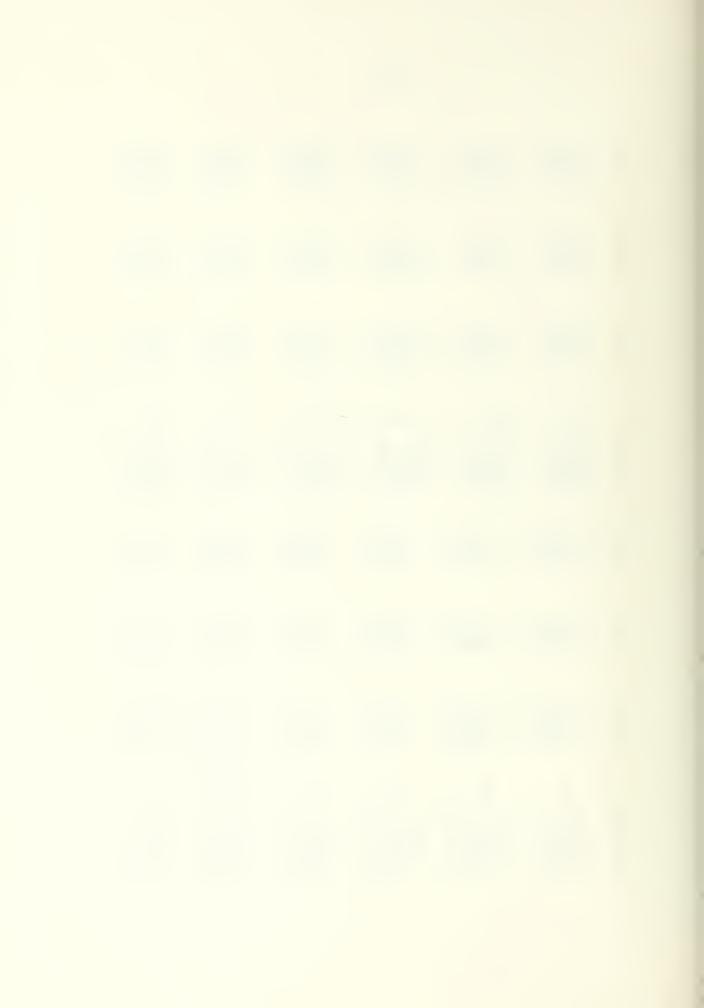
167.60 356.13 206.14 236.14 386.14 404.30	167.60 336.14 226.14 256.14 356.13 376.13	167.60 246.14 246.14 276.14 366.14 373.22	167.60 136.14 255.14 276.14 356.14 364.44	166.95 327.14 257.14 277.14 357.14 357.14	171.42 320.17 270.17 270.17
1700 1700 1700 1700 1700 1700 1700 1700	175.23 264.30 204.30 204.30 304.30 304.30	286 286 286 286 286 286 286 286 286 286	187.63 228.35 268.35 228.35 188.35 268.35	196.22 286.63 286.63 216.63 218.63 288.77	203.85 195.14 316.14 206.14 86.14
320.24 11410.24 -220.40 -221.40 1146.47	338, 37 666, 63 -729, 93 166, 27 -729, 95	- 10 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	357,77 476,77 -1460,96 -200,56 -1460,96	351.72 94.75 -1752.21 -1752.60 -1793.63	349.81 -21.51 -1952.93 -900.07
TEMPERATURE STRAIN A. SMECH.) STRAIN B. STRAIN C. STRAIN C. PRINC. STRW. "PRINC.	TEPFRATURF STARTA A. (MECH.) STARTA A. (MECH.) STARTA C STRAIN C INNG. STRA PRINC. STRA	TEMPERATURE STRAIL A. (MECH.) STRAIL A. (MECH.) STRAIL A	45.00 TEMPERATURE STAAIN A. (MECH.) STAAIN C	FERPERATURE STRAIN A. (RECH.) STRAIN A. (RECH.) (INAIN C	FERFERATIRE STRAIN & (MECH.) STRAIN B. STRAIN C. I GNG. STRAIN C.
166.65 525.14 215.14 5.14 315.14 315.14	166.65 189.14 89.14 89.14 99.14 90.06	166.65 475.14 175.14 75.14 375.14 498.75	166.65 445.14 175.14 125.14 395.14 479.30	14 11 11 14 14 14 14 14 14 14 14 14 14 1	1866 385 1955 1955 186 186 186 186
11266 11266 11266 11266 1136 11637 611637	1066 806.16 106.16 86.15 86.15 866.20	10000000000000000000000000000000000000	166.15 166.15 166.15 166.15 166.15	165569 416415 166415 166415 466415 48722	166,65 375,14 175,14 225,14
100.01 -750.64 167.46 16.64 -846.76	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	221.98 1140.81 921.17 117.92 922.17	251,55 157,61 782,05 1464,7 782,05	277.31 1590.23 570.45 1277.56 577.56 1630.18	297.34 1391.13 785.94 968.96
TEMPERATURE STRAIN B. (MECH.) STRAIN C. STRAIN C. B.	TEMPERATURE STRAIN A. (MFCH.) STRAIN A. (MFCH.) STRAIN C. TRE.	TERREATINE STRAIL A. (AECH.) STRAIL B. (AECH.) STRAIL C. B. STRAIL C.	TEMPERATURE ATRAIN A. (MFCH.) STRAIN A. ATRAIN A. I CAG. ATRA. PRILC. ATRA.	79°CA STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN B. THAIN. STRAIN.	TEMPERATION TEMPERATION AND ALL AS CRECHS ATRAIN C. S



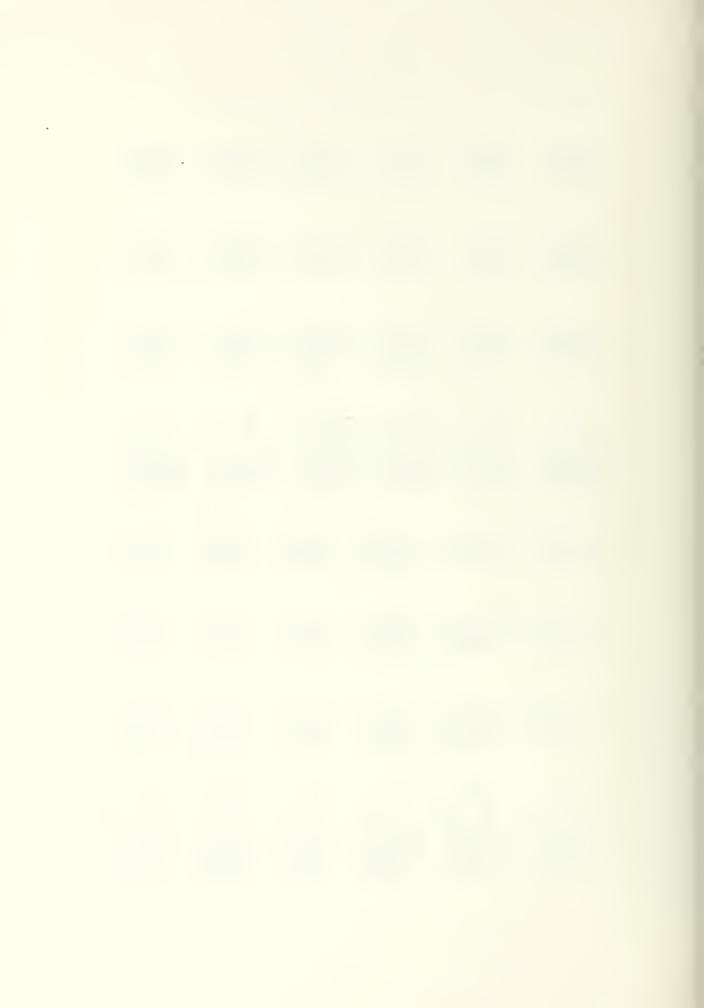
	206.71 291.79 361.79 191.79 121.79	212. 289.25 389.25 159.25 59.25 401.59	200 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1700.00 19090.15 19090.15 1909.15	100 000 000 000 000 000 000 000 000 000	169.51 378.14 516.14 218.14
	2845.24 846.24 846.24 196.25	2288 2888 2869 500 500 600 600 600 600 600 600 600 600	207. 203. 363.02 163.02 93.02 37.85	166.55 337.14 337.14 227.14 187.14 391.91	386 386 386 396 306 306 306 306 306 306 306 306 306 30	166.65 385.14 575.16 295.14
	277.31 -1276.51 -2405.80 -1635.45 -2415.80 -2442.14	247674 -14146.00 -22936.0 -17938.40 -22956.0 -22956.0	217.21 -1347.47 -2635.49 -16536.49 -2035.49	171,42 -125,41 -175,22 -146,26 -175,22	173,46 -04%,15 -187%,05 -137%,05 -187%,05	173.46 -849.15 -1893.68 -1376.85
	TREPERATION CTEATOR CHAINS CTEATOR A. CARCHAIN C	THEFFE TIME STRAIN A. (MFCK.) ATRAIN A. (MFCK.) ATRAIN B. B. ATRAIN B. ATRAIN B. ATRAIN B. ATRAIN B. PAINC. STRA.	TEMPERATURE STRAIN A. (MECH.) STRAIN A. (TRAIN B. (TRAIN C. (TRAIN	CHAROLA	PAKKS 11 C.C. TEMPERATURE STRAIN B. (MECH.)	TEMPORATURE STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN G
330.53	1 74° 28 3 23° 28 2 73° 28 2 73° 28 3 23° 61	180.00 379.59 279.59 249.59 249.59 330.82	186.68 377.23 297.23 227.23 237.23	1962 200-00 310-00 200-00 170-00 170-00	22002 2000 2000 2000 1000 1000 1000 100	204.81 289.85 359.85 189.85 119.85
316, 25	2111 2017.046 3917.049 177.049 8 8 8 7 7 9 9	221 1920 1920 1920 1920 1920 1930 1930	230.56 231.17 361.17 131.17 -28.83	236.29 105.02 375.02 115.07 106.03	238 2078 2076 1176 1176 1176 1176 1176 1176 1176 1	238°.20 227°.51 397°.51 117°.51 -52°.49
-1971-18	346.05 -252.06 -252.36 -171.67 -222.38		325° 1 -063° 01 -063° 04 -1663° 04 -1663° 05 -2651° 05 -2651° 06	11313131313131313131313131313131313131	295.39 -1217.56 -2487.61 -1682.73 -2487.61	265.40 -1312.17 -2652.57 -1662.17 -2662.57 -2662.57
PAINC. STRN. "	TEMPERATURE TYPAIN A. LWFCH.) TYPAIN B. TYPAIN C. PAINC. ATRN. B	TEMPERATURE STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN A. STRAIN	TEMPERATURE STRAIN A. IMFCH.) STRAIN A. IMFCH.) STRAIN B. IOND. STRN. B.	TEMPERATIRE ATRAIN A. (MECH.) ATRAIN A. (MECH.) ATRAIN C.	TREPERTORY ATRAIN A. LAFOTA ATRAIN A. LAFOTA ATRAIN C. S.	125.03 TRMPEARTURE STRAIN A. IMECH.) STRAIN A. STRAIN C. STRAIN C. STRAIN C. STRAIN C.



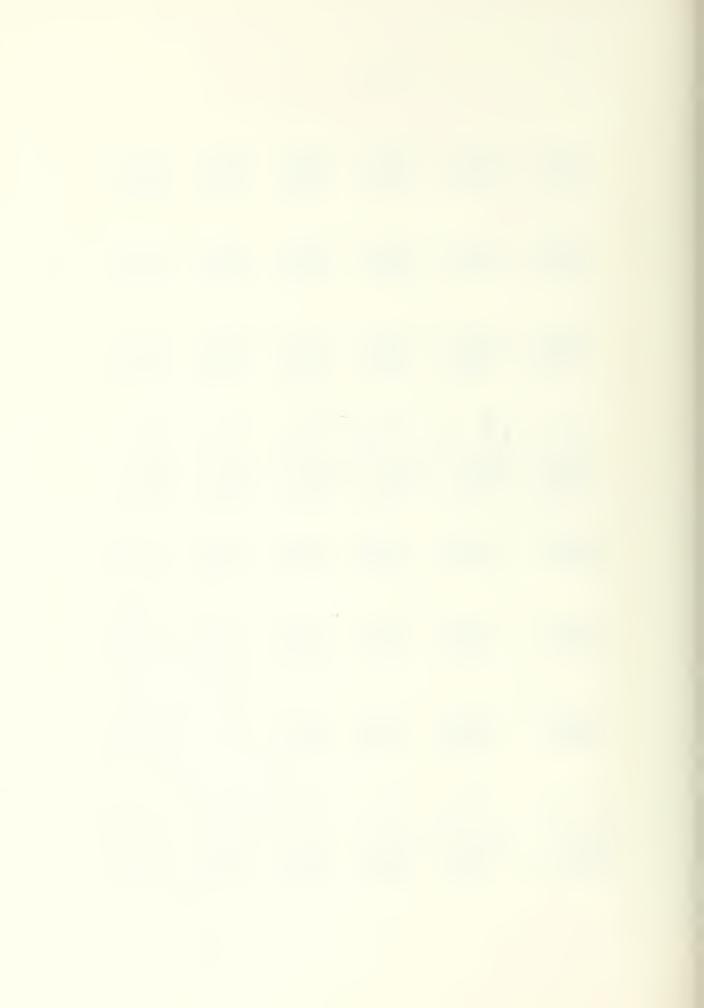
634.21	160.51 600.14 950.14 -550.86 160.14 617.70	16696 51 9706 114 9706 114 - 47.0 86 602.0 114 602.0 114	160.14 590.14 290.14 -20.06 290.14 910.14	169.51 488.14 2188.14 488.14 3188.14 4938.75	16001 21001 21001 21001 3000 3000 4100 4100 4100	169.51 399.14 218.14 158.14 158.14
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-2774.44	- 915- - 915- - 915- - 915- - 182- - 182- - 95- - 95-	190.50 -190.60 935.29 924.74 935.29	228.66 1895.55 71095.53 1895.03 2106.63	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	293.53 2541.08 1116.27 1517.33 1116.27 2676.14	2 2 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
PRINC. STRN. 8	10.27 FRMPERATURE STRAIN A. (MECH.) STRAIN A. STRAIN C. W. LONS. STRN. W.	PAPERATURE STARING STRAIN A. (WECH.) STRAIN C. STRAIN C. I ONG. STRN.	FEMPRATURE STRAIN A. (MECH.) STRAIN A. STRAIN B. STRAIN B. B. L'ANG. STRN. B.	FAMPERATURE STRAIN A. (MFCH.) STRAIN C. I DMG. STRN. PRINC. STRN.	PERPERATURE STRAIN A. (MFCH.) STRAIN R. B. STRAIN C. LONG. STRN. B. PRIMC. STRN. B.	TEMPERATURE STRAIN A. (MECN.) STRAIN C. CONG. STRN.
78-14-532-24	1666.51 1788.14 1788.14 1988.14 568.14 568.14	164.51 468.14 548.14 128.14 48.14 600.47	16.9.51 9580.14 9580.14 988.14 78.14 78.14	160,51 598.14 458.14 -21.86 118.14 641.70	164,51 608,14 418,14 418,86 148,14 635,06	186.51 616.51 886.14 191.86 178.16
105.14	1166 4185 4185 4055 4055 8455 8455 6466 6466	50 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	166.65 655.14 6455.14 145.14 125.14 786.67	166.65 765.14 575.14 -114.86 775.14 831.20	1000 000 000 500 1000 1100 000 000 1100 000 0	166.65 62.14 42.14 -23.46 165.14
-1830.68	117-66 - 817-66 - 1872-69 - 1872-76 - 1873-76	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	170.46 -595.85 -765.85 -1769.67 -1269.99 -7869.88	171.642 -558.61 -2476.66 -653.60 -2446.21	171-42 -2310-59 -2310-59 -2310-59 -2917-12	-11000-11 -17070-11 -161.083 -1707-683
LONG. STRN. #	FERFEATURE STRAIN A. (MECL.) STRAIN R. B. I DNG. STRN. B. PRING. STRN. B.	LC.O.) FEMPERIURE STRAIN A. (MECH.) STRAIN G. G. G. TRAIN C. G. TRN. FING. STRN. G. G. FING. STRN. G.	TEMPERATURE STRAIN A. (MECH.) STRAIN R. (MECH.) STRAIN C	TEMPERATURE STRAIN A. (MFCM.) STRAIN A. (MFCM.) I PMG. STRN. W.	TEMPERATURE STRAIN A. (MECM.) STRAIN B	TRMPERATURE STRAIN A. IMPCH.1 STRAIN B. W. STRAIN C. C. W.



183.82 303.82 403.92 263.92 163.92 405.83	195.27 297.46 437.46 237.46 97.46 97.46	205,76 270,57 480,57 210,57 0,57 482,44	213.39 270.31 300.51 190.51 539.49 53.46	206.62 284.26 514.26 194.26 -35.74 517.91	1964, 31 3064, 30 4966, 30 1966, 30 66, 30 50. 40
228.66 229.52 569.52 569.52 -130.48 569.66	239.15 226.27 596.27 176.27 176.28 -191.73	241.06 239.78 609.78 169.78 -237.22	235.33 265.19 605.19 165.19 -156.81 607.29	218.20 303.00 303.00 233.00 233.00 24.00 36.00 36.00	194.31 316.31 566.30 256.30 6.30 96.30
1337.41 -254.26 -2513.98 -1253.57 -2513.98	314.52 -R91.66 -2543.08 -1635.43 -2543.09	286.76 -968.77 -2499.11 -1739.22 -2499.11 -2499.11	261.09 -1061.88 -2361.14 -1706.79 -2361.16	225.79 -1046.47 -2184.32 -1984.32 -2184.32 -2299.34	200.04 -100.06 -2013.89 -2013.76 -2017.08 -2019.82
TEMPERATIRE STRAIN 8. INFECTA.) STRAIN C. INFECTA.) STRAIN C. INFECTA.) STRAIN C. INFECTA.) PRINC. STRN. INFECTA.	90.07 TEMPERATURE STRAIN A. IMECH. STRAIN B. STRAIN B. STRAIN C. LIMG. STRN. PRINT. STRN.	120.00 TEMPERATURE STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN C. III IONG. STRN. III	TEMPFRATURE STRAIN A. IMECH. STRAIN C. STRAIN C. LING. STRA.	TEMPERATURE STRAIN B. " " STRAIN B. " " STRAIN B. " " " STRAIN C. " " " " " " " " " " " " " " " " " "	SN6.07 TEMPFRATURE STRAIN A. (MECH.) STRAIN C. STRAIN C. LONG. STRN. PRINC. STRN.
166.51 366.14 228.14 198.14 338.14 364.36	169.51 336.14 268.14 268.14 339.14 352.64	160.51 908.14 298.14 298.14 308.14 310.21	169.51 308.14 328.14 308.14 288.14	11.00 900.00 9100.15 9100.15 900.15	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
11 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	175.23 266.30 366.30 316.30 276.30 316.30	1800.96 250.66 350.66 320.66 310.66	185.73 225.12 395.12 316.13 166.13	194, 31 226, 30 476, 30 306, 30 56, 30 480, 08	2100 2100 53 2200 74 2550 74 1550 20 1570 63
1991. 98 1991. 98 124.50 946.72 1998.13	4	354.56 1363.50 -1011.17 -1012.17 1304.45	1 3558 -1 3550 -1 3550	350, 35 654, 90 -1710, 77 -495, 49 -1710, 35	354, 36 -26, 31 -223, 12 -107, 17 -223, 64
TEMPERATURE STRAIN A. GRECH. I STRAIN B. CTRAIN B. B. CTRAIN C. B. B. CTRAIN C. STRAIN B. B. B. B. CTRAIN B. B. CTRAIN STRAIN STRAI	NA.C) TEMPERATURE ATMAIN B. [MECH.] STRAIN B. ATRAIN C. B. IONS. STRAIN BRING. STRA.	TEMPERATURE STRAIN B. (MECH.) STRAIN B. STRAIN C. B. STRAIN C. B. STRAIN C. B. STRAIN B. B. STRAIN B. B. STRAIN.	40.07 TEMPRATURE STRAIN A. IMECH.I STRAIN B. B. STRAIN C. B. L'DNS. STRN. B.	45° 27 FRAIN A. (MFCH.) STRAIN R. STRAIN C. STRAIN C. PRINC. STRN.	55.00 TEMPERTURE STRAIN A. INECM. I STRAIN R. 10MI. STRAIN C. PRINC. STRN.

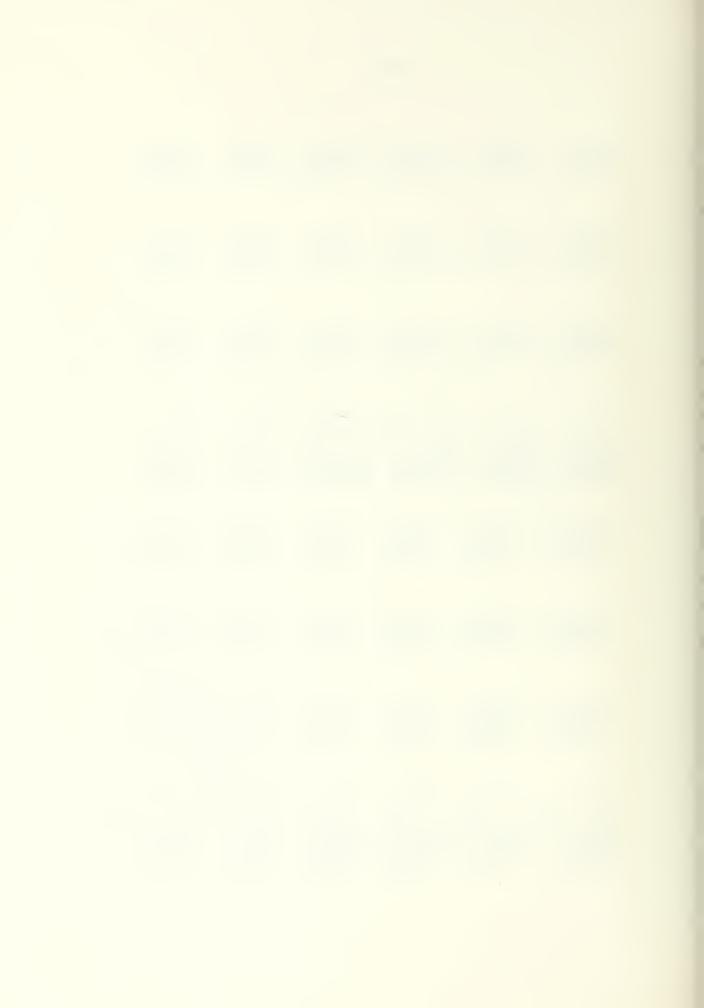


167.65 5 36.14 6 366.14 196.14 136.14 5 77.66	167.60 526.13 366.13 16.14 176.14 543.26	167.60 516.14 336.14 166.14 196.14	167.63 496.14 316.14 26.14 206.14 502.49	167.60 466.14 276.14 56.14 56.14 466.68	168.55 427.14 267.14 77.14 237.14
165.69 665.15 516.15 -5.85 116.15	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	165.60 616.15 826.15 -356.15 616.03	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	9 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	166.65 495.14 235.14 125.14 41.55.14
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TEMPERATURE STRAIN A. (MFCH.) STRAIN B. STRAIN C. (TAGIN C. (TAGIN C.) PRINC. STRN.	70.09 (ARC) TEMPERATURE STRAIN A. (MECH.) STRAIN B. STRAIN C. STRAIN C. FOMD. STRN.	TEMPERATURE STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN A.	TEMPFRATURE STRAIN A. (MECH.) STRAIN A. STRAIN C. STRAIN C. C. LUNG. STRA. C.	74.07 TEMPERATURE STAIN A. (MFCH.) STAIN A. (MFCH.) STAIN C (DMG. STRN PRINC. STRN	76.03 TEMBERATION STOATH A. (MECH.) STOATH G. S STOATH G. S STOATH G. S TOWN, STRU.
168.55 317.14 497.14 217.14 37.14 502.51	167.69 366.13 516.14 226.14 780.0	167.60 386.14 526.14 236.14 96.14 538.84	167.60 406.13 526.14 206.14 86.14 86.18	167 46.00 46.00 46.00 160.00 46.00 66.00 66.00	167.60 516.14 4.75.14 56.14 96.14
166.65 345.14 575.14 295.14 65.14 576.36	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	44444444444444444444444444444444444444	100 434 434 624 15 624 94 94 15 15 15 15 15 15 15 15 15 15 15 15 15	165 505 504 504 504 74 74 15 678 600	16.26.06.06.06.06.06.06.06.06.06.06.06.06.06
- 1 896 6 91 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 4 5 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	100 - 100 -	168.55 -133.65 -1264.66 -1264.66 -1974.11	1688-55 -1868-55 -1968-67 -1968-67 -2966-8
1620. CO TEMPERATURE STRAIN A. (HECH.) STRAIN C. (TNG. STRN. B PRINC. STRN. B	SEASON S	TEMPERATIRE STRAIN A. INECH.) STRAIN B. INCCH.) STRAIN C. INCCH.) LONG. STRN. INCOME.	FAMPEATIBE STRAIN A. (MFCH.) STRAIN A. (MFCH.) STRAIN C. MPCH.) FORM. C. MPCH.	TEMPERATURE STRAIN A. (MFCM.) STRAIN A. (MFCM.) STRAIN A. (MFCM.) STRAIN A. (MFCM.) CONG. STRN. MPRINC. STRN.	TEMPERATURE STRAIN R. (MECH.) STRAIN R. (MECH.) STRAIN R. (MECH.) STRAIN S. (MECH.) STRAIN S. (MECH.)

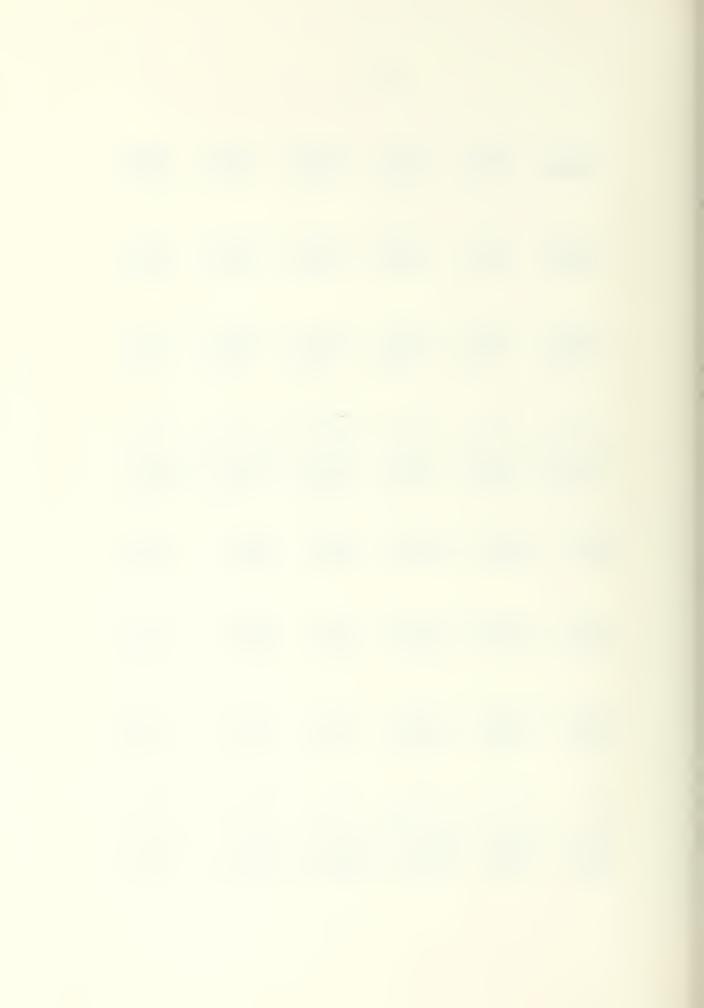


171.42 357.42 400.17 260.17 210.17	173.32 332.22 452.22 252.23 185.22 409.27	177. 336.43 416.40 236.40 156.40 425.69	182.86 312.83 422.83 222.83 112.83	189,54 310,59 450,59 210,59 70,59	193.36 3753.26 475.15 195.15 25.15 481.78
185.73 326.12 496.12 396.13 136.13	1992 1992 1992 1994 1995 1995 1995 1995 1995 1995 1995	1999, ne 302, 15 542, 15 262, 15 762, 15 762, 15	206.71 291.79 561.79 241.79 -26.21	211.48 297.99 577.99 227.99 -527.99 579.93	2011.048 2012.090 227.090 227.090 570.01
254.41 -394.13 -176.72 -176.72 -176.72	- 555° - 28 - 1999 - 73 - 1917 - 74 - 1999 - 73	257.28 -694.35 -2076.94 -1866.80 -2076.94 -2016.94	253.46 -2151.50 -2151.50 -2151.50 -2151.59	246.78 -932.34 -2211.05 -1651.68 -2211.05	241.06 -977.49 -222.98 -1695.17 -2222.88
TEMPERATURE STRAIN A. (RECH.) STRAIN S. (ARCH.) STRAIN C. STRN. SPRINC. STRN.	TFAPFRATURE TRAFTS A. IMECH.) STRAIN C. STRAIN C. B. STRAIN C. B.	TEMPERATURE STRAIN R. (MECH.) STRAIN R. STRAIN C.	TEMPERATURE STRAIN A. (MECH.) STRAIN G. MECH.) STRAIN C. M. I DNG. STRN. M. PRINC. STRN. M.	TEMPERATURE TEMPERATURE TEMPERATURE TRAIN R. AFCH.) TRAIN R. B. TING. STRN. B.	TEMPERATURE STRAIN R. (4ECH.) STRAIN R. STRAIN C. TRAIN C. TRAIN C. TRAIN C. TRAIN C. TRAIN C. TRAIN C.
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2000 2000 2000 2000 2000 2000 2000 200	3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	186.55 317.0 317.0 347.0 347.0 347.0 346.0 346.0 346.0 346.0 346.0 346.0 346.0	171.42 311.17 450.17 360.17 220.17	1174 - 28 325.26 485.26 365.26 265.26 486.66	1805.96 1937.666 407.666 186.67 186.67 400.74
166,73 -736,64 -1175,66 -1177,66			235.33 -235.33 -1444.31 -978.82 -1466.31 -1460.27	243.92 -245.34 -1530.36 -1534.91 -1575.16	251.55 -926.12 -1698.15 -1167.66 -1406.22
POS.)) TEMPFRATURE STRAIN R. RECM.) STRAIN R. R. STRAIN C. R. LONG. STR. PRINC. STR.	FAMPRATURE STARIN A. (MFCH.) STARIN A. (MFCH.) STARIN C. B. COMS. STAN.	STRAIN A. (MFCM.) STRAIN A. (MFCM.) STRAIN B. B. STRAIN B. B. LONS. STRA.	45.00 TEMPERATURE STRAIN A. IMECH.) STRAIN C. STRAIN C. C.	90.00 FFFFFATINE STRAIN 9. (MECH.) STRAIN 9 STRAIN 9 LONG. STRN PRINC. STRN	SE, DO TEMPESATURE STRAIN A. (WECM.) STRAIN A. STRAIN C. DNG. STRN.

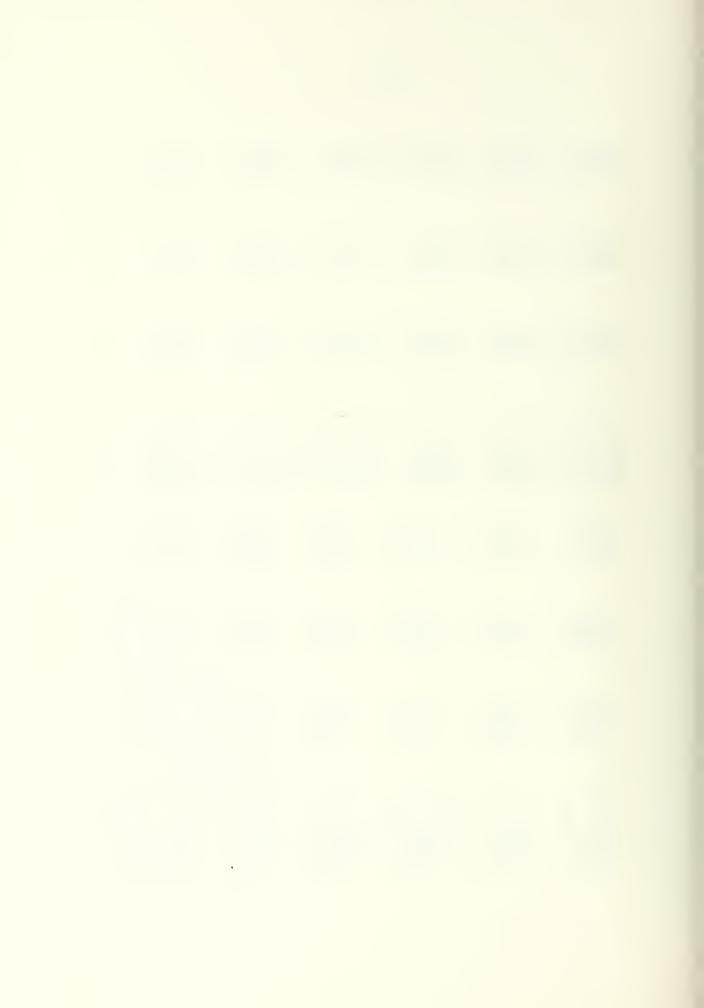
970



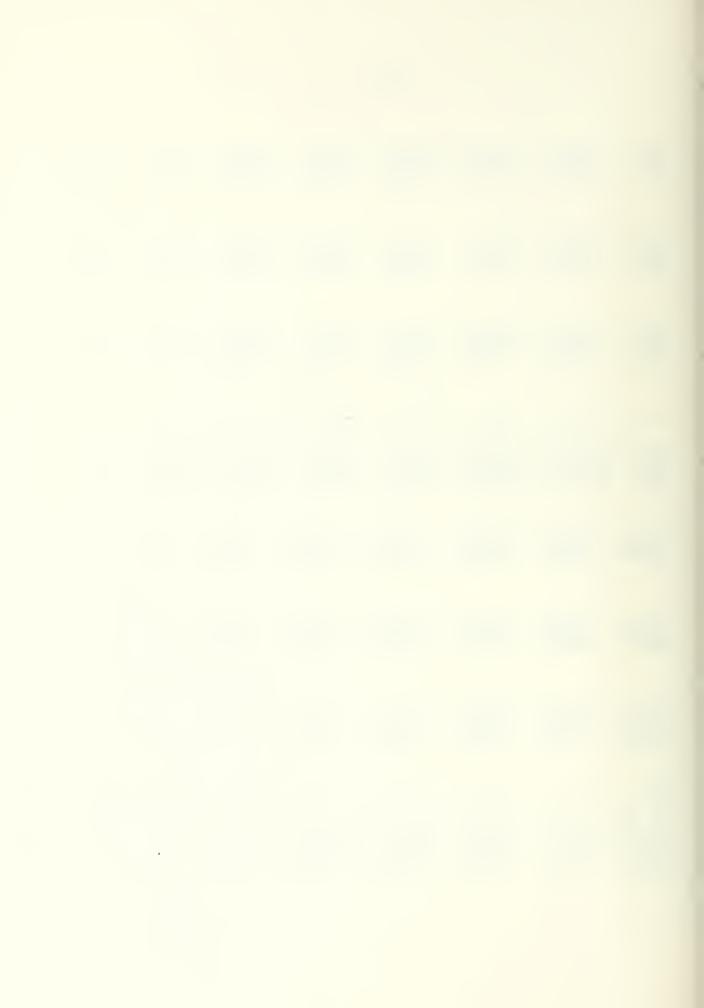
1715-42 190-17 540-17 250-17 80-17 870-1	171. 460.17 460.17 200.17 100.00	171.42 640.17 660.17 170.17 190.83	171.42 530.17 660.17 120.17 -0.63 717.92	171.42 570.17 690.17 60.17 0.17	172.37 601.20 991.20 81.20 31.20
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TEMPERATURE STARIN O. (MECH.) STRAIN O. (MECH.) STRAIN C. O. (LOMG. STRA.)	FERPERATIRE STRAIN B. (AECH.) STRAIN G. B STRAIN G. B CING. STRA.	TEMPERATURE STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN C. B. (TRAIN C. B.	TEMPERATURE STRAIN & (MCCM.) STRAIN & (MCCM.) STRAIN & B.	15.07 TEMPERATURE STRAIN A. (MECM.) STRAIN C. M. LINGS STRN. W.	TEMPERATURE STRAIN A. (MCCH.) STRAIN A. (MCCH.) STRAIN C. STRAIN C. ELDMG. STRN PRINC. STRN
	1	11 146 3186 3186 666 1866 52 1866 54 84 84 84 84 84 84 84 84 84 84 84 84 84	165.60 104.15 174.15 174.15 695 605 805 805 805	1946 1876 1876 1898 1898 1899 1999 1999 1999 1999 199	171 380.17 860.17 290.17 -29.83
200° 200° 200° 200° 200° 200° 200° 200°	189.54 337.59 757.59 775.99 -170.41	177.14 326.40 586.40 286.47 26.47 587.11	163.78 312.19 972.19 272.19 12.19 572.91	151.36 355.03 610.03 850.03 60.03 611.12	1 4 8 6 1 1 4 8 6 1 1 4 8 6 1 1 4 8 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
216.75 -275.84 -2765.12 -2765.14 -2767.71	1966. 22 -1956. 85 -1956. 85 -1956. 85 -1956. 85	1881	1 65.00 34 1 1 65.00 34 1 1 65.00 34 1 1 1 65.00 34 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	154,24 -18079,44 -13079,44 -1307,44 -1309,44	- 1
TEMPERATURE STRAIN A. (MECH.) STRAIN B. STRAIN B. STRAIN STRN. B. FRINC. STRN. B.	TEAPFRATURE STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN A. (MECH.) FRAIN A. B. B. C. B. C. C. B. C. C. C. B. C.	FRANCE A (MFCHa) A TRAIN A. (MFCHa) A TRAIN G. B I TANG. STRN. B PRINC. STRN. B	TEMPERATURE STRAIN A. (MECH.) STRAIN G. B. TRAIN G. B. 1 JNG. STRN. B.	PEMPERATURE STRAIN R. (MECH.) STRAIN R. STRAIN C. LONG. STRN. W. PRING. STRN.	D. D. D. STEADER ATURE STRAIN A. (MFC M.) STRAIN C. M.



172.97 431.20 341.20 231.20 231.20 441.28	172.37 371.19 351.20 231.20 231.20 391.19	172.37 331.10 391.20 281.20 394.80	172.37 261.20 491.20 331.20 101.20	172,37 311,29 491,20 371,26 191,29	172,37 311,27 531,27 531,27 36,27 14,20 532,79	173.32
171-42 430-17 320-17 390-17 430-29	1171. 347.152 347.17 347.17 240.17 340.17	173.32 312.22 462.22 462.22 471.46	175, 23 274, 30 574, 30 644, 30 1444, 30 590, 49	180.96 280.66 660.66 460.67 81.47 67.63	189% 54 280% 59 720% 59 420% 59 -110% 41 727% 16	195.27
235. 235. 235. 255. 176. 176. 176.	2557 9995 1992 1992 1992 1993 1993 1993 1993 1993	273.649 1065.67 -475.02 375.09 -475.09	10540 10540 10540 10540 10540 10540 10540	299.25 790.75 -1352.72 -170.67 -1358.44	1000 1000 1000 1000 1000 1000 1000 100	304.98
TEMPERATURE STRAIM B. (MFCM.) STRAIM B. STRAIM C. CONT. STRA. PRINC. STRM.	TEMPERATIRE STRAIN AS IMPCM. I STRAIN B. STRAIN C. IONG. STRN. B. BRING. STRN.	TEMPERATIME STRAIN & MECH.) STRAIN & MECH. STRAIN C. MECH. LING. STRN. MECH.	THEFATURE TRAPERATURE STRAIN A. INFCH. STRAIN C	42.C) TEMPERATURE STRAIN A. IMECH.) STRAIN B. STRAIN B. C. B. LONG. STRU. B. PRINC. STRU.	TEMPERATURE STRAIN A. IMFCH. I STRAIN B. STRAIN C. STRAIN C. STRAIN C. B. STRAIN C. B. PRINC. STRW.	55, no Temperature
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11 40 00 00 00 00 00 00 00 00 00 00 00 00	170.46 824.15 629.15 -110.85 86.15	170.46 839.15 539.15 -170.84 1490.84	171.42 763.17 560.17 -109.83 93.17 919.59	171.42 640.17 360.17 -19.83 263.17	171-42 510-17 310-17 310-17 310-17	
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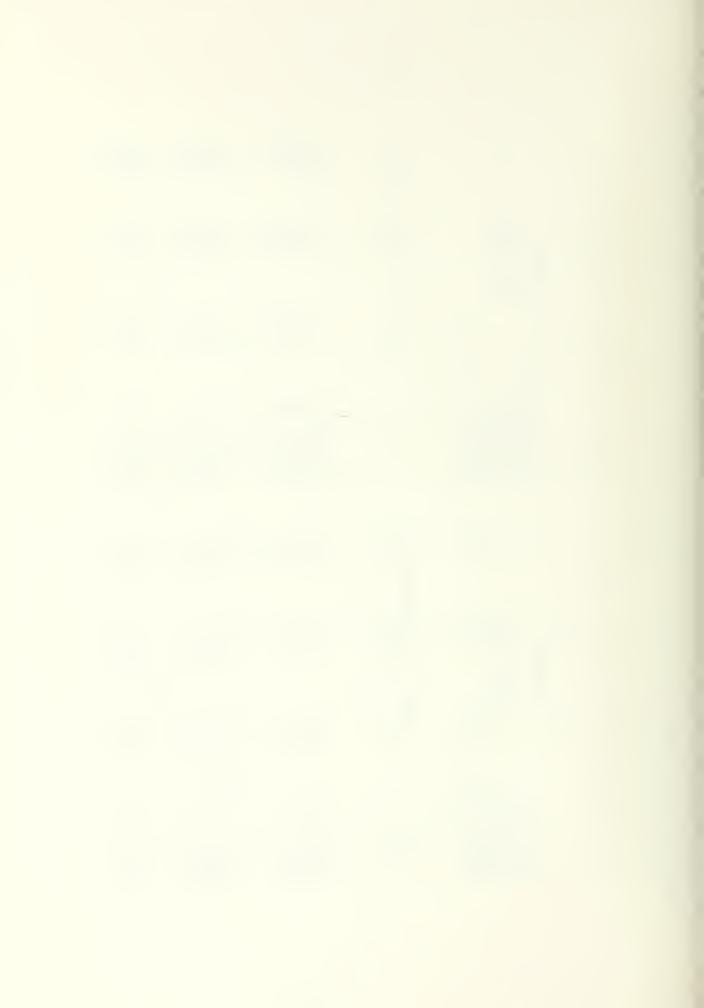


613.34 233.34 - 86.66 614.62	202.90 296.93 616.93 226.93 -936.93 618.65	2006.81 2006.35 530.35 220.35 -110.98 640.98	2000 2000 2000 2000 2000 2000 2000 200	1188.49 226.647 226.647 1.006.547	174.28 353.26 263.26 253.26 -56.74	24 00 00 00 00 00 00 00 00 00 00 00 00 00	-56.34
817.84 267.84 -242.16 818.21	2255.79 336.99 816.99 276.99 -235.01	223.89 324.73 814.73 284.73 -205.27 615.12	200.62 344.26 804.26 304.26 -155.74	188,59 379,47 799,47 739,47 739,47 183,53 799,92	172.37 391.20 391.10 371.10 -58.87	153,29 301,03 601,03 601,03 361,03 361,03	-58.16
-2418.33 -1552.87 -2419.33	- 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	257.60 -669.34 -257.98 -1570.98 -2577.98	227.17 -697.65 -2185.77 -2185.77 -2186.93	196.22 -666.15 -2049.84 -1427.15 -2049.84	177.14 -525.18 -1907.77 -1205.63 -1917.77	157,11 -57,11 -1055,09 -1055,01	-1856.01
STRAIN G. STRAIN C. LINGS STRN.	140.00 FEMPERATURE STRAIN A. (MFCH.) STRAIN C. TPAIN C. LONG. STRN.	TEMPERATIRE STRAIN A. IMECH., STRAIN A. IMECH., STRAIN C. INC.	TEMPFRATIRE STRAIN A. (MFCH.) STRAIN A. (MFCH.) STRAIN A. (MFCH.) LINEN C	537.07 TEMPERATURE STRAIN A. (MECH.) STRAIN A. STRAIN C. I DNG. STRN. W PRINC. STRN. W	TEMPERATIRE STRAIN R. (MFCH.) STRAIN R. (MFCH.) STRAIN R. (TRAIN C. (MFCH.) STRAIN C. (TRAIN C. (MFCH.) STRAIN C. (TRAIN C. (MFCH.)	u E	I UNG. STRN. "
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28 29 29 29 29 29 29 29 29 29 29 29 29 29	2001 3004 79 7654 79 1654 73 1644 27	216. 53 296. 74 776. 74 336. 74 -143. 26	217.21 295.61 785.61 315.61 -174.39	222. 93 293.41 803.41 283.41 -226.59 803.43	225, 79 336,99 886,99 286,99 -225,01 817,38	226.75 337.86	
252.35 -1921.76 -613.09 -1921.79 -1946.16	35.45.26 -2101.22 -855.83 -2119.22	301.16 -212.62 -2217.90 -1146.38 -2217.99	296,48 -355,91 -2382,29 -1256,56 -2382,29	284,94 -2436,36 -2436,31 -1433,67 -2436,31 -2436,83	279,22 -674,62 -263,81 -1613,94 -2563,82	765.86-602.99	
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POST.OD TEMPERATIME						
	154.24	150.43	152.34			
• 1	-1863.31	809.13	690.93			
STRAIN CO.	-1863.31	-50.86	-49.07			
•		80%.25	654.48			
2357.10			6			
TEMPERATURE	152.34	167.51	150.14			
CTEATE A. CHECHO!	-1461-71	605.81	649.14			
		375.81	249.14			
		-44.19	-40.86			
	-1644.18	805.84	653.49			
2700.03	***	10.1	143,75			
THE MAN TO SECURE	147.13	150.17	331.45			
	-1828.05	779.37	621.45			
		349.37	241.45			
	-1826.05	-70.63	-48,55			
	-1629.37	779.40	624.46			
10000.03	000	117.99	110.00			
CTDAIN A. CHECH.	-107.92	349,34	360.28			
CTDATE A. B	-786.41	769.04	640.28			
STATING.	-487.34	379,04	240.28			
LOWG. STRN. "	-785.41	-67.96	-39.72			
PRINC. STRN. "	-794.53	769.31	645.53			
COMPLETIME. 0.76	SEC.EXECUTION TIME=		8.87 SEC.OBJECT CODE	8144 BVTES, ARRAY AREA.	7992 AVTES, UNUSED.	83864 AYTES
				4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	SAC BANKE CHANGED	RIBBA BYTES
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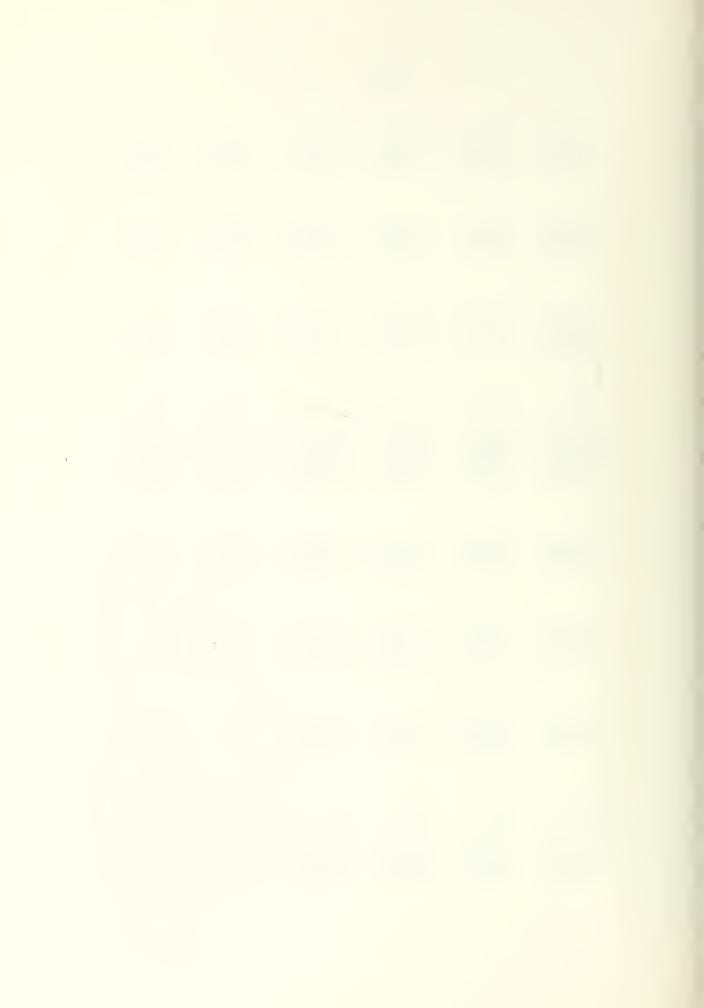
L RESULTS		WELD. 2.5		00000000000000000000000000000000000000	59.19 -29.73 -20.73 -20.73 50.27 51.27	43.14 -34.73 -34.73 50.27 60.27
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RESULTS		M WELD.		( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( (	C F F F F F F F F F F F F F F F F F F F	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
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RATURE VARIATIO	·	TRANSVFR		6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	-43.26 -43.26 -63.26 -63.26 -113.26 -114.00	1111.31 -43.26 -5.74 -63.26
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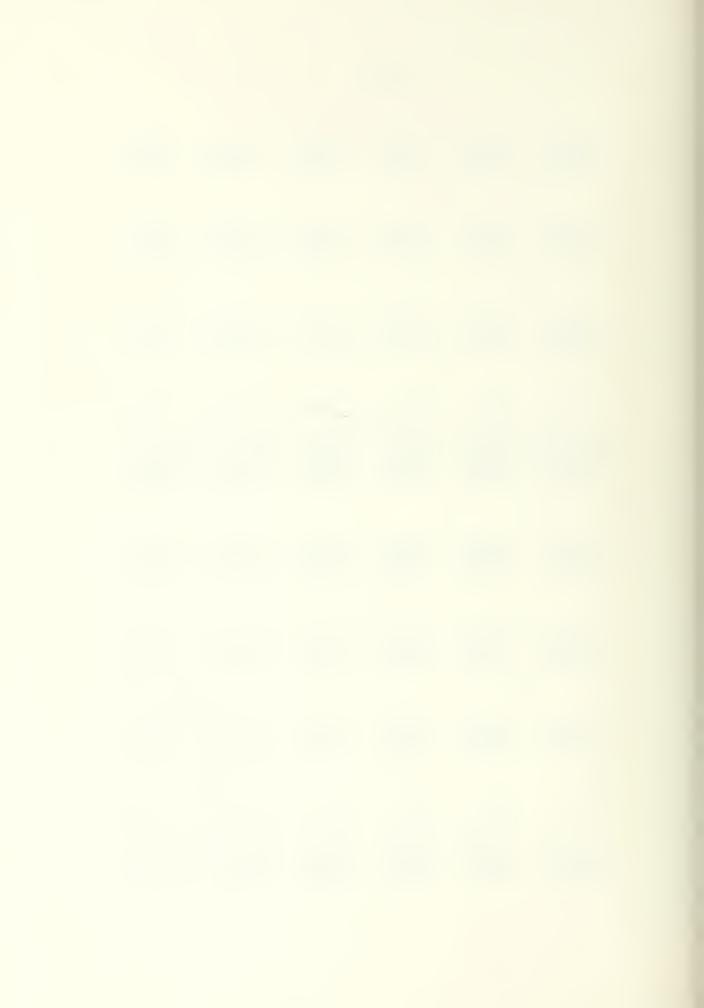
64.30	63.19 -70.73 -90.73 -90.27 100.27	63.19 - 99.73 - 120.27 130.27 170.27	63.19 -190.73 -190.73 -150.27 -160.27 -259.25	93.19 - 899.73 - 89.73 - 170.27 - 167.27 - 27.27	63.19 - 690.73 - 690.73 - 600.73 - 600.73 - 600.73	63.19 -699.73 -590.73 -180.27 -212.37
-73.28	56.91 -57.67 -57.67 -52.87 -119.87	640-61 -1470-97 -1470-97 -1470-97 -1470-13	58.91 - 57.87 - 147.87 122.13 172.13	94.31 -57.657 -147.657 142.13 192.13	58.91 -57.67 -137.67 -137.67 -197.13 -197.13	. 64.007 194.007 195.013 24.007 24.007
-71.72	1055 -946-73 -946-73 -96-73 -100-685	1099-45-46-49-45-49-49-49-49-49-49-49-49-49-49-49-49-49-	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	105.59 -194.73 -45.27 -205.27	10% 55 19% 55 19% 23 21,023 22,023	1050-95 -1740-73 -1740-73 2250-27 2250-27 2250-27
DRING. STRN. B	10°CO TEMPERATURE STRAIN BO BECTO STRAIN CO BECTO LCRG STRNO BE	TREPERATURE STRAIN B. (PECT.) STRAIN B. (PECT.) STRAIN C. (PECT.) LONG. STRA.	TEMPERATURE STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN C. LUNG. STRV.	19.00 TEMPERATURE STRAIN B. (PFCP.) STRAIN B. (PFCP.) STRAIN C.	70.00 (ARC PASSES) TEMPERATURE STRAIN B. (MECH.) STRAIN C. STRAIN C. LCAG. STRN.	72.0C TEMPERATURE STRAIN A. (MECH.) STRAIN G LCNG. STRN
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98.00	######################################	2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	11346	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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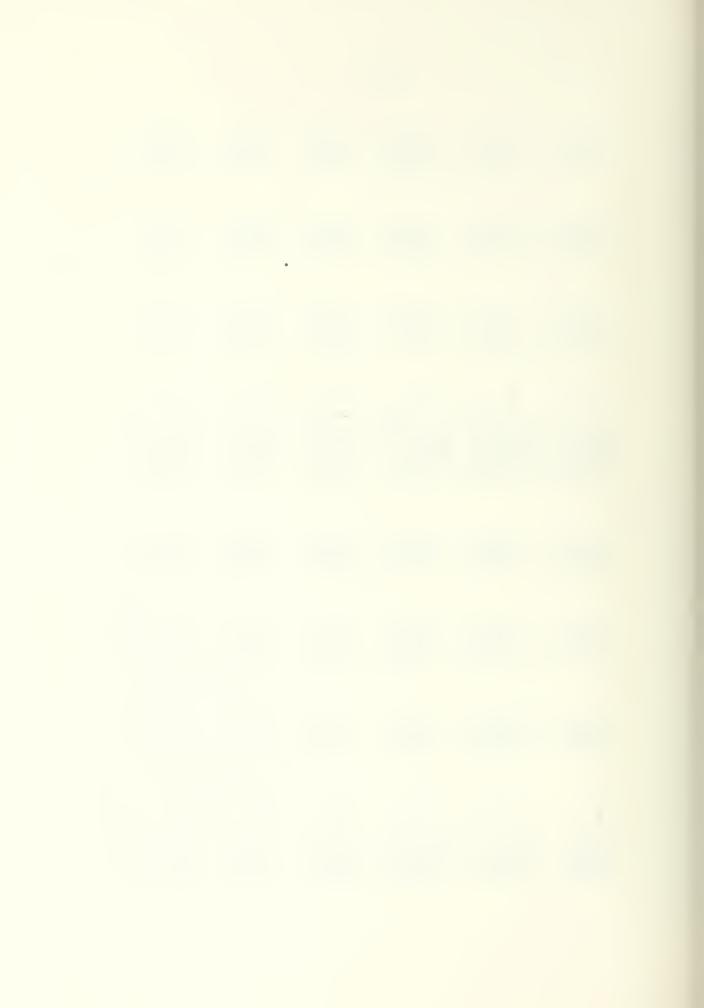
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BAROR 105.59	_			42784.7			VC 201	-	•			4H ° 5 1 2 · H		167.56	CF. 1 66.3¢	~	a 24.36		317.16					2011C	38	389.38		121.21	•	•		m 347.16	350.67	13,24		- 3 C) C -	10011	959.17	10,67
24.0C TEMPERATURE	STRAIN A. (MECH.	STRAIN B.	STRAIN C.	LCMG. STRN.	PRINC. STRN.	26.00	TEMPERATURE		STRATE B.	STRAIN C.	LCAG. STRN.	DRINC. STRN.	00.76	TEMPERATURE	STRAIN A. (PECH.)	STRAIN B.	STRAIN C.	LCNG. STRV.	PRINC. STRN.	4	20°50	CADATA A AND	STABLE BO LPRCTO	STREET OF STREET	LENG STAN	OF INC. STRN.	50.04	TEMPERATURE	STORIN A. (P	STRAIN B. "	STRAIN C.	LCAG. STAN.	DRING. STRN.	TEMPERATURE	CTUATE A. INSTH. 1	CARRIO S	STRAIN C.	L CMC CTON	LC MC DING
95.1"	-74. n3	44.97	164,97	24.97	145.42		95.10	-55.23	84.07	144.07	14.97	166.69		95, 10	-25.33	104.07	144.97	14.97	156.14		:	CT .50		10.00		160.41		96.15	114.07	164.97	54.97	-15.73	169.37	21° 90	10 401	174.07	14.07		24.97
1,1,68	-54.65	15.94	05.35	15.35	88.38		103.68	-14.65	75, 35	75.45	-14.65	93. 99		17 3. BR	25.35	115,35	65,35	-24.04	110,15		:	17 3° 68	(1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	175.34	17, 57	101.01		84.50	24 . A.S.	175,35	-54.65	5.34	248.43	10.1	30 E 30 E	1 - 20 - 21 - 21 - 21 - 21 - 21 - 21 - 2	-04.65		75.15
5585) 111.31		16.74	-193.26	-91.26	-124.41		111.31	86.74	76.74	-141.26		-101.99		111.31	176.	90	-213.26	-131.26	-244.65			112.		76.98	2 °CC1 -	-347.64		117 CA	318.41		-421.54	-11.50	-423.74	121.01		916	440.77		47,23
TEMPERATURE	STRAIN A. (MECH.)	STRAIN A	STRAIN C		PRINC. STRN	21 62		A (NF		STRATM C		PRINC. STON	20.00	TEMPERATINE	STRATH A. CHECH. 1	STRAIN R		ż	PRINT STRN			TEMPERATION	A. CHIP	CTRATA B.	S MOLO CHOR	-	4	TEMPEDATION	METM	STRAIN R.	STPAIN C.	I CHG. STRN	DRING. STRN	TEMOSCOATION		TO THE PERSON OF		3 6 6	A MOLY CLOSE



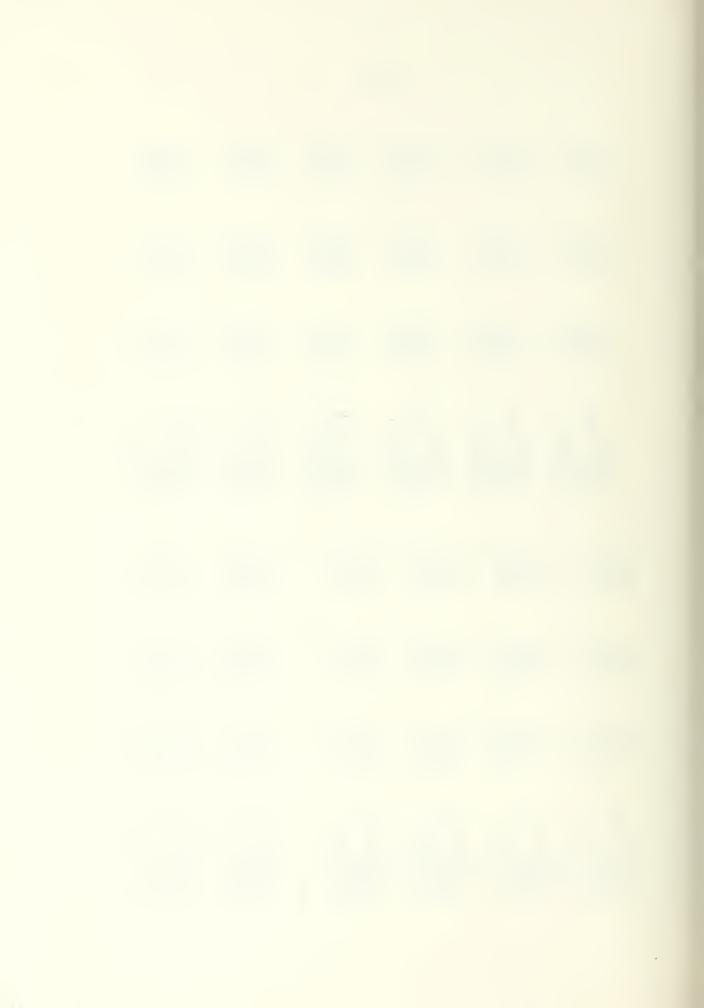
94.14 50.43 -120.47 110.53 290.43	96.10 90.81 -130.20 90.81 90.81 320.81	01.06 61.77 -130.23 01.77 201.77	90° B7 52° 52 -117° 69 02° 62 23° 57 243° 57	1046.94 146.27 156.87 265.87 268.87	113.22 20.12 -139.88 90.12 250.12
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163-74 -157-23 -247-23 -62-77 -275-48	4	11776.54 -11776.54 -11776.56 -276.05 -276.05 -276.05	- 2246.81 - 2246.81 - 156.81 - 236.81 - 236.81	106.22 -219.79 -138.79 21.21 -98.79	1111 1214 1314 1314 1314 1314 1314 1314
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95.11 244.97 154.97 -25.73 64.97	2000 2000 1000 1000 1000 1000 1000 1000	67. 304.93 44.94 145.04 276.94	97. 294.96 115.94 115.94 115.94 114.96	2345.70 2345.70 25.00 25.00 3715.70	105.25 165.25 - 64.74 64.25 275.25 289.89
173.68 355.35 95.35 -134.65 125.35	104,04 395,47 995,47 -144,57 205,47	10.00 32.00 32.00 -04.00 -04.00 -04.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -01.00 -	111.31 236.74 -123.26 -83.26 276.74 332.86	118.95 139.10 -120.90 -40.90 219.10	127,54 52,92 - 97,78 - 27,78 122,92
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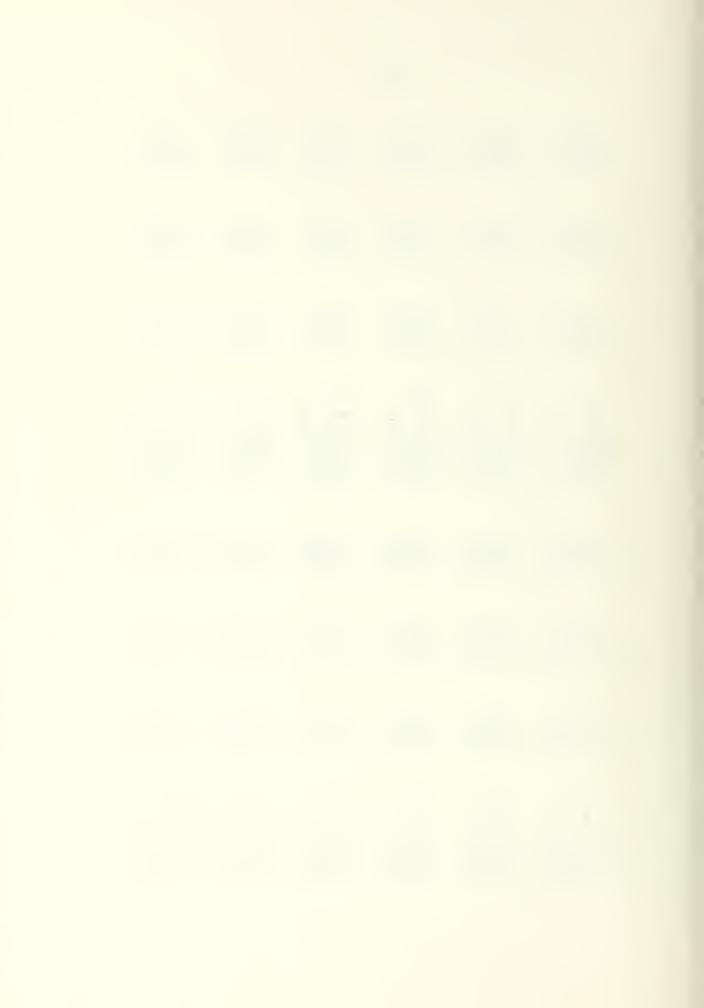
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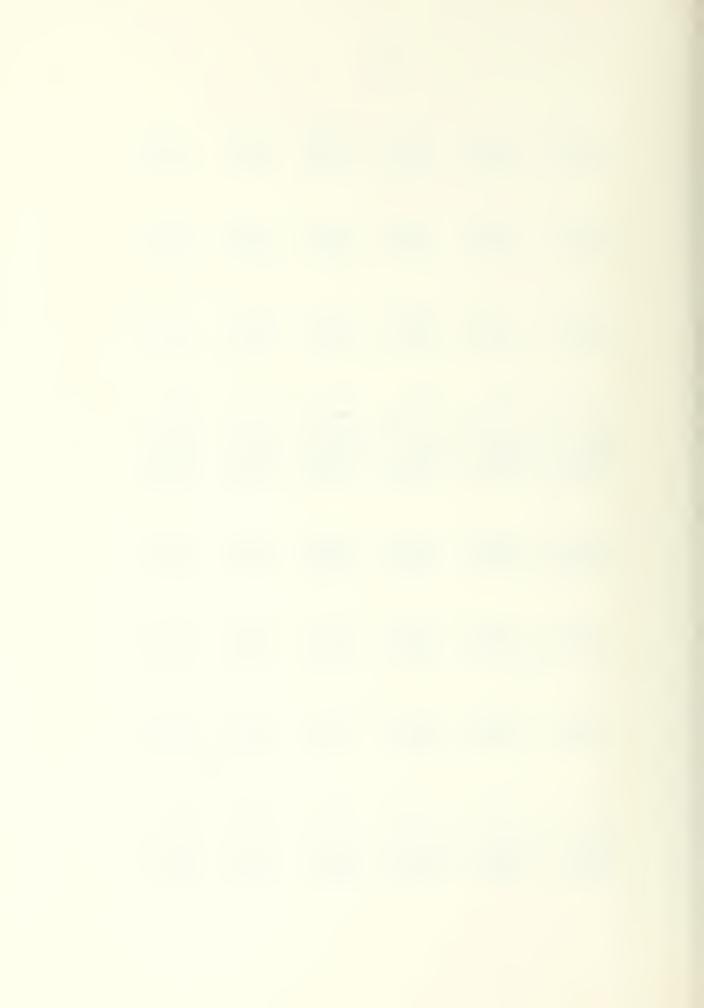
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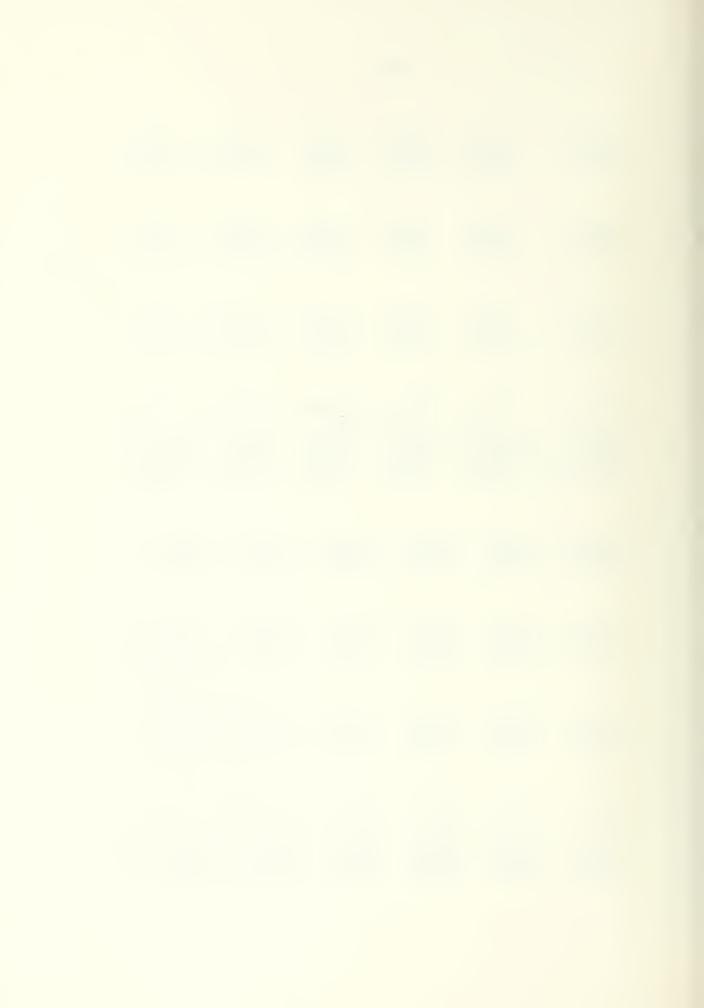
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90.09 TEMPERATURE STRAIN A. (MFCH.) STRAIN B. C.	TEMPERATISE STRAIN D. (MFCM.) STRAIN D. (MFCM.) STRAIN C 1 DAG. STRN PRINC. STRN.	15.74 TEMPFRATURE STRAIN B. (MFCH.) STRAIN B. 8 LINK. STRN. 8 DOINT. ATRN. 8	TEMPRATURE STRAIN A. (MFCH.) STRAIN B. STRAIN C LONG. STRM PRINC. STRM.	TEMPERATURE STRAIN A. (MECH.) STRAIN A. (MECH.) STRAIN A. B.	TEMPERATISE STOATURE, MECH.) STOATURE, STOATUR



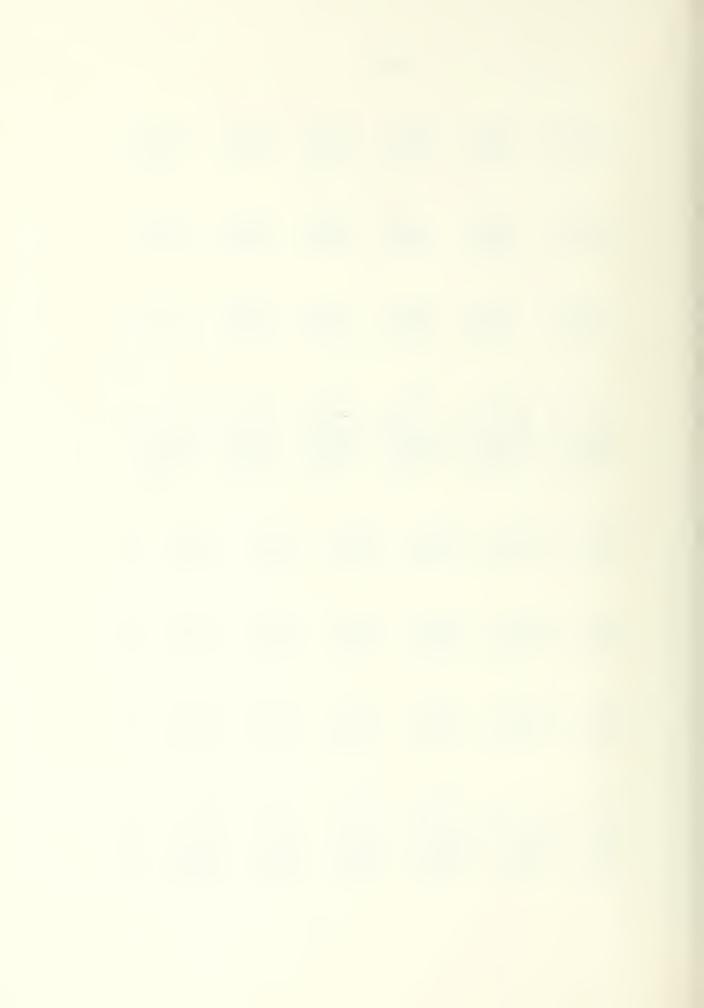
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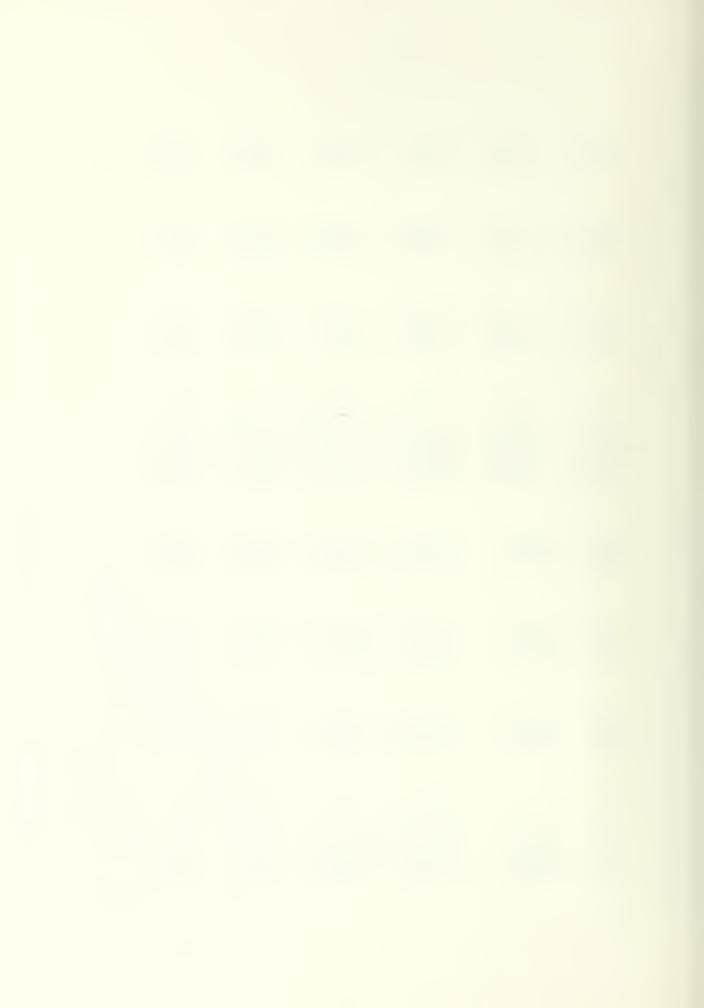
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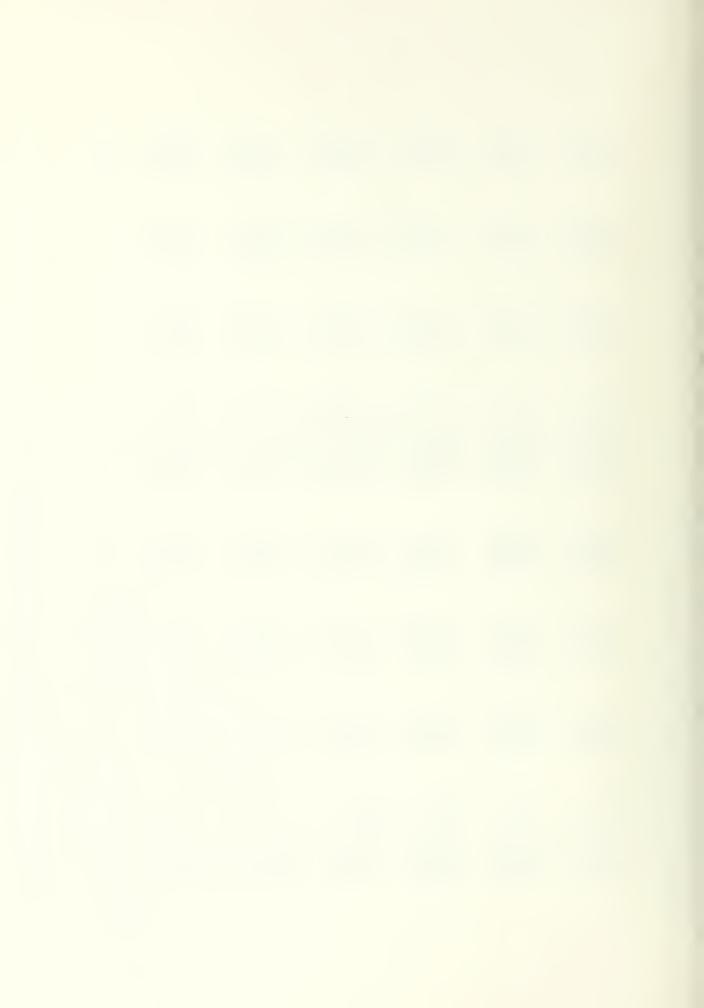
	134.21	CL 0001	-229.70	20,30	160,30	-237,341				136.21	-79.69	-219° 70	3C°30	140.31	-227.30				17061	\$ C 0 C 0 C 0 C 0 C 0 C 0 C 0 C 0 C 0 C	00000		1,0001				134.21	CF - 64-	-169,75	40.40	170.11	194,15				133.26	-50.83	-150.83	80°17	144.17	2030				134.20	- 10 mg	-120° H.	109017	219.17	1 P D J		
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33.14	0 4 6 6 6	4	133,50				177.32	-34,35	-35.47	24.1	4.10	-60.62				184.77	10 m m m m m m m m m m m m m m m m m m m	D	79.77	10 T T T T T T T T T T T T T T T T T T T	00000				0 C C C C C C C C C C C C C C C C C C C	30 0 0 1		0.000	00 10 1				204,76	60°CE-	29.93	90.01	000000	- 2 3 3 B C				184.77	-77.38	12.67	-57.38	-147,38	- I & B - C - C - C - C - C - C - C - C - C -			94 5	107.04	7 7 9 7 7 -
-2.5.03	7,000	3 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 -	-247.97	•			219.12	-787.97	12.04	-1-7-97	-4.7.97	-42 A. 44				229.61	- 30.0 - 24	30. 10	-107.24	67 ° ( 6 4 )	*7*1.9*-				234,33	*****	0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	**************************************					222.03	5	16.65	10 m	A 1 4 1 4 1	C7-816-				164.31	-R9.7R	-9.7R	-69.78	-149.78	-150.49			4 6 4 6	10,00	7A 0 6 T =
-768.78	1 9 No. 1 No. 1						304,98	-277. R3	- 47. 8 4	-587. A3	- 797. A3	-877.RJ				297.34	-> 64.44	45.56	-464.44	-774.66	-786.46				27 9. 26	-209.21	87° 70	-149.21	17.649-	-667.67			***	7.96.7	7 0 0 0 0	16 0 / 2	04 686	-373.66				777.67	11.50	1.59	-128.41	-119.41	-157.60				168.45	71.74
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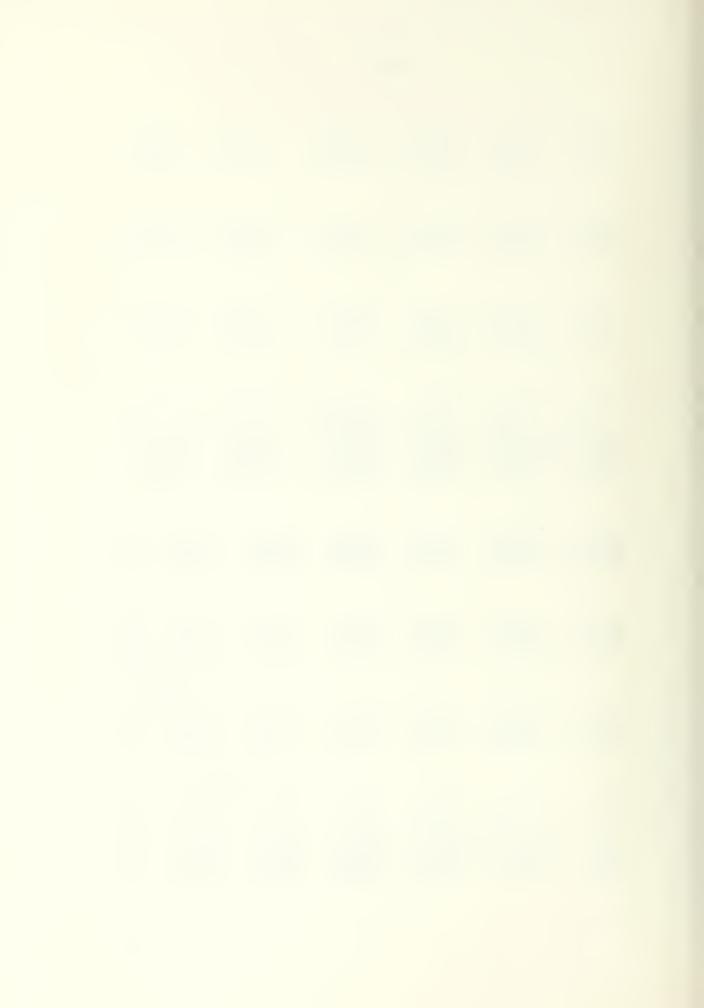
133.26 19.17 -130.83 119.17 269.17	133,26 20,17 -167,83 100,17 209,17	133.26 49.17 -197.83 59.17 299.22	133.26 20.17 -190.83 30.17 259.17	1 1 2 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	115.15.15.16.54.54.54.55.294.64.5
134.21 -104.21 -107.21 -157.21 -24.0.28	13.0.21 - 130.21 - 70.31 - 70.31 - 77.31	134°16 -231°46 -231°46 111°46 301°46	13 4 6 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		11.0 11.0 11.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0
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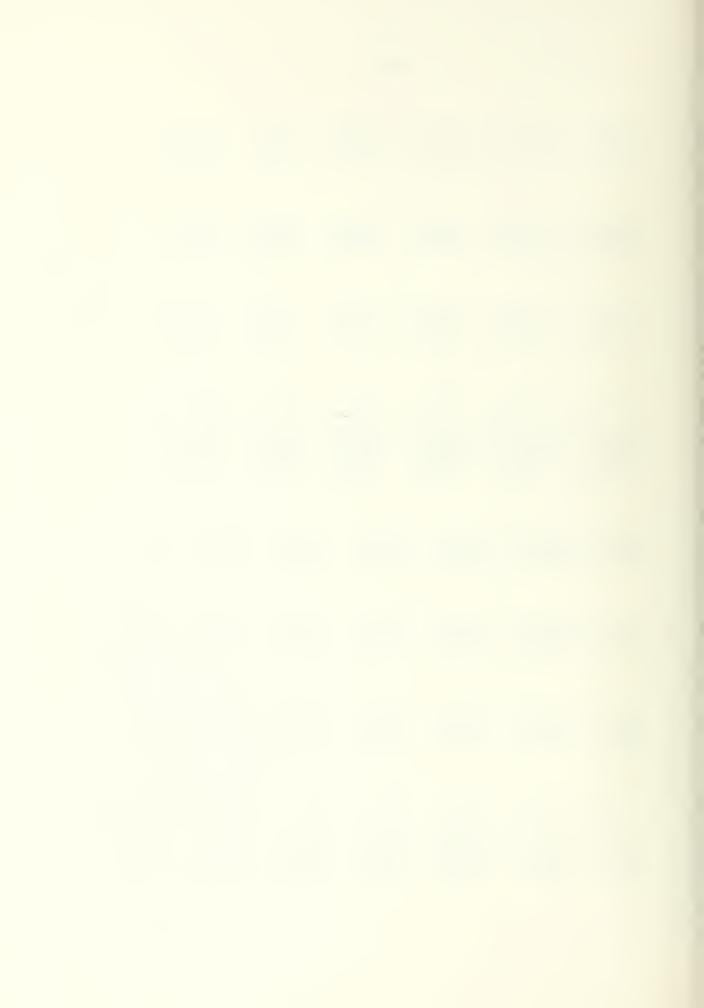
137.07 -46.17 -246.17 -243.83 -21.69	17.2 - 74.8.5 - 248.57 - 71.6.5 - 21.6.5 - 25.0.6.3	140.47 -98.77 -219.78 51.23 -232.77	156.15 -127.671 -200.671 -200.60 100.90 -217.20	159.01 -126.17 -196.17 -13.83	57.11 -179.74 -179.74   1.25   41.25 -199.12
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TEMBERATURE STRAIN & (PECH.) STRAIN C. STRAIN C. ECNG. STRN.	PROPERTURE STRAIN & (PECH.) STRAIN C. LONG. STRN. H	TEMPERATURE STRAIN 0. DECK. STRAIN 0. STRAIN 0. LONG. STRA. PRINC. STRN.	14C.00 FERSTURE STRAIN A. (FFCT.) STRAIN A. (FFCT.) STRAIN C LCNG. STRN	TEMPERALRE STRAIN & LPECT, STRAIN C	300.000 Trappature Stable a. (PFCT.) STRAIN B. (PFCT.) STRAIN B. (PFCT.) STRAIN C. (PFCT.) LING. ATRN. B.
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146.61 315.62 135.62 -254.18 -74.18 334.55	147.57 386.62 16.62 - 273.88 96.62	147.57 476.62 6.62 -263.38 196.62 412.87	1426.657 -283.38 -283.38 276.62 86.62	147.47 - 436.62 - 213.38 - 216.63 - 71.69	1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
144, 70 424, 25 84, 26 - 455, 74 - 115, 75 + 665, 96	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1466.61 645.82 -743.18 -624.18 95.82 651.48	146.61 465.62 -214.18 -614.18 769.82	147.67 606.62 - 939.38 - 513.38 126.62 723.38	156.15 362.53 -447.47 -287.47 527.47 621.36
TTERREATION CAPAINS CA	TA. CA TEMPERATURE STRAIN A. (MFCH.) STRAIN C C.PMG. STRM PRIMC. STRM	TEMPERATURE STRAIN A. IRFCH. ) STRAIN G. B. CTRAIN C. B. CTRAIN C. B. COMM. STRA. B.	TEMPERATISE STRAIN B. (MECH.) STRAIN B. STRAIN C. m LONG, STRA. m	TEMPERATURE STRAIN A. (MECH.) STRAIN C. STRAIN C. 1 DIM. STRN S.	TEMPERATISE STEALW A. LMECH.1 STEALW B. LMECH.1 STEALW C. G. B. LONG. STEW. B. PRINT. STEW. B.



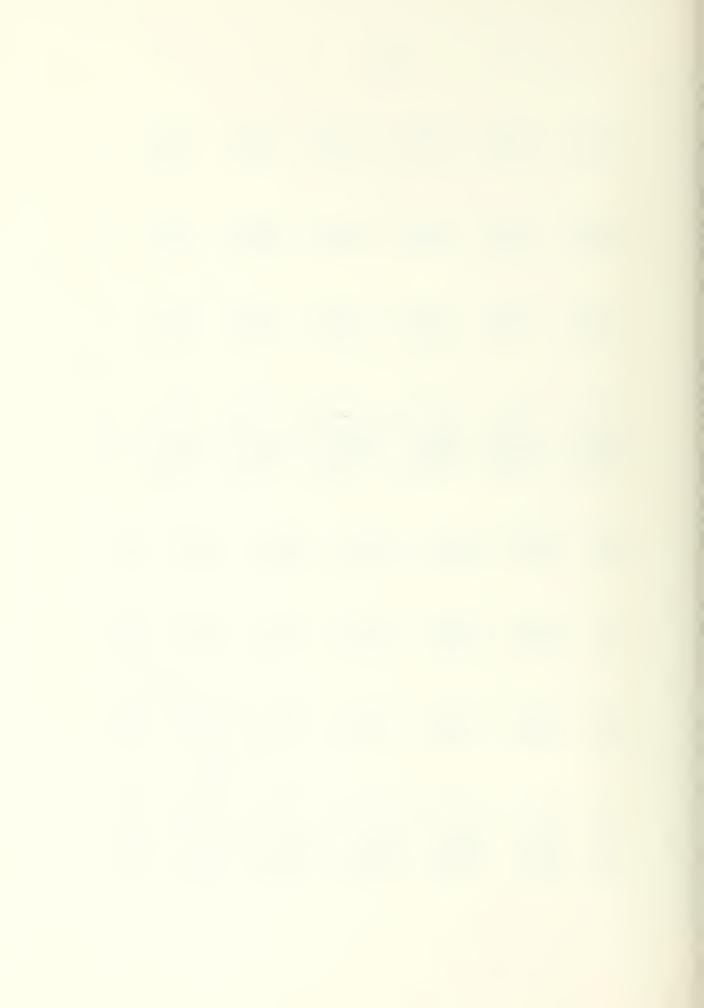
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ATBAIN A. (MECH.) ATBAIN G. S (TRAIN C. S (TAM, ATBA. S	TEMPERATURE STRAIN A. (MECH.) STRAIN C	TEMPFRATIPE STRAIN A. (MFCH.) STRAIN A. (MFCH.) STRAIN A. (MFCH.) TONG, STRA	TEMPERATISE STEALS A. (MECH.) STEALS A. (MECH.) STEALS C	TERPERATURE ATRAIN A. CAPITA ATRAIN A. CAPITA DRING, ATRAIN PATOR ATRAIN AND ATRAIN	STRAIN A. (MECH.) STRAIN A. STRAIN G. STRAIN G. STRAIN G. FRIFT STRAIN MECH.) STRAIN A. (MECH.)



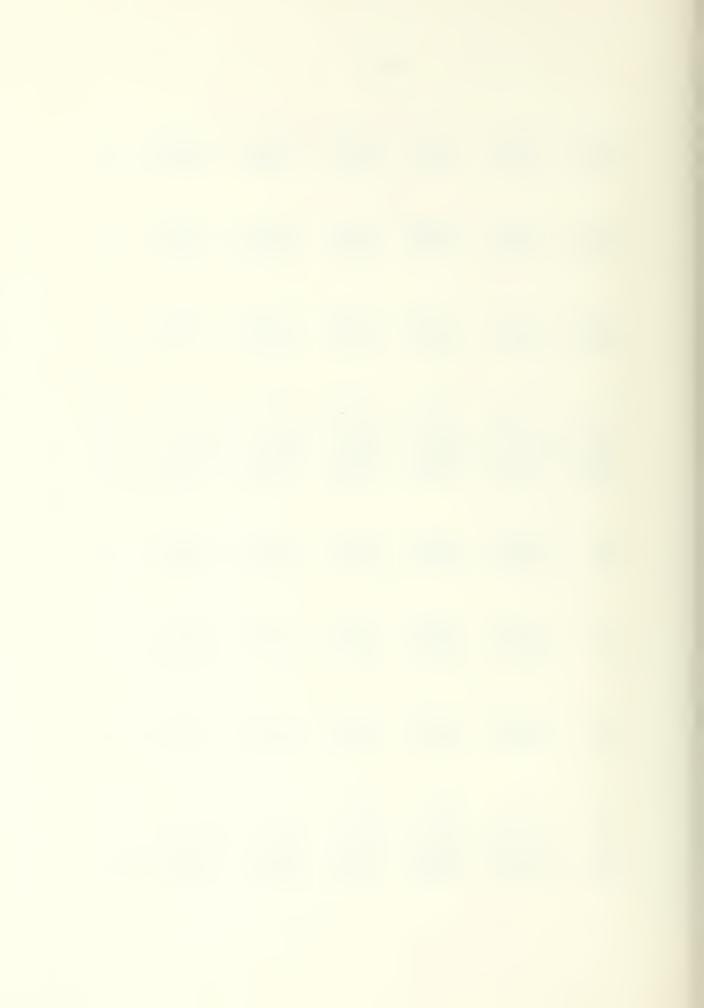
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100.5   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.6   100.	Ī	r	246.53	333° 46		-77-37	-50.83	-41.94
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120.08   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.78   12.	ī	112.64	92.63-	38.25	10.00		76 251	132.50
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179,05   152,34   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   170,00   1	1 1	592.64	120.00	206.48	STRAIN AS LECTS!	-47.37	1 60 6 C 4 - 1	-41.94
179,05   152,34   152,34   122,65   136,15   139,26   139,27   152,34   152,34   122,65   136,15   139,26   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   139,27   1		*	04.01		* CALCATA	52.63	4.17	-1.04
179,					٠	122.63	30.17	38.06
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-81.95		197.38	-21.72	236.16	STRAIN A. (PECH.)	92.63	39.17	00000
197.17   159.97   150.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   170.07   1	7	845.38	-81.95	266.76	STORIN B	-27.37	0 K 0 C C C	*010*
197.17   150.97   150.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   170.67   1					STRAIN C. "	-67.37	10 · 10 · 10 · 10 · 10 · 10 · 10 · 10 ·	***
197,17   199,97   19,07   19,07   19,07   19,07   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,097   19,09					CAG. STRN.	52.63	20.17	4 N C C C C C C C C C C C C C C C C C C
197,17 199,97  197,17 199,997  12.58					RINC. STRN.	102.08	- 14. Hb	
15.65 194.98 15.06 137.67 133.26 133.26 1449.88 15.06 13 133.26 133.26 1449.88 15.06 13 143.67 193.26 1449.88 15.06 13 143.67 193.26 1449.88 194.97 578.81 8.0 146.17 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.85 144.		317.38	197,17	150.97				
12.58	T	244.89	-67.42	134.98				
-147.42 164.94 STRAIN A. (PECP.) 17.00 1 1.00.07 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.09 1 1.00.		15.11	12.58	14.98	10.61		133 34	132,30
18.29 169.51	•	654.89	-47.42	64.98		1 4 4 6 7 4	135e CO 80-17	68000
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2134.39 169.51	i	0.00	00.7		8 10 22 40 40	-166-17	Ed . CD-	-51.04
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13   13   13   13   13   13   13   13		320,24	213.39	169.51				
19		256.81	75-57-	61.40				
# 1		63 10	86.73	31.4	18.00			
## -283.27	•	626. B1		71.40	TEMPERATURE	138.03	134,21	132.30
45 -293.54 Inl.76 STRAIN R. " -274.65 -149.77 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70 -119.70	•	966.81	-2 M 3 - 2 7	101040	STRAIN A. (MECH.)	225.06	150,30	99°68
78		998.45	-293.54	101.76	STRAIN 8. "	52.4.02-	-140.10	-111.04
136 228.66 187.86 187.86 187.86 187.87 228.49  10 179.31 61.86 2C.0C (AQC) 137.C7 134.21  11 179.31 61.86 5741.8 8 1 -35.81 -99.67  11.16 5741.8 8 1 -35.81 -99.67  11.16 5741.8 8 1 -35.81 -99.67  12.06.574.8 8 1.95.7 56.37  12.06.574.8 8 54.66  13.17.7 578.8 8 -35.81 -99.67  14. 236.79 197.4 8 403.92  15.18.8 8 54.66  11.19.9 8 54.66  11.19.9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9					STRAIN C. "	-344-5	-110.70	-61.94
38 228.66 187.86 18.16 20.0C (ARC) 11 -6.66 1.16 20.0C (ARC) 12 -6.66 11.16 574.81 32 -46.3.15 79.17 574.8 8 (PECH.) 37.82 160.37 34 -47.3 5 79.17 574.8 8 -36.17 -99.77 576.8 6 11.16 574.8 8 -36.17 -99.77 576.8 6 192.4 8 60.3 60.3 60.3 60.3 60.3 60.3 60.3 60.3					LONG. STRN. "	185.05	190.30	148.75
38 228.66 172.86 1.0.86  89 -22.66 1.16 20.00 (ARC)  11 1.04.21 134.21 134.21  80 -6.66 71.16 55RAIN A. (PECH.) 373.62 160.37  32 -473.15 79.17 55RAIN B. " -566.17 -99.77  510.80 C					DRING. STRN. "	+397.57	228.49	170.70
11 1-2266 1.16 2C0C (AAC) 137C7 13421 1  -666 7116 FEMPERATURE  -9		317,38	228.66	187.86				
1		234.89	-220.66	1.16				
89 -6.66 71.16 TEMPERRURE 137.07 134.07.1 14.05.1 17.07 134.07.1 14.05.1 17.07 134.07.1 17.07 134.07.1 17.07 134.07.1 17.07 17.04.1 17.07 17.04.1 17.07 17.04.1 17.07 17.04.1 17.07 17.04.1 17.07 17.04.1 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17.07 17		145.11	100,33	61.16	20.00 (ARC)		10 761	112 30
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32 -463.15 70.17 STDAIN B. " -366.17 -1994.54 -1316. STDAIN " -366.17 -69.77 -516. LCNG. STRN. " 463.82 266.37 179. RR 236.29 192.45 BFINC. STRN. " 546.65 264.56 195.	Ì	044.40	- 30 66	11.16	STRAIN A. (PECH.)	D - C - C	100.00	
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LCNG. STRN. # 403.92 266.30 178.0 RA 236.29 192.4 EFINC. STRN. # 546.65 296.50 195.2 28 -247.40 -1.34					STRAIN C. "	-356.17	-69.70	-51.94
PRINC. STRN. " 546.65 236.29 192.45 PRINC. STRN. " 546.65 236.29 192.45 236.29 -71.34					LING. STRN. "	403.83	260.30	178.5
84 236,29 192,47 28 -247,49 -31,34					FINC. STRN.	£44.65	25°756	195.25
78 -247.49 -11.34		377.84	236, 29	192.4				
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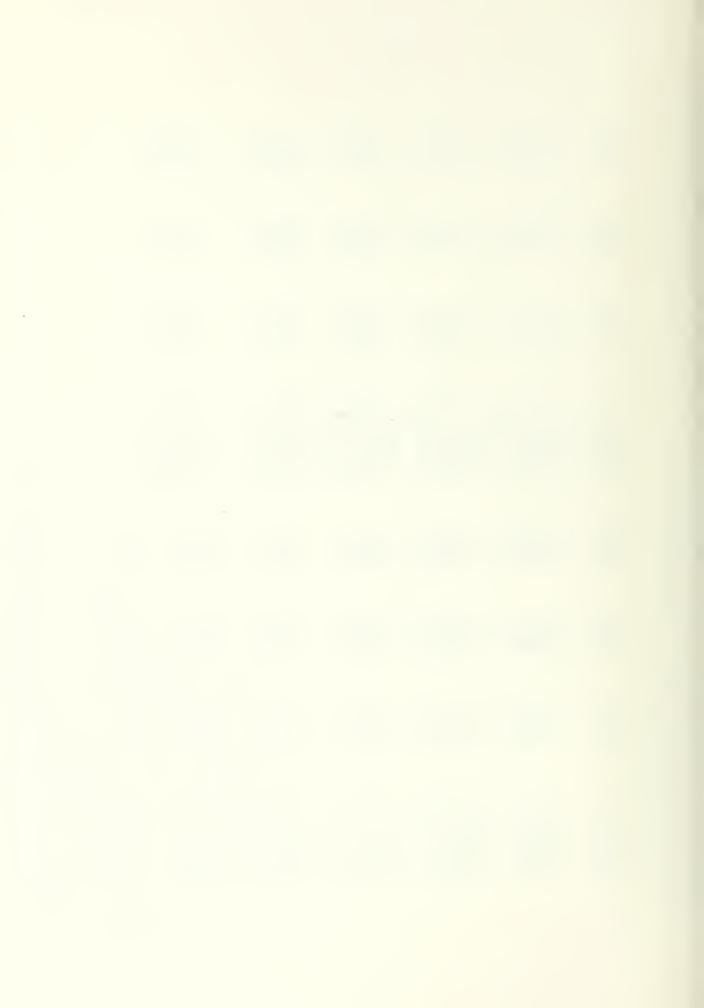
132,30 99,06 -151,946 -11,946 234,06 246,21	132.37 69.06 -161.94 28.06 259.06	132.30 38.06 -151.96 78.06 268.06	132.30 22.66.06 25.66.06 25.66.06	131.35 16.96 -123.64 1266.96 266.96	1300 300 300 300 300 300 300 300 300 300
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46.66 -81.34 107.19	- 15.34 11.6.61 25.51 - 153.39 - 16.69	779,54 - 156,71 123,59 - 6,71 - 221,35	213.39 -73.27 176.73 -93.27 -233.27 -233.66 169.56	-13,04 -13,04 -43,04 -173,04 -174,41 177,46 42,77	112.07 -62.07 -62.09 114.27 17.44 17.44
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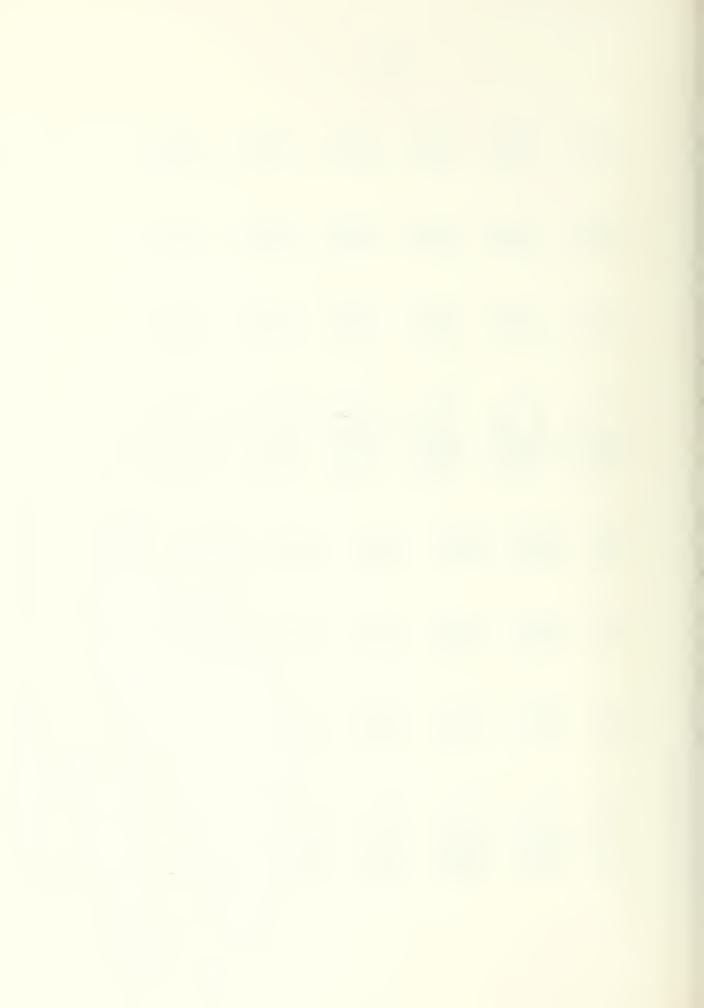


15.899 -94.11 145.889 255.89	.77.39 15.86 -116.86 -1165.86 275.86 275.86 275.86	131.935 -113.056 -113.056 166.96 266.96	132 -310 -1310 -1310 -1310 -246 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3730 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -3700 -370	136.12 -157.37 -157.37 -192.63 242.64 260.91	142.80 - 79.57 - 118.57 - 16.43 - 241.43
-110.43 149.17 249.17 375.36	13.25 1.724.9 1.12.10.55 1.21.10.55 2.31.10.55 2.31.10.55 2.31.10.55	13% - 273° 72 - 273° 72 156° 28 266° 28	164.52 -157.23 -277.24 164.76 219.76	1600 1640 1640 1640 1670 1670 1670 1670 1670 1670 1670 167	176.19 -211.40 -111.40 -278.60 -278.25
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STRAIN A. (PECH.) STRAIN G. STRAIN C. LCNG. STRN.	#C.00 TEWFRATURE STRAIN A. (MECH.) STRAIN B. STRAIN C. LOMS. STRN. BRING.	ASSOC TEMPRACIDE STRAIN AS (PECHO) STRAIN AS STRAIN CO LCNG, STRA	FEMPRATURE STRAIN A (MECH.) STRAIN B. STRAIN C. CLNG. STRN PRINC. STRN	TEMPERALLS STRAIN A. (PECH.) STRAIN B. STRAIN C. LCNS. STRN. B. B. STRAIN C. B. STRN. B. B. STRN. B. STRN.	GC.00 TEMPERATURE STRAIN B. (*ECP.) STRAIN B. " STRAIN B. " STRAIN C. STRN. " PFINC. STRN. "
-12.56 114.53	146-61 125-82 155-82 155-82 15-82 168-28	1246 1246 1246 1468 1468 1468 1770	146.61 185.82 226.82 -4.18 -4.18	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
45. #2 116. 65	146.01 165.00 115.30 25.00 75.00 168.00	146.61 165.85 165.82 25.82 65.80 171.98	146.61 215.93 275.93 46.13 7.93 7.4.9	14.5.6.1 2.7.5.8.2 2.7.5.8.2 2.8.2 4.6.18.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 4.8.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8	255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0 255.0
176.43	144. 744. 144.24 144.24 14.24 14.24 25.25	144-77 244-75 174-26 74-26 74-26 254-26	144, 27 264, 25 -15, 74 -5, 74	446 446 446 466 466 466 466 466 466 466	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~
PRINC, STRN, "PRINC, STRN, "PASS"	VERPERATIRE STRAIN R. LECTA. ) STRAIN R. R. STRAIN R. C.	TEMPERATIBE STRAIN B. (MECH.) STRAIN B. (MECH.) STRAIN B. (MECH.) STRAIN C. (MECH.) STRAIN C. (MECH.)	TEMPERATURE TOTALN A. (MFCH.) STRAIN A. CTRAIN C. B. ( OMG. CTRN. B. PRINC. STRN. B.	TEMPERATION STRAIN S. S. TRAIN S. S. PRINC. STRN. S. PRINC.	TEMPERATIBE STRAIN A (METH.) STRAIN A (METH.) STRAIN A TRAIN B FINS. STRAIN B POINT. STRN. B

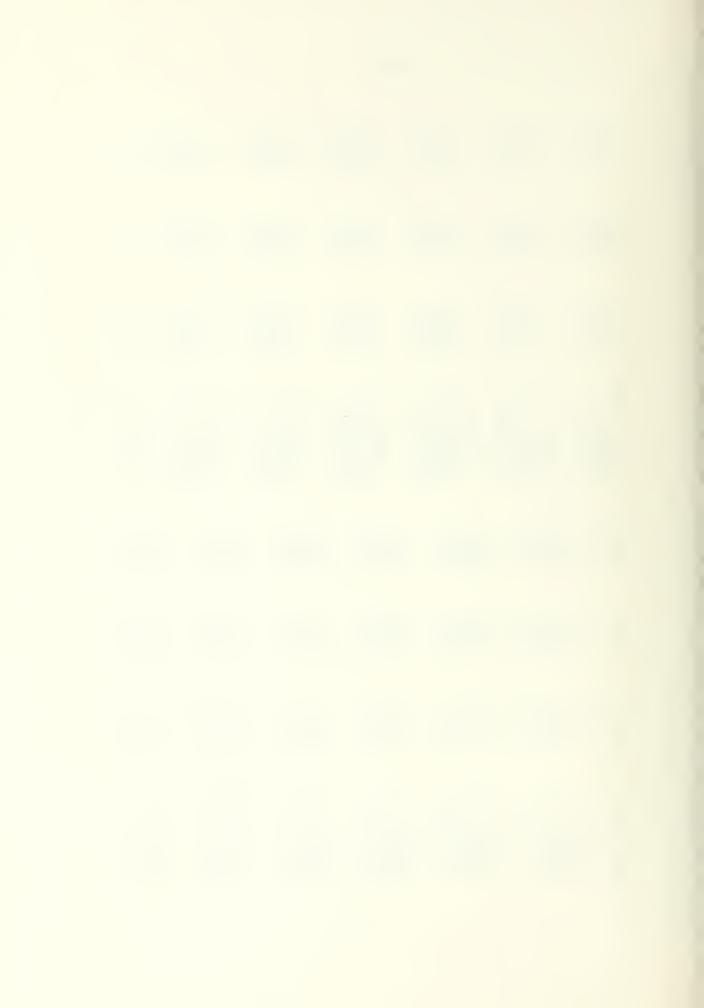


	-92.56 423.88	380.73	LONG. STRN. BRILC. STRN. B	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10.70.69	136.24
145.66 495.73 424.73 -334.97	1449.47 438.28 248.28 -251.72 -81.72 489.12	144 36 m 6 1 26 m 6 2 27 % 6 2 -184 % 18 54 % 18	170,000 TEMPFRACKS STRAIN B. STRAIN B. STRAIN G. ECMG. STRN.	213, 35 -217, 77 -310, 77 -310, 77 -37, 77 -27, 77	1 6 6 6 1 1 4 6 6 6 6 6 6 6 6 6 6 6 6 6	1 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
146.01 014.87 195.82 -574.18 -314.18	144-47 498-28 238-28 -321-72 -61-72 524-86	1466 2756 2756 2756 2756 1276 138	JOG OCT TEMPERATURE STRAIN B. (PECM.) STRAIN B. STRAIN C. ICNG. NTRN.	181-91 -172-64 -92-649 107-61 27-61	1746.2P -1946.3C -1946.3C -1946.3C -1946.3C	161 162,089 -050,086 -050,086 -070,086 -120,086
140.47 765.28 245.28 -711.72 -191.72	1 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	147.41 426.65 426.65 546.65 76.65 76.63 79.63	TERPERATION STRAIN SO TECHO STRAIN SO TECHO STRAIN SO SE	157-11 -128-74 -168-74 141-26 171-26	17376 -17376 -17376 -17376 -17376 -17376 -17376 -17376 -17376	11 - 12 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2
135.34 -769.00 -769.00 -110.16	5 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	147.57 446.67 139.62 -139.88 76.67	TERPERATOR  TERPERATOR  STRAIN CO.  STRAIN	12 8 6 8 8 8 8 9 1 1 6 8 9 1 1 6 8 9 1 1 6 8 9 1 1 6 8 9 9 1 1 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	A 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	127.53 - 177.27 - 27.27 - 27.27 - 17.2.87
155.27 011.03 -278.77 -758.77 281.03 846.35 150.07 150.07 175.07 175.07	56 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	147.67 186.62 116.62 176.62 176.62 456.66 147.65	PASS# 14  -20°CC TEMPERATURE STRAIN 8° TPCP° 1 STRAIN 8° TPCP° 1 STRAIN C° TPN° # PRINC° STRN° #	6.0 = 1 = 4 = 1	134.21 -110.65 -10.65 -10.37 -150.37 -150.51	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

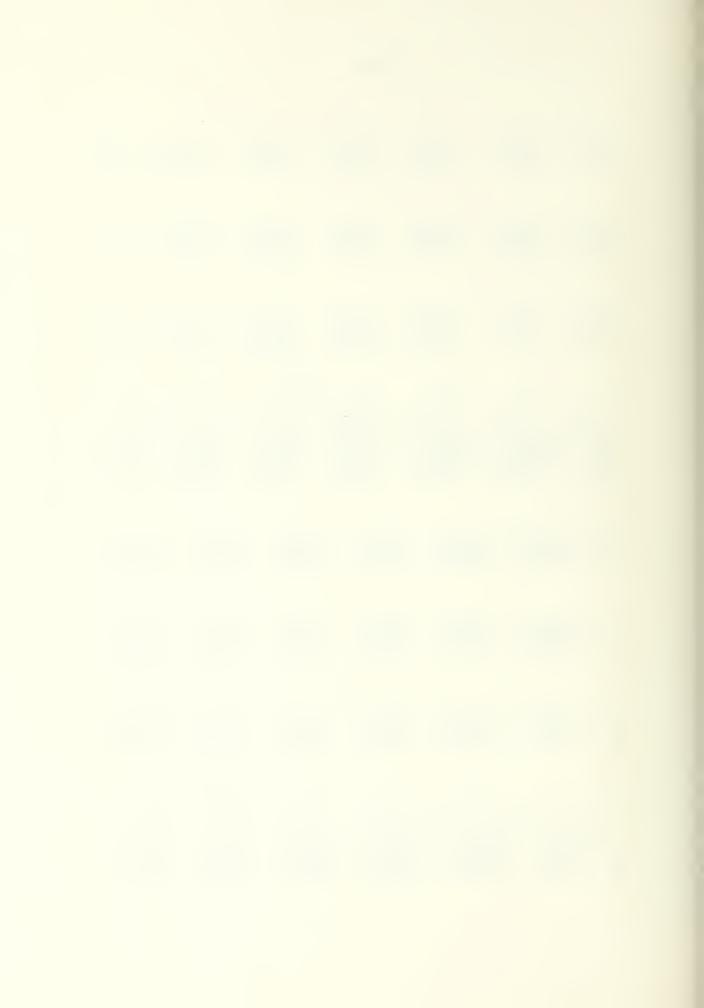




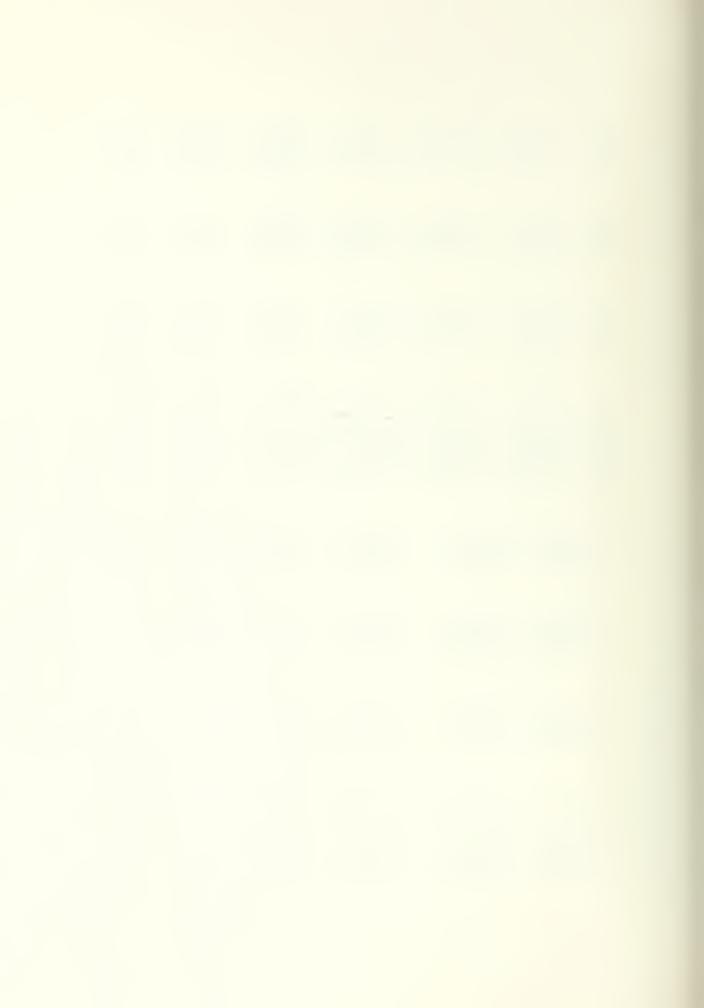
LONG, STRW W	-319, 62	3-7-16	276 62	STRAIN A. INECH. )	320.36	1990.17	130,31
PRIME SIRMS II	-329.71	314,17	116.92	STRAIN B	270.30	129.17	70.30
				STRAIN C.	-219.70	-130.43	000
43					90908		134.01
TEMPFRATURE		154.24	147.57				
100	-64.16	231.34	266.62				
	-	51,34	76.67	19.00			
		61.34	56.62	TEMPERATLAE	134.21	133,26	134.21
LONG. STRN "	-467.36	241,14	246,62	STRAIN A. IPECHA)	550,30	269.17	160.10
DRING. STRV	-498.66	273. R1	296.72	STREIN P. B	20,35	70017	10.10
				STABLE C	-519.70	-200.43	-99.70
				LCAG. STAN. "	10,30	39.17	50°31
46.				PRINC, STRN, "	550, 13	265.22	161.83
TREPERATION		158.76	147.57		•		
U W	-0.35	103,75	246.62				
		63.75	86.62	20.0C (QRC)			
	-457.34	33, 79	66.62	TEMPERATURE	134.21	134.21	134.21
I MAG. STRN	-617,34	153,74	226.62	STRAIN A. INFCH.	610.30	240,30	170.31
PRINC. STRN	-646.24	196.21	275.64	STRAIN P.	-295.69		-39. 70
				STRAIN	-619.75	04-941-	-84,70
					290, 15	170,30	120.31
40.10					-606.79	2000	192.05
TEMPERATION		165.69	149.47				
STRAIN A. (MFCH.)	-114.99	146, 78	238.28				
	91.12	MM. 78	178,28	22.00			
STRATE C	-40 M. B.B	10.78	78.28	TEMPERATURE	136.12	134.21	134.21
		78.78	208.28	STRAIN A. INFCH.1	432.67	240.30	160.17
PRINC. STRN. "	- 751.71	148.97	252.62	STRAIN B	-467.37	-100,70	-79.70
				STRAIN C	-517.37	-140,70	-50.70
				LCAG. STRW. "	\$22.63	90°006	16031
	;			PRINC. STRA. "	- 787 - 50	74.47	220.60
TABLE STATE OF STATE	746.44	173.32	151.38				
CANALA M CONT.	CO	1000	219.58				
1		21.451	# 5 ° 6 F	24.00			
TO THE STATE OF TH	10.00		99, 58		141.84	134.21	134,21
		400	# C - C - C - C - C - C - C - C - C - C	STREIN AS IMECHS!	140.11	16.081	1900 41
		21 0001	54.727	CHAPTA GO	70.000	200	
				E 2000 C40 -	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	200	2 2 2 2
36				B NOLD CALL	708.40	481.184	236.55
TEMPERATIME	295, 44	182.86	154.24				
STRAIN A. IMPON. 1	-153.68	41.16	181.34				
E	216, 12	161,16	151,34	26.00			
	-433. A.B	21.16	171.34	TEMBERATURE	149.47	134.21	134.21
v	-973. AP	1000	131,34	STRAIN A. INFCH.	-119.78	15001	100.30
PRINC STRW,	-938°-4	161.54	142.57	STRAIN 8. "	-726.77	-229.70	-119.70
				STRAIN C	-128.78	47.30	30030
				LCNG. STRN. "	4M1.22	280.30	250.30
				DRING. STAN	-128.79	101.13	251.49
	3-2-11	80°06	167.83				
STRAIN A. CAFOH	-146.87	-45, 82	136.86				
		734.13	104. BG	28°C			
	-406. 5	44.18	144.86	TEMPERATURE	162.63	137.76	14.21
LUNCO CTRN.	-965. 4"	-235.82	96.86	STRAIN A. 1PFCH. )	- 5000-	23.17	0 P 9 J



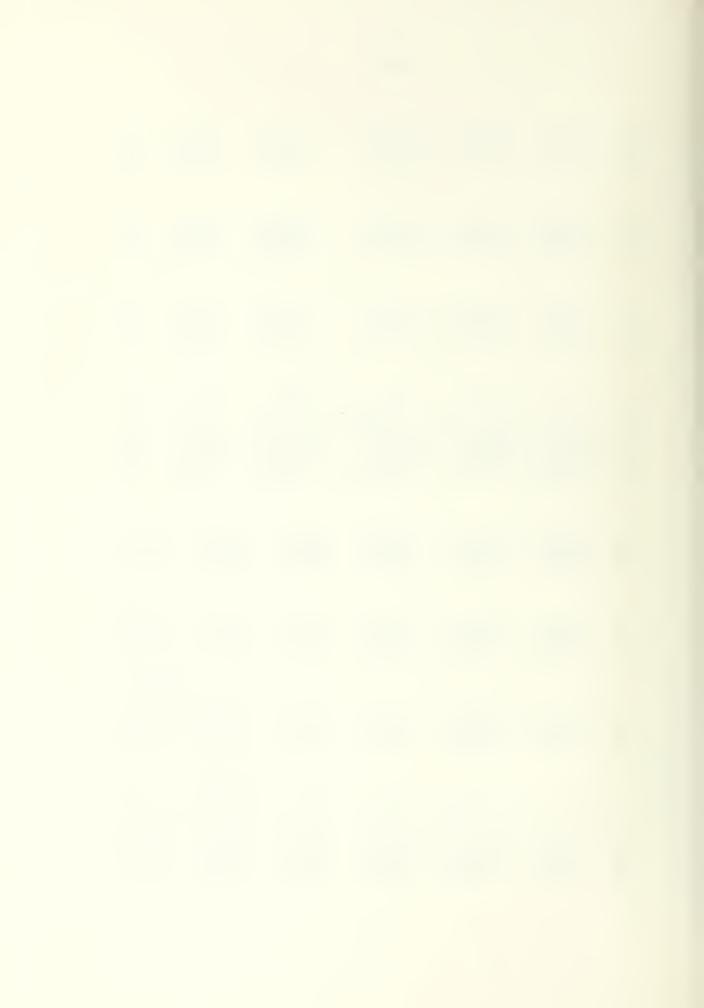
1110.70	267.57	134.21	109° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10	, •Cr.	1 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	134.21	150.30 150.30 220.31 240.31	64 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	11.00.00.00.00.00.00.00.00.00.00.00.00.0
1110.17	102017 102017	153.26	100011			134.16	44044	1111 1111 1114 1114 1114 1114 1114 111	144 547 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
-580.93 5.07	244.09-	175.27	4 4 5 5 5 4 1 4 4 5 5 5 5 5 5 5 5 5 5 5			207.67	\$4.00 \$4.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00 \$1.00	222.65 1572.65 130.35 159.35 159.35 2002.53	- 433 - 5 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6
STRAIN G.	PFING STRN. I	30.00 TEMPERATURE STRAIN A. (PECH.)	STAIN B	THE WALL STATES	STRAIN BOOK TO TO THE TOTAL TOTA	36-00 TEMPFATURE	STRAIN A. (PECH.) STRAIN A. STRAIN C. ICNG. STRA.	FEMFERATURE STRAIN A. IMEC. STRAIN C. STRAIN C. LCAG. STRA.	TEMPERATURE STRAIN D. (PECH.) STRAIN G. B. LCNG. STRN. B. SS.C. TEMPERATURE STRAIN B. B. STRAIN B. B. STRAIN B. B. STRAIN B. B.
187.13	170.46	222.07 162.07 22.07	229.77	184.47 22.62 242.62	194°38	10.22 110.22	-149,79 267,46	273,85 -740,25 270,25 270,25 270,25 280,25	2-1,-94 2-6-6-1 2-6-6-1 -2-3-9 -2-3-9 +2-5-3-9 -1-8-9 -15-1 -15-1 -15-1 -15-1 -15-1 -15-1 -15-1
-245-0	209.58	243.29 53.29 -346.71	-396•966 -	224.84 -132.51 327.49	16 . C. 4 4 1 1 4 8 . C. 4 4 1 1	237.56 -129.84 320.17 -19.83	- 460.00.00.00.00.00.00.00.00.00.00.00.00.0	12300 mm	11: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5: 23:5
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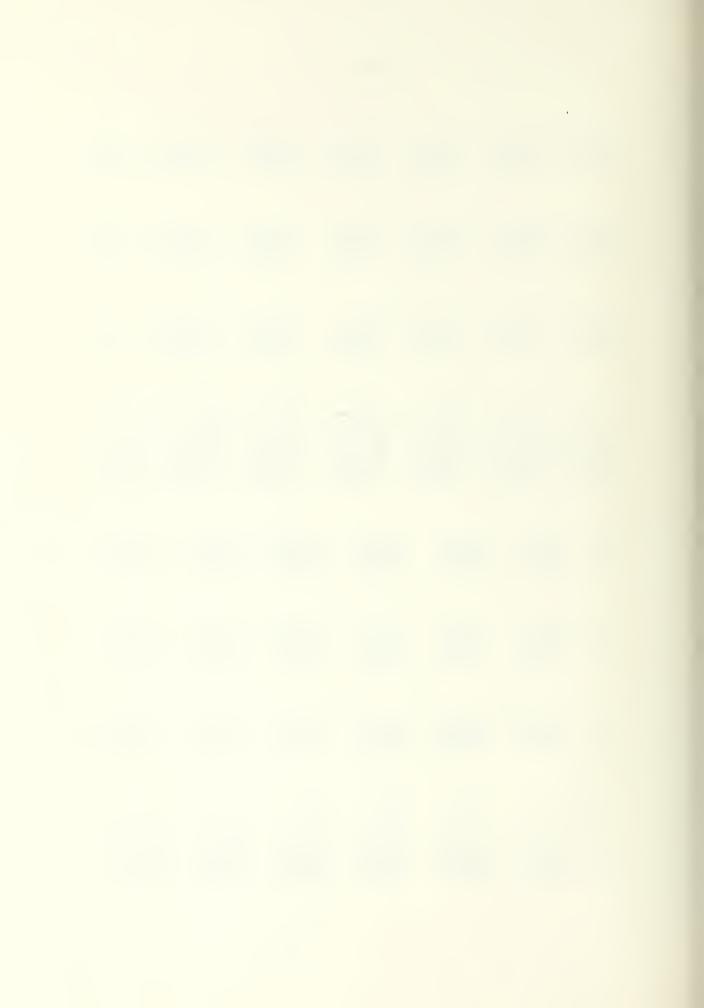
103.83	225° P3			138.03	-44.05	-34.95	105,65	165,08	229.64				144, 70	-75. A7	-15.87	174.13	114,13	190,02		152,34	00.00-	66 9-	145.01		144.71		141 00	1010101	17 75	127.75	-12.28	a offa		170.44	-139,99	50.01	12.00	00.00=	62.2		14.7 40	-134 14	010101	74.84
157.48	217.12			164.74	-268,25	-24,25	191.75	1.75	-7CA.83				177.14	-210.64	20.€6	140.06	40.00-	-229.68		187.63	-233.25	46.75	196,75	-173,25	-265,73		192.40	-225.30	14,70	04.70	-205,30	16.772-		1 49 . 54	-220,10	20.06	49.40	-237.10	-287,35		173, 27	-185.74	94.74	94.26
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STRAIN C. LUNG. STRN. B			65° nC	TEMPERATURE	STOAIN A. (MECE.)	STRAIN S	STRAIN C.	LINC. VIRA.	PHINC. STAN.				TAN	STRAIN A. (PECH.)	and Production	STRAIN C		PRINC. STRN.	100.001	TEMPERATURE	STRAIN A. (MECH.)			LCAG. STRN. "		130.00	TEMPFRATURE	- 4	STRAIN R			PRINC. STRN. "	210.00	TEMPERATURE	-	S SERVICE		LONG. STAN.	PRINC. STRN	340,00	TEMPERATURE	RAIN A. IPE	STRAIN B. "	
	1 40, 1	94.36	184, 36	14.36	174,64	L * * UO T			4	40.000	0000	149.00	200		6.001					147.97	96.62	196.62	1 de de	-104,38	2.4.74		147,47	176.62	196.62	- N - W W	-93,38	276.75		147.57	126.62	210.62	1 3 4 48	= 1 × 3° 38	231.27		147,47	156.62	236.62	-33,38
	160.01	124,36	164.36	15.64	40.00	187.85			1	CC-841	*****	****		C						147.57	146.62	176.62	EM ON-	-43.38	197.1		147.57	146.67	176.62	-3.38	-33.38	20h.66		16161	79.961	190.02	E 2 0 0 0 1	En anni	61.0227		147.57	186.62	236.62	-43.38
	149.1	174.76	214.46	-55.64	-45.64	232.46				104 43	70.071	2000	DF *6 F	E	84-162					146.61	185.82	24.86	81.44-	- 44.18	263.82		146.61	185.82	225.82	-44-	1.34.10	261.82		10.041	75.071	24°C62	1 · 1 · 1	01 *671	16 % 97		146.61	22% 82	205.82	-64.18
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-175°74 -236°79	1560.15 -157011 -157011 -1199999 -130011	136-12 -137-37 137-63 -142-63 -127-37	133.26 -17°.83 114.17 140.17 -40.83	134.21 119.69 1157.31 1157.32 227.65	134.21 1870.30 1870.30 -1140.30 -228.60 -228.60 -44.70
-104°CC -172°11	1566-011 1669-011 1669-011 1966-011	86-4 86-4 86-4 86-6 86-6 86-6 86-6 86-6	133.24 -70.63 99.17 189.17 199.17	135.16 16.56 116.56 116.56 116.56 216.56	1335 1710 1710 1710 1710 1710 1710 1710 171
LONG. STRN. **	570,00 TEMPERATURE STRAÍN A. (PECP.) STRAÍN C	SEPERATORE STRAIN A. CRECT. STRAIN C. STRAIN C. CLAND. STRAIN C.	ICAC.OD TEMPERATURE STRAIN B. PFCH.) STRAIN C. STRAIN C. LONG. STRN.	PASS= 17 -20.CC TEMPERATURE STRAIN 8. FECH.) STRAIN 8. FECH.) STRAIN 8. FECH.) STRAIN 8. F.	TEMPERATURE STRAIN B. (FECH.) STRAIN B. (STRAIN C. B. (CNC.) LCNC. STRA. B. (CNC.) LCNC. STRA. B. (CNC.) TEMPERATURE STRAIN B. (PECH.)
-113,38	147.57 20662 206662 -73.38 -113.38	147.57 266.62 246.62 -153.38 -133.38	147,57 326,62 216,62 -23,38 -93,38 366,67	147.57 356.62 136.62 -233.38 -633.8	374.657 136.657 -24.38 -3.34 36.43 36.43 147.97 370.65 -20.65 -20.65
-93.38	147. 236.62 236.62 -85.38 -113.37	147.44 116.62 226.62 1183.83 1183.33	184 184 1955 1055 111 111 125 145 145 145 145	40 1 4	14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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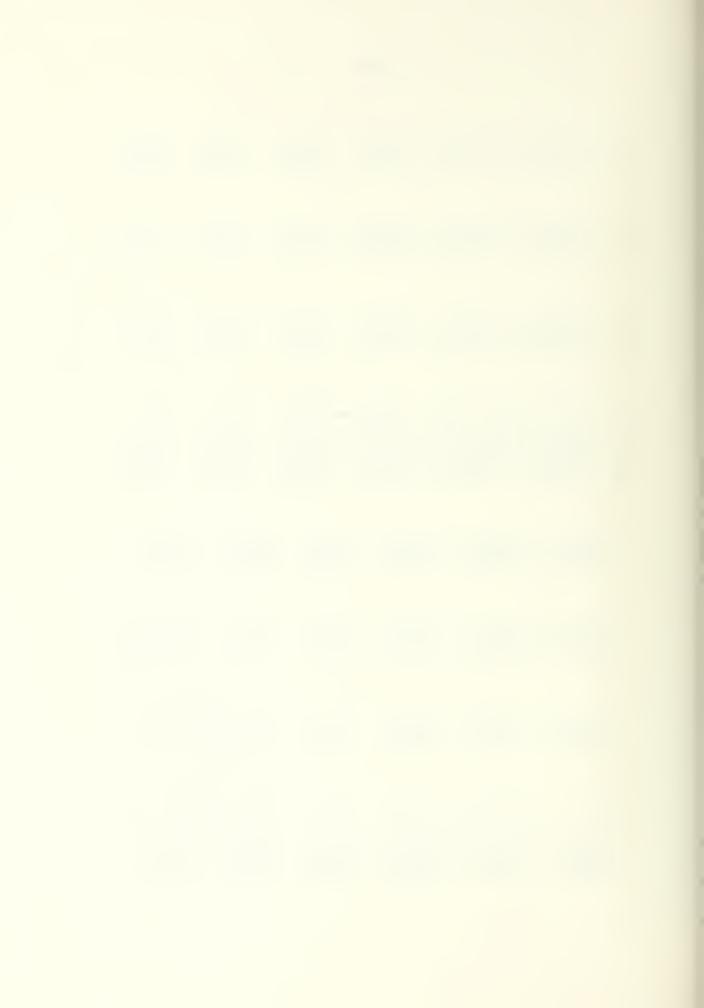
777.98	521.35	37A.56	STRAIN B.	251.46	150.30	201.46
				40.000 0.000 0.000 0.000 0.000	265.01	211.74
	151,38	147.57				
	5 4° 5	76.67	20-1			
	- 160.42	-243.38	TEMPERATURE	135.16	134.21	135.16
	149.58	29.95	Ē	-6.54	- 30.69	-14, 44
	214.76	376.78		251.46	250.30	201.46
			STRAIN C	191.46	140.30	81.46
				-66.54	-140.70	#C % # C # C
	142, 14	147.47	PRINC. STRN	280.14	20.692	00000
	47.16	366.62				
	-79.84	26.62	20-21			
	-289.84	-213, 38	TEMPERATURE	135.16	134.21	135.16
	26.16	126.62	STRAIN A. (PECH.)	151.46	120.30	101.46
	506.45	370.00	STRAIN 8	381.46	290.30	211.46
				51.46	-19.70	-14. K4
			LONG. STRN. "	-178.54	-149.70	-12A.54
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	150.43	147.57				
	420	346.62				
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'	-251000	-193.38	TEMPERATURE	137.67	135.16	135.16
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				471.67	347.75	231.74
	149.47	147.57				
	35A.28	316-62				
	-121.72	E (1)	18.40			
	-171.72	-153,38	TEMPERATURE	142.85	136.12	135,16
	3º 8.2A	166.62	STRAIN A. (PECH.)	701.43	272.43	231.46
	434.53	111.52	STRAIN B	311.43	162.63	91.46
			STRAIN C. "	-538,57	-257.33	-134.54
				-149.57	-47.37	1.46
			DEINC. STRN.	142.12	0	C 300 H 2
	208.28	286.62				
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	-81.72	RE-12-11-	TENDER ATION	148.52	134.12	135.16
	128.28	196.67	CTOATE A. CRECE.	R10.74	342.43	231.46
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			STRAIN CO.	-750°23	32.63	41.46
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	775.78	70.0r.				
	-41.72		A STANDED T	157,11	136.12	135.16
	3.8.29	2:6.62	CTDATA A. CRESTA	761.76	182 E	231046
	348.78	200.70	STORING P. B	136.0074	-17.17	1.46



				224017	-818-74	-247.37	-134,54
41,00				LCAG. STRA	111.26	132.63	31.46
TEMPERATURE	184, 77	150.43	147,57	2	,		
-	-47.38	219.70	236.62				
	-137,30	-61.00	-3,36	00.4		1	
	-157.38	-1.00	-23.36		164.74	136.12	115.16
Cons. Strat.	67.38	21.01.01.01.01.01.01.01.01.01.01.01.01.01	216.62	STRAIN A. (PECH.)	441.7	222.64	44 64
		1110 44	20.0012		-678.28	76.27.5 -277.37	108051
				LCAG STRA	2 - C - C - C - C - C - C - C - C - C -	252.€3	151.46
45.00					-917,31	346.65	240.14
TRHPFBATURE	30.00	151.30	147.57				
A. ( MF	14.21	179.58	196.62				
	-54. 21	-20.45	16.62	26.00			
		0.00	16.62	TEBPERATORE	180.00	el di el di el di el di el di el di	135.16
PARTY STREET	-254.71	7.0.58	196.62	STRAIN A. INFCH.	16.46	731.46	040111
	1907.6-	96 0/12	6330 V		7 (F	\$C 0 K 1/2	# W
					000624-	41.45.01.1	4 0 0 0 0
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TEMBERATURE	200		140 82	07.21.0			
CTOATE A. TERFEE.	119.72	17.00CI	147.44				
CTRAIN B		) d 10 45 10 11	47.44	00 0			
ن :	-340. 43	14.46	57.44	TEMPERATURE	214,25	135.12	136.21
LONG. STRM "		1.4.36	157.44	THUSAL W NIWALV	-345.96	52.63	10000
4		114.45	173, 51		-615.54	-217.37	- 99. 70
				CTRAIN C.	45.46	72.63	50,31
				,	40.441	367.63	750 30
65.74					-456.10	352.6₽	252004
TREST BATINE	251.55	169.51	152.34				
STRAIN A. (MECH.)	-199,59	-18.6	15.16				
STRAIN 8. "		\$1.4	70.16	34.70			
	-362. 59	41.4	100.16	TEMPERATLAE	240.10	139.00	134.21
-	-632.59	-78.67	134.16	STREEN A. INFILM	-463.63	-53,72	20.10
PRINT. STRN. "	-642.62	41.40	130.16	STRAIN B. "	rv°Edl-	-16%-72	-80°7C
				STRATH C. "	66.57	166.29	120.00
				L JNG. STRN.	-213°C	20002	291 0 27
		** ***		DRING. STRN.	40104-	44.47	57 ° 2 5 1
TOUR A MARKET	170 43	0000	1.0661				
	82.00	124.11	124.16	36.74			
	-369.63	24.11	174.36	TEMPERATURE	267,14	144.70	135.16
-		-195,89	34.36	STRBIN A. INFCH.	-445.11	-125.07	- 30° 54
PRINC, STRN, "		-266.77	137.84	S F D B F B D D	14.49	-115.87	-58.54
	•			STORIN C. "	14.80	194.13	191.45
				LCAG. STRN. "	-445.11	174017	501°46
95.77 GRAPK				PRINC. STRN. "	-540.36	741.38	241.75
TEMPERATURE	271.50	*** ~ ~ ~	167.67				
	120,17	-115.72		4			
I E MINIS		DA * * * * I			24.6.03	95 191	136 16
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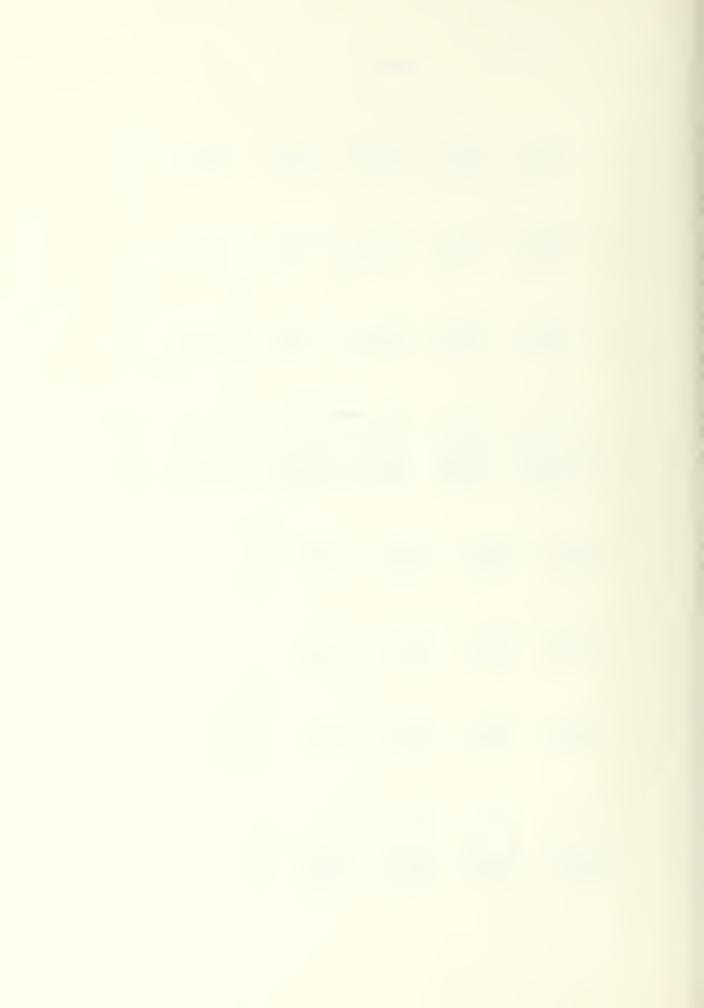


		21.2.44	30	PRING STRN. #	-526.22 -606.25	53,79	171.46
17.   18.   17.   18.   17.   18.   17.   18.   17.   18.   17.   18.   17.   18.   17.   18.   17.   18.   17.   18.   17.   18.   17.   18.   17.   18.   17.   18.   17.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.   18.	-119.	•	-10-1	;			
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17.21	- 456		200	THE PERMICAN		16.30.78	138.73
17. 21	- 62.		1:0121-	1 1 1	20.004	55.052-	20.49-1
217.2   190.68   PHING. STRM.   -590.00   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791.03   -791		Ľ.	700.01		70.05	210-41	2 C C C C C C C C C C C C C C C C C C C
217.21   86.68   PRINC, STRN,   -599,11   -231.63    -20.75   16.11   Teperature   -394.77   -134.09    -307.75   16.11   Teperature   -394.77   -134.09    -307.75   16.11   Teperature   -394.77   -134.09    -307.77   -16.57   STRAIN   -256.77   -118.77    -307.70   -397.70   -394.77   -234.11    -307.77   -16.57   STRAIN   -256.77   -118.77    -307.70   -397.70   -396.77   -394.77   -234.11    -307.70   -396.77   -396.77   -394.77   -394.77    -307.70   -396.77   -396.77   -394.77   -394.77    -307.70   -396.77   -396.77   -396.77   -396.77    -307.70   -396.77   -396.77   -396.77   -396.77    -307.70   -396.77   -396.77   -396.77   -396.77    -307.70   -396.77   -396.77   -396.77   -396.77    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -396.77    -307.70   -396.77   -396.77   -396.77   -396.77    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -396.77   -396.77    -307.70   -396.77   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -397.32    -307.70   -396.77   -396.77   -397.32    -307.					-530°CC	-30.50	165,05
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200.62				PINC. STRN.	-584.57	-375, 62	195, 17
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192,44  192,44  192,44  197,44  -65,82  184 N 8. (PECH.)  242,97  192,94  -266,82  STRAIN 8. (PECH.)  175,44  176,00  177,14  176,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  177,14  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00  170,00	22.	5.5	-25.82				
-97.56 -937.56 -265.82   TRMIN A. (FECH.)   242.97   197.17 -338.74   -265.82   STRAIN A. (FECH.)   -276.92   197.16 -338.74   -266.73   STRAIN C.     42.66.73   197.16 -178.74   178.74     178.14     178.66.73   -377.16 -178.75   186.87   170.00   222.93   197.17 -178.57   186.87   170.00   222.93   197.17 -232.43   -273.13   STRAIN A. (FECH.)   -229.36   197.17 -232.49   -273.13   STRAIN B.     90.65   197.17 -240.49   -278.18     90.65   197.17 -240.49   196.20     178.69     178.69     178.20     178.69     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20     178.20	232.		174.18	120.00			
-336.74 -265.82 STRAIN 8. (PECH.) -778.67 -737.14 -336.74 -266.73 STRAIN 8. (PECH.) -778.67 142.86 -34.74 STRAIN 8. (PECH.) -58.67 162.86 -47.57 176.87 176.87 170.00 -42.64 -27.13 STRAIN 8. (PECH.) -27.93.14 -232.64 -27.13 STRAIN 8. (PECH.) -27.93.14 -232.64 -27.13 STRAIN 8. (PECH.) -27.93.14 -242.64 -27.13 STRAIN 8. (PECH.) -365.38 -37.14 -242.64 -26.65 STRAIN 8. (PECH.) -365.38 -37.16 -242.65 -27.13 STRAIN 8. (PECH.) -365.38 -377.16 -36.07 171.93 3.60.00 -168.07 STRAIN 8. (PECH.) -186.67 -165.26 -131.00 -168.07 STRAIN 8. (PECH.) -186.67 -165.26	-187.		-65.A2	TEMPERATURE	242.97	157.17	162.83
-336.74 -266.73 STRAIN 80 m 241.077 142.00 C	- 497.		-265,82	STRAIN A. (PECH.)	-278,52	-237,14	-120.03
STRAIN C. 170.46  170.76	-414-		-266.73		241007	142.86	69.77
### ### ### ### ### ### #### #### ######					61.67	102.46	149.07
## 176.70   177.14   PRINC. STRN.   -498.67   -337.32   ## 17.57   30.87   170.00   ## 17.57   180.87   170.00   ## 17.57   180.87   170.00   ## 150.43   -273.13   STRAIN A.   PECH.   -229.3   197.17   ## 150.43   -273.13   STRAIN A.   PECH.   -229.3   ## 150.43   154.20   STRAIN A.   PECH.   -390.0   ## 150.00   170.93   160.00   ## 150.00   170.93   TEMPERATURE   178.0   ## 150.00   170.93   TEMPERATURE   ## 150.00   ## 150.00   170.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 170.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 150.00   ## 170.00   ## 150.00   ## 150.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.00   ## 170.0					-45E.93	-277.14	-40.03
## ## ## ## ## ## ## ## ## ## ## ## ##					-498.03	-337,32	1500 65
17.57   190.87   170.00   222.92   197.17   190.89   17.57   190.87   170.80   222.92   197.17   190.87   190.87   190.87   197.17   190.87   197.17   190.87   197.17   197.17   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197.27   197	183	2 6	177.14				
11	116		10.00	200			
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53   159-37   171-93   3-60-00 47 -51-07 -38-07   TEMPERATURE   178-09   173-32 47 -131-00 -186-07   STRAIN A- (PECH-0   -148-47 -195-74 172-91   176-58   STRAIN B-   151-23   154-26 STRAIN C-   131-53   174-26	157		66.14	4			
47 -91.00 -168.07 TEMPERALURE 178.09   173.32   -47 -191.00 -168.07 STRAIN 8. (FCM.( -148.47 -195.74   176.26   STRAIN 8.	212	5.5	171.93	360.00			
-131.00 -168.07 STRAIN A. (FECH. ( -148.47 -195.74 - 175.91 176.58 STRAIN G. H. 151.53 154.26 STRAIN C. H. 131.53 174.26 STRAIN C. H. 131.53 174.26 STRAIN C. H. 131.53 174.26	-67	47	-00°0-		178.09	173,32	167.60
77 172.91 176.58 STAIN 8. " 151.53 154.26 STAIN C. " 131.53 154.26 STAIN C. " 131.53 154.26	-127	1.4	-10.80		-148.47	-195,74	-184.16
92°401 (SS°80)	245	22	176.58		151.43	154.26	125.84
						104.26	75° FF



126				PAINC. STRN. *	-221°C?	-25E-14	-260329
TEMPERATIBE	139.94	130.01	140.89				
STRAIN A. (MFCH.)	187.61	11. 61	51.31				
STRATM R. "	19.662	15. 61	161.31	630°06			
STRAIN C "	-49.30	-29.19	-38.69	TEMPFRATLRE	162.92	159,07	A C @ G S M
1 THG. STRN "	-69.39	-69.39	-148.69	STRAIN A. IPECH.)	-110.53	-164.68	-137.46
PRINC, STAN, "	247.95	171.	167,71	STRATM B	169.07	16 6, 12	152,54
				STRAIN C	165.07	114.12	172.54
				LONG. STRN.	-11-03	134.88	-197.46
\$100.00				PRINC. STAN. "	227°04	-240.19	-226, KG
TERPERATIME	97.96	98.91	98,91				
STRATE A. (MFCH.)	304.96	104.00	146.09				
STRAIN P.	264,96	224,99	234.99	30,403			
STRAIN C	54.96	66.99	44.09	TFMPFRATURE	142,95	140.80	141,04
COME, STAM, T	94.96	34.99	19.86-	STRAIN A. (PECH.)	-RA.57	-141.18	-119,89
PRINC. STRW. "	331.12	245.19	245,76	STRAIN 8	171.43	179.92	140,11
				* CEATA	181.4	148.47	10001
				FORES STAN	-78.57	-171-18	- 1 to B 3
0000				PRINC. STRN. "	230.41	33100	-204°CS
TEMPERATIRE	91,28	91.28	94,1"				
STRAIN A. (MECH.)	295, 19	195.19	134.97				
STRATE 8	255,10	195,19	204.97	1,500,000			
STRATE C	54,19	64.19	44.97	TEMPERATURE	122.76	122.76	125.62
LONG. STAN. "	95.19	54.19	-25.03	STRBIN & (MECH.)	-51.95	-121,35	-89.16
PRINC. STRN. "	110.41	24.19	213.46	STRAIN 8. "	188.75	50000	170.R4
				STRAIN C. "	208.05	164.04	130.04
				LING. STRY	-31.54	-161.95	-120.14
ITHE CHOLD-DOWN CLAMPS		RELEASEO)		PRINC. STRN. "	24 P . 3 F	254.10	2r6.R5
TEMPERATIIRE	91.28	91.28	95.1		010 (40.000)	(at et a consolition	
STRAIN A. IMPCH.1	195.19	95,19	54.97	PASS ZO (FINAL C			
STRAIN B	95.19	15,19	54, 97	20.6555			
STRAIN C. "	25,19	-984.81	24.97	TEMPERATURE	74.11	73.18	73.15
LONG. STRN "	125.19	-924.81	24.97	STRAIN A. IMECH. 1	-70.41	-100.21	-90.21
PRINT STRM. "	196.51	-1167.3	61.18	STRAIN B	250.65	279.79	230.70
				STRAIN C	189,59	149.79	RO. 79
				LCNG. STRN. "	-140.41	-210.21	-230.21
				PRINC. STRN. "	79 A . 1 3	77 a d C E	254.49
COMPTIF TIME	** 46 SEC. EXECUTION TIME.	ON TIME 6	2 SEC, OR JECT CODE=				
COMPTIE TIME.	A THE SECTION TIMES	" "HE" "	"> SEC. DBJECT CODE"	10000,00 (HOLD-DOWN CLAMPS RELEASED)	A CLAMPS RELE	D 5 ( D )	
				TEMPERATURE	73.14	72.2C	71,15
				STRAIN A. IPECH.	-100,21	-140,00	-90.21
				STRAIN R.	134.79	160.36	139,79
				STRAIN C. "	129.79	00°00"	37.79
				LCNG. STRW	-110.21	ひで * シンベー	-10v° 21
						111 111	

CCMPILE TIME» 0.63 SEC.EXECUTION TIME» 6.43 SEC.CAJEGT CODE*
CCMPILE TIME» 0.74 SEC.EXECUTION TIME» 0.03 SEC.09JEGT CODE*



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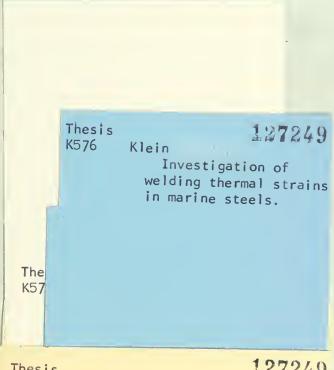
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